

# Carmon Creek

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## Structural Analysis

### Carmon Creek – Base Skids and Dropover Enclosures De Jong Combustion / NEM Energy

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## **Index**

<b>1</b>	<b>Introduction .....</b>	<b>6</b>
1.1	Project description .....	6
1.2	Scope of delivery .....	6
1.3	Code selection.....	6
1.4	Design Load Conditions .....	7
1.5	Load Cases .....	7
1.6	Load Combinations .....	8
1.7	References .....	8
1.8	Materials .....	8
1.8.1	Primary steel .....	8
1.8.2	Secondary Steel.....	8
1.8.3	Fasteners.....	8
1.9	Design Criteria .....	9
1.9.1	Deformation Limits.....	9
1.9.2	Slenderness .....	9
1.10	Computer software .....	9
<b>2</b>	<b>Structural Analysis - Operational - A1 OPE .....</b>	<b>10</b>
2.1	FEA model .....	10
2.2	Load Case Application .....	11
2.2.1	Permanent load – Selfweight Auto .....	11
2.2.2	Permanent load – Selfweight Panels.....	11
2.2.3	Permanent load – Equipment and HVAC .....	11
2.2.4	Variable load - Snow.....	12
2.2.5	Variable load – Roofload.....	12
2.2.6	Variable load – Floorload .....	12
2.2.7	Variable load – Crane Loads.....	12
2.2.8	Variable Load – Wind1 long side (Y+).....	13
2.2.9	Variable Load – Wind2 short side (X-) .....	13
2.2.10	Seismic Loads .....	14
2.3	Results.....	15
2.3.1	Unity Checks .....	15
2.3.2	Stress .....	16
2.3.3	Deformation .....	17
<b>3</b>	<b>Detail Analysis – Operational - D1 OPE .....</b>	<b>18</b>
3.1	Reactions .....	18
3.2	Results.....	18
<b>4</b>	<b>Detail Analysis – Operational - D2 OPE .....</b>	<b>19</b>
4.1	Reactions .....	19
4.2	Results.....	19
<b>5</b>	<b>Structural Analysis – Lifting - A2 LIFT .....</b>	<b>20</b>
5.1	FEA model .....	20
5.2	Results.....	21
5.2.1	Unity Checks .....	21
5.2.2	Stress .....	22
5.2.3	Deformation .....	23
<b>6</b>	<b>Detail Analysis – Lifting - D3 LIFT .....</b>	<b>24</b>
6.1	Shackle.....	24
6.2	Padeye.....	24





6.3	Bolted Connection .....	24
<b>7</b>	<b>Structural Analysis – Deformation - A3 DEF.....</b>	<b>25</b>
7.1	FEA model .....	25
7.2	Results.....	26
7.2.1	Unity Checks .....	26
7.2.2	Stress .....	26
7.2.3	Deformation .....	27
<b>8</b>	<b>Structural Analysis – Lifting - B LIFT .....</b>	<b>28</b>
8.1	FEA model .....	28
8.2	Results.....	28
8.2.1	Unity Checks .....	28
8.2.2	Stress .....	29
8.2.3	Deformation .....	30
<b>9</b>	<b>Structural Analysis – Lifting - C LIFT .....</b>	<b>31</b>
9.1	FEA model .....	31
9.2	Results.....	32
9.2.1	Unity Checks .....	32
9.2.2	Stress .....	32
9.2.3	Deformation .....	33
<b>10</b>	<b>Detail Analysis – Lifting - D4 LIFT .....</b>	<b>34</b>
<b>11</b>	<b>Conclusion .....</b>	<b>35</b>
11.1	Structural Analysis - Operational - A1 OPE .....	35
11.2	Detail Analysis – Operational - D1 OPE .....	35
11.3	Detail Analysis – Operational - D2 OPE .....	35
11.4	Structural Analysis - Lifting – A2 LIFT.....	35
11.5	Detail Analysis – Lifting - D3 LIFT .....	35
11.6	Structural Analysis – Deformation - A3 DEF.....	35
11.7	Structural Analysis – Lifting - B LIFT.....	35
11.8	Structural Analysis – Lifting - C LIFT .....	36
11.9	Detail Analysis – Lifting - D4 LIFT .....	36
<b>Appendix A</b>	<b>Load Combination Table .....</b>	<b>38</b>
<b>Appendix B</b>	<b>Padeye design sheet – Full set.....</b>	<b>43</b>
<b>Appendix C</b>	<b>Padeye design sheet – Dropover Enclosure .....</b>	<b>45</b>
<b>Appendix D</b>	<b>3D lifting point datasheet .....</b>	<b>47</b>
<b>Appendix F</b>	<b>FEA Output Report (Autodesk Robot) .....</b>	<b>50</b>
<b>Appendix G</b>	<b>Addendum .....</b>	<b>51</b>



## **Index of Figures**

Figure 2-1 FEA model showing columns and beams .....	10
Figure 2-2 FEA model showing panels.....	10
Figure 2-3 Seismic input in Autodesk Robot.....	14
Figure 2-4 Unity Checks for top utilized profiles (>40%), sorted on overall ratio, high to low .....	15
Figure 2-5 Visual presentation of unity checks (blue 0-33%; green 34-67%; orange 68-100%) .....	15
Figure 2-6 Stress peaks in profiles .....	16
Figure 2-7 Stress in panels .....	16
Figure 2-8 Deformation of profiles.....	17
Figure 5-1 Lifting set up with spreader beam .....	20
Figure 5-2 FEA model with constraints (x=fixed; f=free) .....	20
Figure 5-3 Unity Checks for top utilized profiles (>8%), sorted on overall ratio high to low.....	21
Figure 5-4 Visual presentation of unity checks (blue 0-33%; green 34-67%; orange 68-100%) .....	21
Figure 5-5 Stress peaks in profiles .....	22
Figure 5-6 Stress in panels .....	22
Figure 5-7 Deformation of profiles.....	23
Figure 7-1 FEA model with constraints .....	25
Figure 7-2 Unity Checks for top utilized profiles (>10%), sorted on overall ratio high to low .....	26
Figure 7-3 Stress peaks in profiles .....	26
Figure 7-4 Stress in panels .....	27
Figure 7-5 Deformation of profiles.....	27
Figure 8-1 FEA model with constraints .....	28
Figure 8-2 Unity Checks for all profiles.....	28
Figure 8-3 Stress peaks in profiles .....	29
Figure 8-4 Stress in panels .....	29
Figure 8-5 Deformation of profiles.....	30
Figure 9-1 Dropover lifting set up .....	31
Figure 9-2 Unity Checks for top utilized profiles (>4%), sorted on overall ratio high to low.....	32
Figure 9-3 Stress peaks in profiles .....	32
Figure 9-4 Stress in panels .....	33
Figure 9-5 Deformation of profiles.....	33

## **Index of Tables**

Table 1-1 References .....	6
Table 1-2 Calculation models.....	7
Table 1-3 Load Cases for Calculation model A1 Operational .....	7
Table 1-4 Reference Drawings of production model.....	8
Table 1-5 Primary structural steel .....	8
Table 1-6 Secondary structural steel .....	8
Table 1-7 Industrial Buildings Informative Maximum Deflections per CSA S16-09 Table D.1 .....	9
Table 2-1 Panel weights .....	11
Table 2-2 Equipment weights .....	11
Table 2-3 HVAC weights .....	11
Table 2-4 Wind load calculation .....	13
Table 2-5 Seismic data input.....	14
Table 3-1 Max/Min ULS Reactions from A1 OPE.....	18
Table 4-1 Max/Min ULS Reactions from A1 OPE.....	19



# 1 Introduction

## 1.1 Project description

For the Shell Carmon Creek site, burner skid units will be delivered by De Jong Combustion BV. For each unit, 5 burner skids will be installed on an enclosure skid with dropover enclosure for protection against environmental conditions.

Alara-Lukagro BV will design and manufacture the enclosure skids and enclosures.

This structural verification, will verify the structural capacity of the enclosure skid and dropover enclosure based the governing Canadian structural codes.

Please note that due to an deviation in the 3<sup>rd</sup> unit an addendum is attached for lifting verification.

## 1.2 Scope of delivery

Alara-Lukagro will deliver:

- 3 identical Enclosure Skids ('main skid') carrying the burner skids by de Jong Combustion BV.
- 3 identical Dropover Enclosures ('hoods') to be connected to the enclosure skids.

Internal equipment:

- Fixed lifting beams supporting a travelling lifting beam and lifting trolley WLL 250 kg by Alara-Lukagro BV
- HVAC system by Alara-Lukagro BV
- 5 x Burner Skids by De Jong Combustion BV
- Header and pipe spools by De Jong Combustion BV
- Header support including local panel by De Jong Combustion BV
- Cable trays to connect valves and instruments for gas system by De Jong Combustion BV
- E-system, like lighting, is part of the scope, but structurally not significant.

## 1.3 Code selection

The governing specification is the Technical Requisition (TR) by De Jong Combustion BV: 08750-SP020-R01 with below referred to specifications with regard to structural verification.

*"The scope of supply shall be in accordance with all the documents mentioned below (in sequence of priority) and the documents and specifications referred therein"*

Table 1-1 References

No	Ref	Name	Description	Rev	Date
1	TR §1.1	CSA S16-09	<i>Design of Steel Structures</i>	2	2012-02
2	TR §1.2	MoM	<i>Minutes of Meeting 20-11-2013</i>	0	20-11-2013
3	-	MoM	<i>Minutes of Meeting 11-04-2014</i>	0	11-04-2014
4	TR §1.3	DEP 34.00.01.30-Gen	<i>Structural Design and Engineering of Onshore Structures</i>		2011-09
5	TR §1.3	DEP 34.28.00.31-Gen	<i>Onshore Steel Structures</i>		2011-09
6	TR §1.3	DEP 34.28.00.33-Gen	<i>Onshore Ancillary Steel Structures</i>		2011-09
7	TR §1.3	CCK-0000-CS-7880-00-0002-000	<i>Spec for Detailing, Supply and Fabr. of Struct. And Misc. Steel</i>	02A	21-11-2012

The primary code to be used is CSA S16-09 with extra requirements where applicable according the provided structural Shell DEPs.

In CSA S16-09 for determining the load factors, there is reference made to NBCC 2010 (National Building Code of Canada) §4.1.2.1. The NBCC was not available for this project, so a Basis of Design provided by contractor NEM Energy BV is used.<sup>1</sup>

<sup>1</sup> 36026-300-10-001-R1PE with Permit No. 11193



## 1.4 Design Load Conditions

The table below shows the conditions and considerations for the structural verification and the resulting calculation models to be made.

Table 1-2 Calculation models

Consideration	Calc.	Condition	Comment
The complete set must be able to withstand the environmental conditions	A1	OPE	
Bolted Connection to existing support structure	D1	OPE	Using results of model A1
Bolted Connection between enclosure skid and dropover enclosure	D2	OPE	Using results of model A1
The complete set must be able to be lifted to its final location	A2	LIFT	
Design of Primary Lifting Eye for lifting a complete assembled set of enclosure skid and dropover enclosure.	D3	LIFT	Based on total 30T
According Technical Requisition 08750SP020-R01 the enclosure skids + enclosure sets "will be supported in the field by a platform with maximum deflection, being length/300 mm. Supplier to confirm that skid enclosure is stiff enough of deal with bending of the support platform" The deformation of the structure will be compared to this limit.	A3	DEF	Extra limit to be considered
The enclosure skid must is required to be lifted while carrying the burner skids and other applicable equipment.	B	LIFT	
The dropover enclosure must be able to be lifted with attached applicable equipment	C	LIFT	
Design of (removable) Secondary Lifting Eye for lifting the dropover enclosure	D4	LIFT	Based on total 10T
OPE :	Operational Condition		
LIFT:	Lifting Condition		
DEF :	Deformation Condition		

Structural Calculations for transport conditions (ship inertia etc.) are excluded from the scope of Alara-Lukagro BV: sea transport and dynamic loads are excluded according Chapter 11 of the Technical Requisition.

The objective of this report is to verify the structural safety of each calculation model and detail design as seen in Table 1-2 subjected to the applicable loads.

## 1.5 Load Cases

As NBCC<sup>2</sup> 2010 was not available for the project, BoD 36026-300-10-001 as provided by NEM Energy BV will be adopted. This Basis of Design is used on an equivalent structural application for the Carmon Creek Project.

The load cases in the table below are applicable for the operational condition.

Table 1-3 Load Cases for Calculation model A1 Operational

No	Lbl	Description	Nature	Value	Misc	Ref
1	G1	Structure Selfweight	dead	auto		Structural members, panels and nodal masses
2	SN1	Snow	snow	2,8 kN/m <sup>2</sup>		
3	L1	Roof load	live	1,0 kN/m <sup>2</sup>	120 kg/pt	ABC <sup>3</sup> Table 4.1.5.3
4	L2	Floor load	live	4,8 kN/m <sup>2</sup>		
5	L3	Crane loads	live	WLL 250kg		DEP 34.00.0130-Gen 3.11 / 3.15
6	W1	Wind1 - long side	Wind	0,51 kN/m <sup>2</sup>	Base value	ABC Table C-2
7	W2	Wind2 - short side	Wind	0,51 kN/m <sup>2</sup>	Base value	
8	E1	Modal	Modal			
9	SEI_X	Seismic - NBCC 2010 Direction_X	Earthquake			ABC
10	SEI_Y	Seismic - NBCC 2010 Direction_Y	Earthquake			ABC
11	SEI_Z	Seismic - NBCC 2010 Direction_Z	Earthquake			ABC

<sup>2</sup> National Building Code Canada

<sup>3</sup> Alberta Building Code (local implementation on national code)

## 1.6 Load Combinations

Load Combinations are per NBCC 2010. These are automatically generated in Autodesk Robot when selected. See the table in Appendix A for the combinations.

## 1.7 References

The referred drawings of the 3D production model are the following:

Table 1-4 Reference Drawings of production model

Drawing Nr.
405109540-100 1/2
405109540-100 2/2
405109540-600 1/4

Please note that the referred

- De Jong Combustion Technical requisition 0875-SP020;
- NEM Energy BoD 36026-300-10-001;
- CSA;
- EN;
- ASTM;
- Shell DEP;
- and other codes

are not attached in the appendices.

## 1.8 Materials

### 1.8.1 Primary steel

The TR specifies ASTM 572 Grade 50 to be used with Longitudinal Charpy test value of minimum 27 J @ -45 °C. As this material is locally not available for the structural profiles, an European equivalent is selected:

EN 10025-2<sup>4</sup> S355 (or higher) material with extra impact tests to confirm the Charpy test value for the minimum 27J @ -45°C as specified in the TR.

During inquiry for the required material and sections the following materials were available and selected.

Table 1-5 Primary structural steel

Application	Pos	Use		Grade	fy (MPa) yield	fu (MPa) tensile	Cert.
Rectangular Hollow Sections	Enclosure	Primary	EN 10219	S420MH	420	500-660	3.1
Open H-; I-; U- profiles	Skid	Primary	EN 10225	S355G11+M	355	460-490	3.2
Plating 2mm	Encl. Walls	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>5</sup>
Plating 3mm	Encl. Roof	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>5</sup>
Plating (Checker plate) 4mm	Skid Floor	Primary	EN 10025-2	S235JR	235	360-510	2.2 <sup>5</sup>

### 1.8.2 Secondary Steel

Secondary steel comprises the cold formed steel sheet for small brackets for miscellaneous lightweight equipment. These brackets are not modeled.

Table 1-6 Secondary structural steel

Application	Pos	Use		Grade	fy (MPa)	fu (MPa)	Cert.
Brackets small equipment	Wall, Roof	Secondary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>5</sup>

### 1.8.3 Fasteners

Metric sizes will be used, unless noted otherwise:

<sup>4</sup> Fine grain normalized steel according EN 10025-3 is a near equivalent material, for example S355NL with 27 J @ -50 °C. But it is only available for plates, but not for structural profiles.

<sup>5</sup> EN 10152 is applicable for plate material, for impact test ref. EN 10025-1 §7.3.2.1 which states that impact tests are not required for nominal thickness <6mm.



- MoM 2014-04-11 Item 5 is regarding the structural bolt for fastening the enclosure skid with enclosure to the supporting platform. NEM Energy BV would investigate details. 2014-04-14 NEM Energy BV stated:

“With regard to point of the MOM please be informed that for mounting of the enclosures on the steel structure Imperial bolts (UNC) and nuts shall be used.  
Mounting bolts and nuts shall be in the DJC / Alara Lukagro scope of supply”

These UNC fasteners will be considered in the structural analysis, but are at this moment not in scope of Alara-Lukagro BV.

## 1.9 Design Criteria

### 1.9.1 Deformation Limits

The figures refer to the maximal deflection under permanent and variable actions under SLS-combinations according design code.

*Table 1-7 Industrial Buildings Informative Maximum Deflections per CSA S16-09 Table D.1*

<b>Deflection</b>	<b>Specified loading</b>	<b>Application</b>	<b>Maximum</b>
Vertical	Live, snow	Members supporting floors	L/300
Vertical	Maximum wheel loads (no impact)	Crane runway girders for crane capacity under 225 kN	L/600
Lateral	Crane lateral	Crane runway girders	L/600
Lateral	Crane lateral or wind	Storey drift*	h/400 (to h/200) (3360/300=8,4mm)

Legend:

h = storey height.  
L = length or span.

\*The permissible drift of industrial buildings depends on such factors as wall construction, building height, and the effect of deflection on the operation of the crane. Where the operation of the crane is sensitive to lateral deflections, a lateral deflection of less than h/400 may be necessary.

### 1.9.2 Slenderness

- Max slenderness for a member in compression is 200 per CSA S16-09 §10.4.2.1
- Max slenderness for a member in tension is 300 per CSA S16-09 §10.4.2.2

## 1.10 Computer software

- Autodesk Robot Structural Analysis Professional 2014
- Microsoft Excel
- Microsoft Word

## 2 Structural Analysis - Operational - A1 OPE

This chapter regards the analysis of the steel structure comprising enclosure skid and dropover enclosure in operational condition subjected to environmental loads.

### 2.1 FEA model

In the images below the steel structure is shown as only the structure visible and as the structure with panel faces. These faces add stiffness to the structure and distribute the loads to the applicable members. The properties of these panels is based on the plate thickness of the material used for the wall, roof and floor.

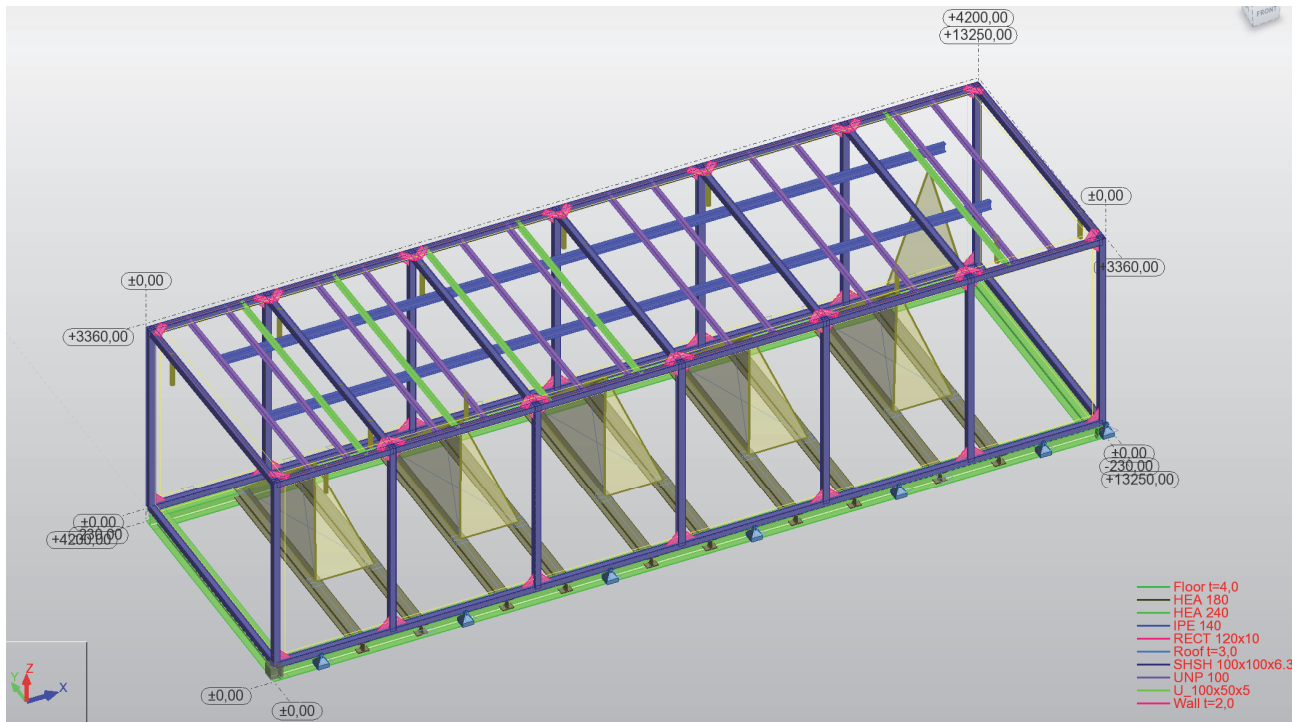


Figure 2-1 FEA model showing columns and beams

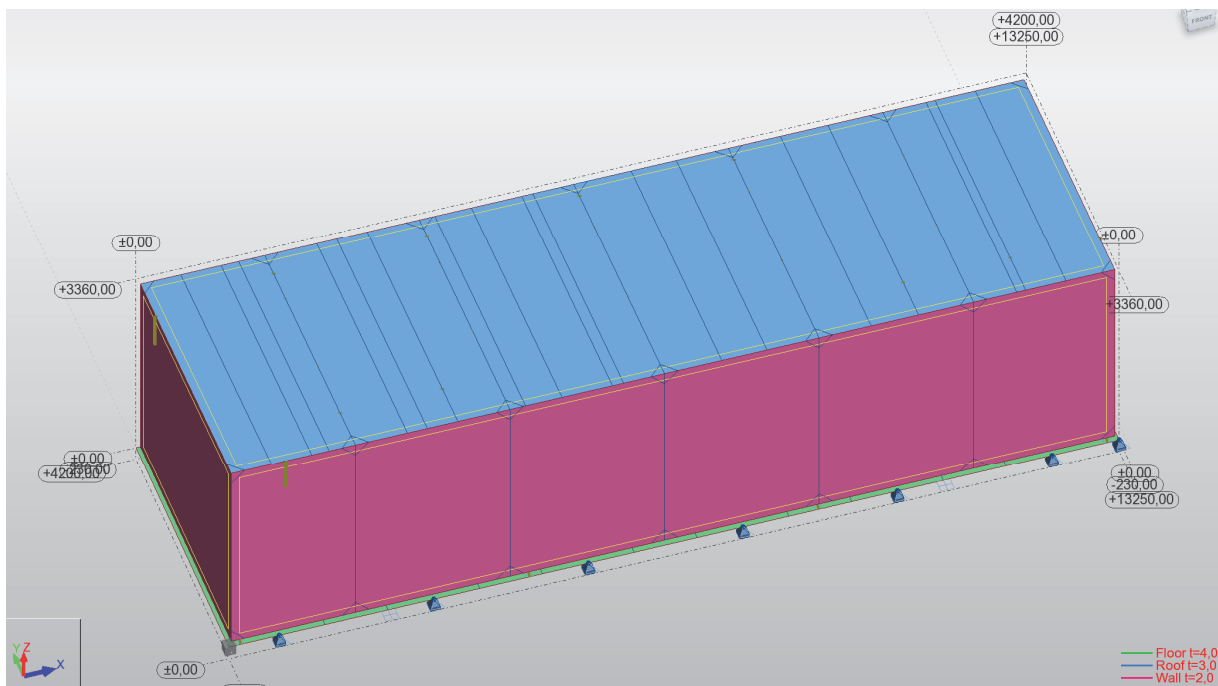


Figure 2-2 FEA model showing panels



The dropper enclosure is modeled as a structure separate from the enclosure skid. At the locations of the connection points the corresponding nodes are connected by rigid link interfaces (infinitely stiff calculation element).

The resulting forces at these locations can be used to verify the connection design.

The enclosure skid is supported at the 14 locations where it will be bolted to the support structure.

## 2.2 Load Case Application

The application of the load cases will be explained below per case.

### 2.2.1 Permanent load – Selfweight Auto

Autodesk Robot automatically assigns the selfweight of the modeled structure to the 1<sup>st</sup> load case as - 9,8065 m/s<sup>2</sup> or -1,0 g in z direction.

### 2.2.2 Permanent load – Selfweight Panels

The structure comprises the wall, roof and floor panels.

As their weight is automatically accounted for based on the modelled plate thickness, an additional load need to be applied to compensate the full weight of the panels.

Table 2-1 Panel weights

Pos	Typical Weight	Modeled thickness / Weight	Additional Distributed load
Wall	32,6 kg/m <sup>2</sup>	2mm / 15,7 kg/m <sup>2</sup>	Z=-166 N/m <sup>2</sup>
Roof	36,0 kg/m <sup>2</sup>	3mm / 23,55 kg/m <sup>2</sup>	Z=-122 N/m <sup>2</sup>
Floor	7458 kg (production model)	5347 kg (members and 4mm panel)	Z=-372 N/m <sup>2</sup>

### 2.2.3 Permanent load – Equipment and HVAC

The equipment by De Jong Combustion and HVAC items are modeled as nodal masses connected to the structure by rigid links.

Table 2-2 Equipment weights

Pos	Weight	
5 Burner skids	5 000,0	kg
Support + loc control	125,0	kg
Headers + cable tray	1 917,0	kg
<i>Total</i>	<i>7 042,0</i>	<i>kg</i>

Table 2-3 HVAC weights

Exhaust		W		QTY	Subtot	
X1-WL-001	Weather louvre	22	kg	1	22	
X1-MCD-001	Closing Damper	36	kg	1	36	
	Transition duct	44	kg	1	44	
X1-SA-001	Sound Attenuator	90	kg	1	90	
	Transition duct	16	kg	1	16	
X1-EF-001	Extract Fan	15	kg	1	15	
X1-MVD-001	Damper	13	kg	1	13	
	Duct	52	kg	1	52	
	Ducts low	25	kg	4	100	
	Transition duct	17	kg	1	17	
	Duct end	58	kg	1	58	
					<b>462</b>	<b>kg</b>
<b>Inlet 001</b>						
		W		QTY	Subtot	
X1-RH-001	Rainhood	70	kg	1	70	kg
X1-MCD-002	Closing Damper	12	kg	1	12	kg
	Bend duct 90°	35	kg	1	35	kg
X1-SA-002	Sound Attenuator	45	kg	1	45	kg





X1-AF-001	Filter	15	kg	1	15	kg
X1-UH-001	Heater				82	kg
					<b>259</b>	<b>kg</b>
<b>Inlet002</b>						
		<b>W</b>		<b>QTY</b>	Subtot	
X1-RH-002	Rainhood	70	kg	1	70	kg
X1-MCD-003	Closing Damper	12	kg	1	12	kg
X1-SA-003	Sound Attenuator	45	kg	1	45	kg
X1-AF-002	Filter	15	kg	1	15	kg
X1-UH-002	Heater				82	kg
					<b>224</b>	<b>kg</b>
		<b>HVAC Total</b>			<b>945</b>	<b>kg</b>

#### 2.2.4 Variable load - Snow

The snow load is applied to the complete roof as a distributed load.

It is calculated according to the ABC, with values that are specified in the project Specifications, based on the BoD provided by NEM Energy.

$$S_s = 2.3 \text{ kPa} = 2.3 \text{ kN/m}^2$$

$$S_r = 0.4 \text{ kPa} = 0.4 \text{ kN/m}^2$$

$$I_s = 1.25$$

$$\text{Wind exposure factor: } C_w = 1.0$$

$$\text{Basic roof snow load factor: } C_b = 0.8$$

$$\text{Slope factor: } C_s = 1.0$$

$$\text{Shape factor: } C_a = 1.0$$

$$S = I_s \cdot [S_s \cdot (C_b \cdot C_w \cdot C_s \cdot C_a) + S_r] = 2.8 \text{ kN/m}^2$$

#### 2.2.5 Variable load – Roofload

The entire roof of about 60m<sup>2</sup> is loaded with an applied distributed load of 1,0 kN/m<sup>2</sup> according ABC as stated in the BoD provided by NEM Energy BV. This is a more unfavorable loading over applying point loads of 120 kg at each member ("at any location").

#### 2.2.6 Variable load – Floorload

The floor ("corridor") of about 60m<sup>2</sup> is loaded with an applied distributed load of 4,8 kN/m<sup>2</sup> according ABC as stated in the BoD provided by NEM Energy BV.

#### 2.2.7 Variable load – Crane Loads

The loads by the hand operated chain hoist of WLL 0,25 T are determined according DEP 34.00.01.30-Gen.

- The DEP 3.11 a) states that "Design lift load shall be equal to two times the lifted load unless a larger factor is required by applicable codes and standards. This factor includes impact."

As the load factor applied due to use of CSA S16-09 load factors is already '1,5', the load of 250 kg will be multiplied with (2,0 / 1,5 =) **1,33**.

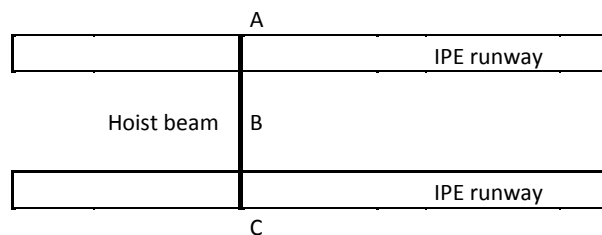
This results in 333,3 kg or 3270N.

The 3 trolleys are each 6,5 kg, chain hoist 5 kg and hoist beam is 26 kg.

- The load is applied in the most unfavourable position: asymmetric and in the middle of the span.



According to DEP 34.00.01.30-Gen Table 3.3 the following load increases are applicable for the 3 directions. This results in the load values shown below.



		increase	A		C	
FX	long	5%	13	N	-184	N
FY	trans	5%	13	N	-184	N
FZ	vert	110%	281	N	-4 043	N

### 2.2.8 Variable Load – Wind1 long side (Y+)

The Design wind pressure is calculated as:

Table 2-4 Wind load calculation

$P = I_w \times q \times C_e \times C_g \times C_p$						
Term	Value	Unit	Description	Ref		
$I_w$	1,25	-	Importance factor	ABC 2006 Table A-2, Commentary A		
$q$	0,51	kN/m <sup>2</sup>	Ref velocity pressure	ABC 2006 Table C-2 (location Peace River, return period 50 years)		
$C_e(z_0)$	1,06	-	Exposure factor	$(h/10)^{0,2} > 0,9$ for open terrain	$z_0$	13,680 m
$C_e(z_1)$	1,12	-	Exposure factor	$(h/10)^{0,2} > 0,9$ for open terrain	$z_1$	17,270 m
$C_g$	2	-	Gust factor			
$C_p$	0,8	-	External pressure coefficient	Windward wall (highest long wall) wind in Y+ direction		
$C_p$	0,5	-	External pressure coefficient	Leeward wall (lowest long wall) wind in Y+ direction		
$C_p$	0,7	-	External pressure coefficient	Roof suction ( $\alpha < 16,7\%$ )		

	Windward		Roof		Leeward	
			996	N/m <sup>2</sup>		
P(17270)	1 138	N/m <sup>2</sup>			711	N/m <sup>2</sup>
P(13680)	1 086	N/m <sup>2</sup>			679	N/m <sup>2</sup>

### 2.2.9 Variable Load – Wind2 short side (X-)

Please see §2.2.7 for wind load input. The input is the same, but direction application 90° rotated.

## 2.2.10 Seismic Loads

Seismic data according to ABC are shown below.

Table 2-5 Seismic data input

Parameter	Value	Ref
Sa(0.2)	0.12	
Sa(0.5)	0.06	
Sa(1.0)	0.02	
Sa(2.0)	0.01	
PGA	0.06	
Soil Class	D	
Importance Factor, IE	1.5	
Structures :		Conventional construction of moment frames, braced frames or shear walls (ABC Table 4.1.8.9)
Rd = 1.5		
R0 = 1.3		

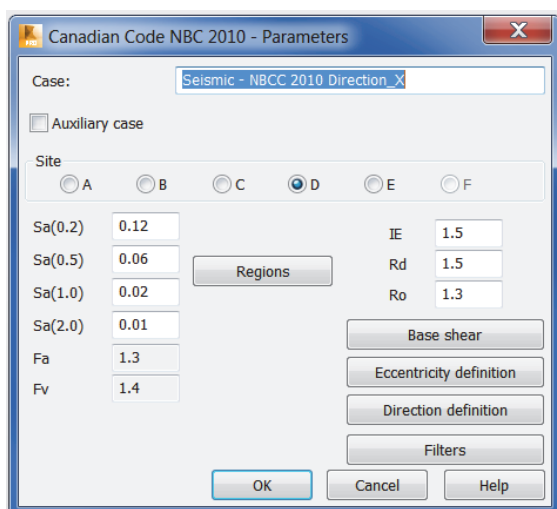


Figure 2-3 Seismic input in Autodesk Robot

In Autodesk Robot the 3 load cases for the 3 directions X, Y and Z are automatically generated.

Please note that load case 8 is a modal load case prerequisite for input of the seismic data and generation of the 3 load cases.

## 2.3 Results

The following section presents the results of the structural calculation. The profiles will be checked according to CSA S16-09 to the ULS cases determining overall ratio. SLS cases are evaluated to determine the deflection ratios, depending on beam or column designation to limits specified in §1.9.1. Stress and deformation will be displayed to show the behavior of the structure.

### 2.3.1 Unity Checks

CAN/CSA S16-09 - Member Verification ( SLS ; ULS ) 2to17 21 23to27 35to71 77to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196

Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)	Ratio(vx)	Case (vx)	Ratio(vy)	Case (vy)
87 dJC Beam 87	UNP 100	S 355	104.96	278.49	0.93	12 ULS /101/	0.02	15 SLS /26/	0.50	15 SLS /29/	-	-	-	-
21 dJC Beam 21	UNP 100	S 355	104.96	278.49	0.92	12 ULS /95/	0.02	15 SLS /26/	0.43	15 SLS /27/	-	-	-	-
2 Beam 2	HEA 240	S 355	131.79	220.67	0.73	12 ULS /45/	0.00	15 SLS /1/	0.00	15 SLS /1/	-	-	-	-
4 Beam 4	HEA 240	S 355	131.79	220.67	0.71	12 ULS /45/	0.00	15 SLS /1/	0.00	15 SLS /1/	-	-	-	-
85 dJC Beam 85	UNP 100	S 355	104.96	278.49	0.58	12 ULS /101/	0.00	15 SLS /26/	0.79	15 SLS /29/	-	-	-	-
25 dJC Beam 25	U 100x50x5	S 235	105.58	266.45	0.55	12 ULS /97/	0.01	15 SLS /31/	0.57	15 SLS /29/	-	-	-	-
24 dJC Beam 24	U 100x50x5	S 235	105.58	266.45	0.51	12 ULS /99/	0.00	15 SLS /26/	0.66	15 SLS /29/	-	-	-	-
26 dJC Beam 26	U 100x50x5	S 235	105.58	266.45	0.48	12 ULS /95/	0.00	15 SLS /25/	0.64	15 SLS /29/	-	-	-	-
82 dJC Beam 82	UNP 100	S 355	104.96	278.49	0.48	12 ULS /97/	0.00	15 SLS /31/	0.78	15 SLS /29/	-	-	-	-
84 dJC Beam 84	UNP 100	S 355	104.96	278.49	0.47	12 ULS /97/	0.00	15 SLS /27/	0.77	15 SLS /29/	-	-	-	-
83 dJC Beam 83	UNP 100	S 355	104.96	278.49	0.46	12 ULS /77/	0.00	15 SLS /31/	0.76	15 SLS /29/	-	-	-	-
79 dJC Beam 79	UNP 100	S 355	104.96	278.49	0.44	12 ULS /97/	0.00	15 SLS /25/	0.69	15 SLS /29/	-	-	-	-
27 dJC Beam 27	U 100x50x5	S 235	105.58	266.45	0.44	12 ULS /99/	0.01	15 SLS /26/	0.57	15 SLS /29/	-	-	-	-
80 dJC Beam 80	UNP 100	S 355	104.96	278.49	0.40	12 ULS /97/	0.00	15 SLS /26/	0.69	15 SLS /29/	-	-	-	-

Figure 2-4 Unity Checks for top utilized profiles (>40%), sorted on overall ratio, high to low

As can be seen the highest utilized members are 87 and 21. These are UNP100 beams in the roof near the edges (marked orange in figure below). For the heaviest loaded beam, 93% of its capacity is used and therefore suffices to the structural verification according to CSA S16-09.

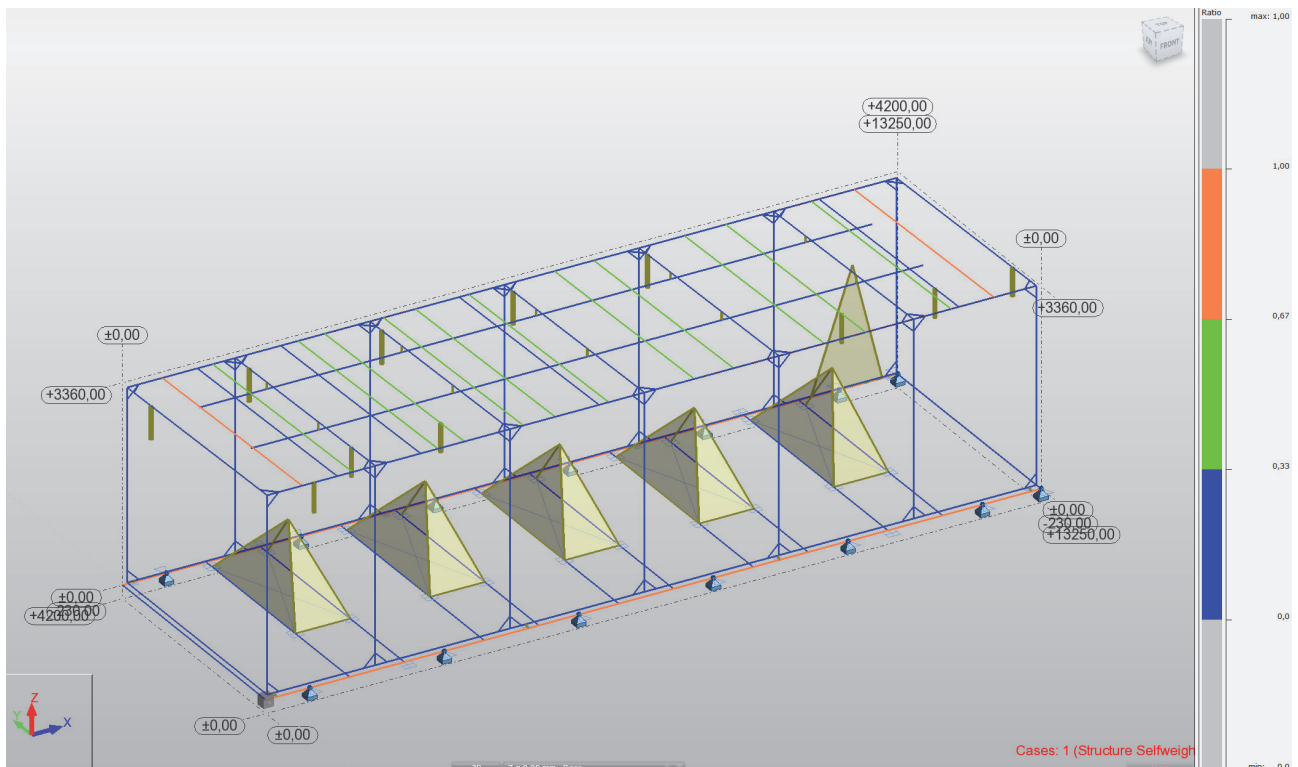


Figure 2-5 Visual presentation of unity checks (blue 0-33%; green 34-67%; orange 68-100%)

### 2.3.2 Stress

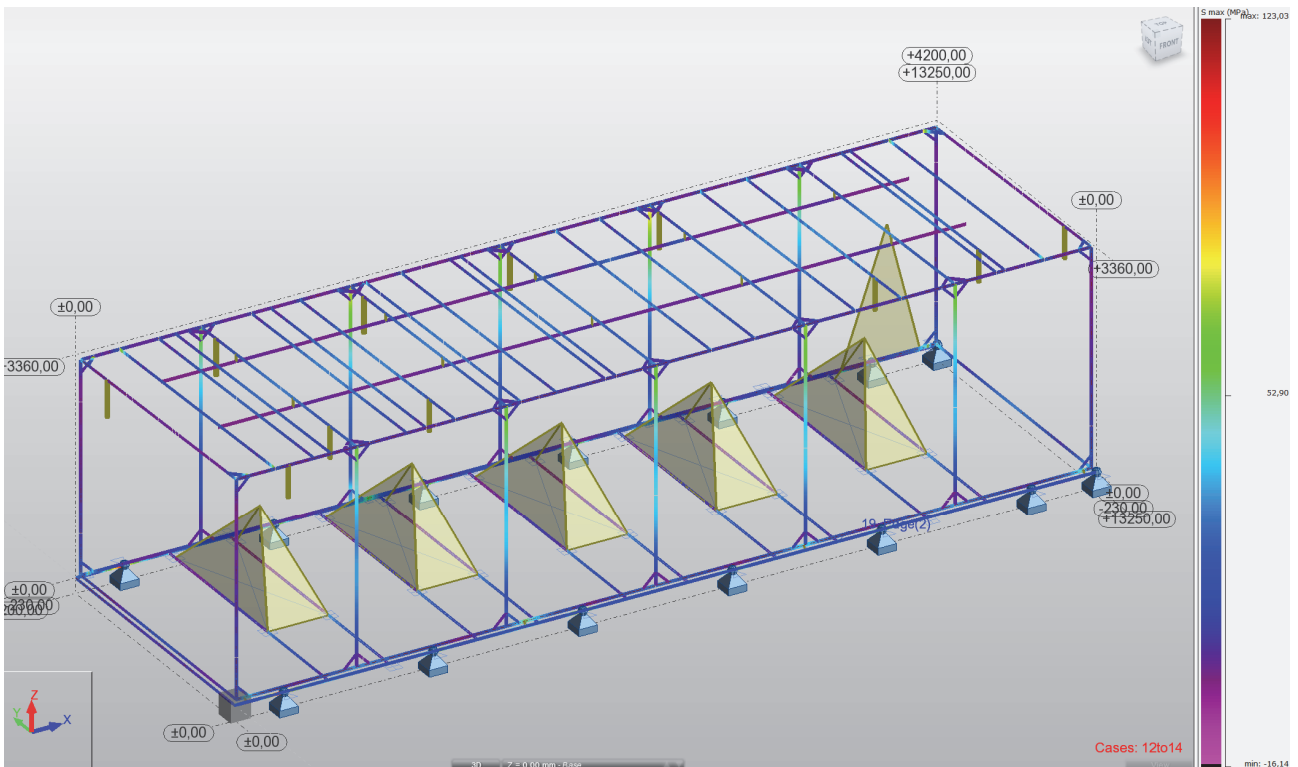


Figure 2-6 Stress peaks in profiles

As can be seen the highest stress peak is 124 MPa in the ULS load cases. This is within limits:  $\max 124 < 355$  MPa.

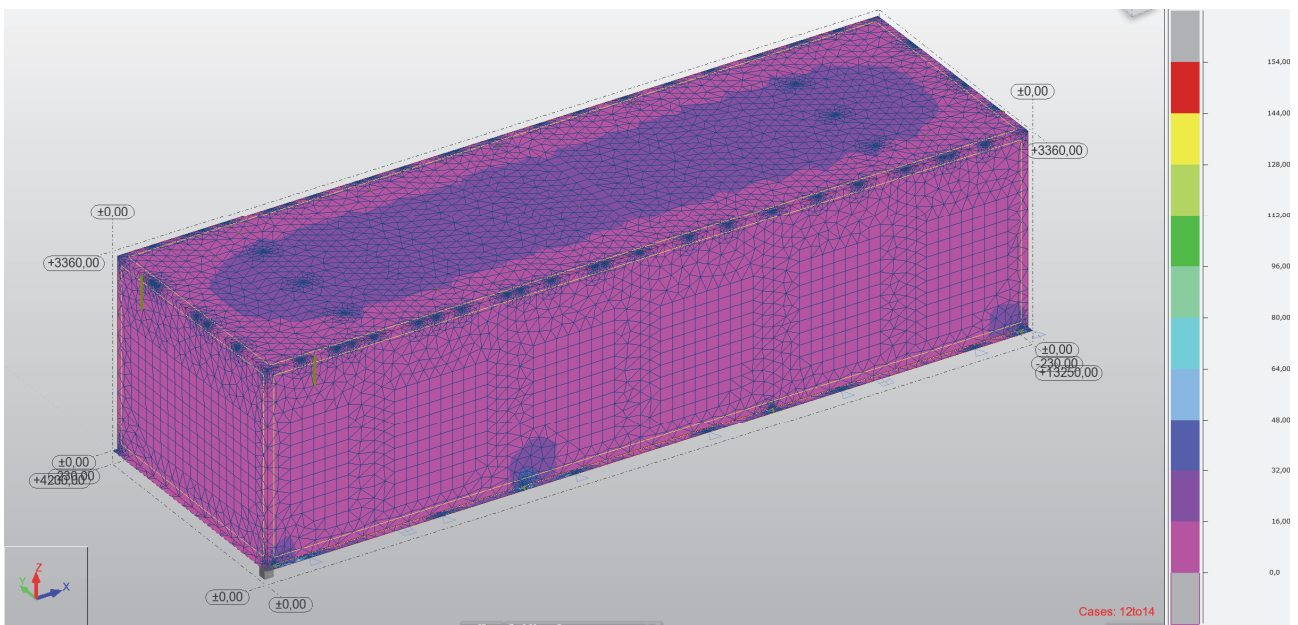


Figure 2-7 Stress in panels

As can be seen global stress values are  $\max 48$  MPa  $<$  limit of 140 MPa.

### 2.3.3 Deformation

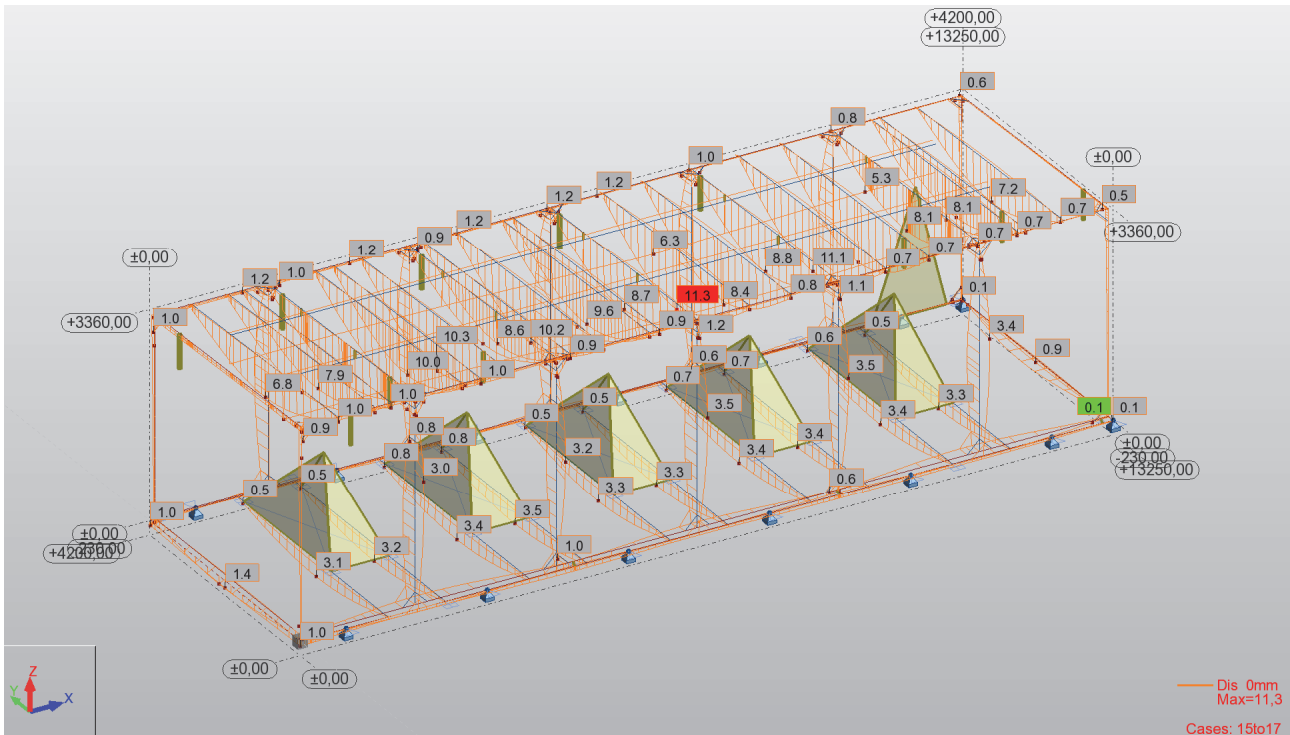


Figure 2-8 Deformation of profiles

As can be seen the largest deformation is about 11,3 mm in the roof in the SLS cases.  
 This is within limits:  $(4200/11,3=) 1/371 < 1/300$ .



### 3 Detail Analysis – Operational - D1 OPE

Verification of the bolted connection to existing support structure.

#### 3.1 Reactions

Below the highest and lowest ULS reaction values from model A1 OPE in the constraints.

The x and y values are combined for the maximum shear force and negative z values represent a tension force. Positive values are compressive and do not affect the bolted connections.

Table 3-1 Max/Min ULS Reactions from A1 OPE

Node/Case	FX(N)	FY(N)	FZ(N)	Shear	Tension	
71/ULS+	10 957	43 114	40 509	44 484	-	
71/ULS-	-1 279	-13 131	1 063	13 193	-	
72/ULS+	5 670	230	48 428	5 674	-	
72/ULS-	-2 972	-57 077	-18 934	57 154	18 934	
1000/ULS+	60 496	-16 152	82 834	62 615	-	
1000/ULS-	10 520	-83 385	-2 711	84 046	2 711	
1001/ULS+	16 615	-12 401	57 149	20 732	-	
1001/ULS-	-78 612	-66 617	9 804	103 042	-	
1002/ULS+	56 504	-13 767	75 262	58 157	-	
1002/ULS-	3 013	-81 283	7 995	81 339	-	
1003/ULS+	2 736	-12 999	57 882	13 284	-	
1003/ULS-	-43 459	-68 199	9 590	80 869	-	
1004/ULS+	21 180	-13 761	63 422	25 258	-	
1004/ULS-	-20 727	-73 944	10 222	76 794	-	
1005/ULS+	7 139	-8 445	36 214	11 058	-	
1005/ULS-	-20 184	-43 487	1 677	47 943	-	
1006/ULS+	69 921	81 018	82 409	107 018	-	
1006/ULS-	-3 409	3 072	14 333	4 589	-	
1007/ULS+	-2 386	66 593	61 621	66 636	-	
1007/ULS-	-69 208	2 521	12 144	69 254	-	
1008/ULS+	48 445	81 622	79 899	94 916	-	
1008/ULS-	-2 180	10 561	13 194	10 784	-	
1009/ULS+	2 048	69 032	65 455	69 063	-	
1009/ULS-	-44 346	8 249	12 028	45 106	-	
1010/ULS+	17 434	69 865	67 155	72 007	-	
1010/ULS-	-10 781	9 105	11 712	14 111	-	
1011/ULS+	6 535	59 935	56 261	60 290	-	
1011/ULS-	-19 589	11 810	14 846	22 874	-	
			MAX (N)	107 018	18 934	N
			MAX (kN)	<b>107,0</b>	<b>18,9</b>	<b>kN</b>

#### 3.2 Results

The used bolted connections will be according ASTM A325. The size on drawing (36026-320-06-004-R00 GA Boiler platform) is ¾" UNC (~M20).

ASTM A325 ¾" UNC bolt ( $f_u = 120$  ksi) ( $f_u \approx 825$  MPa);  $A_s = 0,334$  in<sup>2</sup> <sup>6</sup>

$$F_{n,tension} = 90 \text{ ksi}^7$$

$$F_{n, shear} = 48 \text{ ksi}^7$$

$$F_{v,Rd} = 30\,060 \text{ lbf} \approx 134 \text{ kN} \quad (107 / 134 = 80\%)$$

$$F_{t,Rd} = 40\,100 \text{ lbf} \approx 178 \text{ kN} \quad (18,9 / 178 = 11\%)$$

In comparison: an ISO 4014 or 4017 bolt M20 8.8 bolt ( $f_u = 800$  MPa;  $f_y = 640$  MPa)

$$F_{t,Rd} = 141,0 \text{ kN}$$

$$F_{v,Rd} = 121,0 \text{ kN}$$

This shows that ASTM A325 ¾" bolts will suffice.

<sup>6</sup> According ANSI / ASTM A 325 - 79

<sup>7</sup> According 2004 RCSC Specification for Structural Joints Using ASTM A325 or A490 Bolts Table 5.1



## 4 Detail Analysis – Operational - D2 OPE

Bolted Connection between enclosure skid and dropover enclosure

### 4.1 Reactions

Below the highest and lowest ULS reaction values from model A1 OPE in the constraints.

The x and y values are combined for the maximum shear force and negative z values represent a tension force. Positive values are compressive and do not affect the bolted connections.

Table 4-1 Max/Min ULS Reactions from A1 OPE

Node/Case	FIX (N)	FIY (N)	FIZ (N)	Shear	Tension	
121-129/ULS+	16 296	21 556	-2 021	27 022	2 021	
121-129/ULS-	-7 034	-602	-47 717	7 060	47 717	
122-130/ULS+	2 010	6 282	2 659	6 595	-	
122-130/ULS-	-8 385	-288	-42 399	8 390	42 399	
123-131/ULS+	9 467	6 453	-1 211	11 457	1 211	
123-131/ULS-	-8 474	-353	-56 447	8 482	56 447	
124-132/ULS+	12 857	16 894	-5 073	21 230	5 073	
124-132/ULS-	-8 321	-8 075	-44 275	11 595	44 275	
133-125/ULS+	6 414	13 565	51 985	15 005	-	
133-125/ULS-	-16 709	-23 801	-25 359	29 080	25 359	
134-126/ULS+	7 505	2 671	38 599	7 966	-	
134-126/ULS-	1 268	-9 790	-3 677	9 872	3 677	
135-127/ULS+	15 664	2 401	58 584	15 847	-	
135-127/ULS-	3 501	-9 735	-3 142	10 345	3 142	
136-128/ULS+	10 103	4 903	46 071	11 230	-	
136-128/ULS-	-3 111	-18 767	-7 818	19 023	7 818	
				29 080	56 447	N
				<b>29,1</b>	<b>56,4</b>	<b>kN</b>

### 4.2 Results

The used bolted connections will be metric and bearing according ISO 15048. The used bolts will be ISO 4017 full thread, class 8.8.

Bolt M16 8.8 bolt ( $f_u = 800$  MPa;  $f_y = 640$  MPa)

$F_{t,Rd} = 90,4$  kN (56,4 / 90,4 = 63%)

$F_{v,Rd} = 77,1$  kN (29,1 / 77,1 = 38%)

This shows that ISO 4017 M16 8.8 bolts will suffice.

For practical sizing, M20 will be used in the production model.



## 5 Structural Analysis – Lifting - A2 LIFT

The complete assembly of enclosure skid and dropover enclosure must be able to withstand the lifting forces. This chapter considers the structural verification of the global structure when lifted.

### 5.1 FEA model

The model of A1 OPE is copied and all load cases deleted except load case 1: selfweight. In this load case an extra distributed load is applied to the floor face area to reach a total of 30 000 kg. This equals the 30 t that is used to determine the padeye dimensions.

The calculation model currently weighs in at 25 293 kg.

The set will be lifted from the enclosure skid with a spreader beam as seen below.

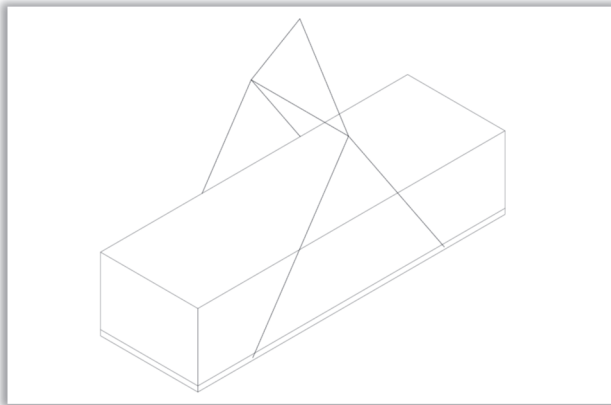


Figure 5-1 Lifting set up with spreader beam

The constraints of A1 OPE are deleted as these fasteners do not apply. New constraints are placed at the lifting points. The image below shows these constraints, recognizable by the support codes indicating the degrees of freedom.

To comply with the degrees of freedom of the lifting setup, the two lifting points on the left side are fixed in X, Y and Z direction and the lifting points on the right side are free to translate in X direction.

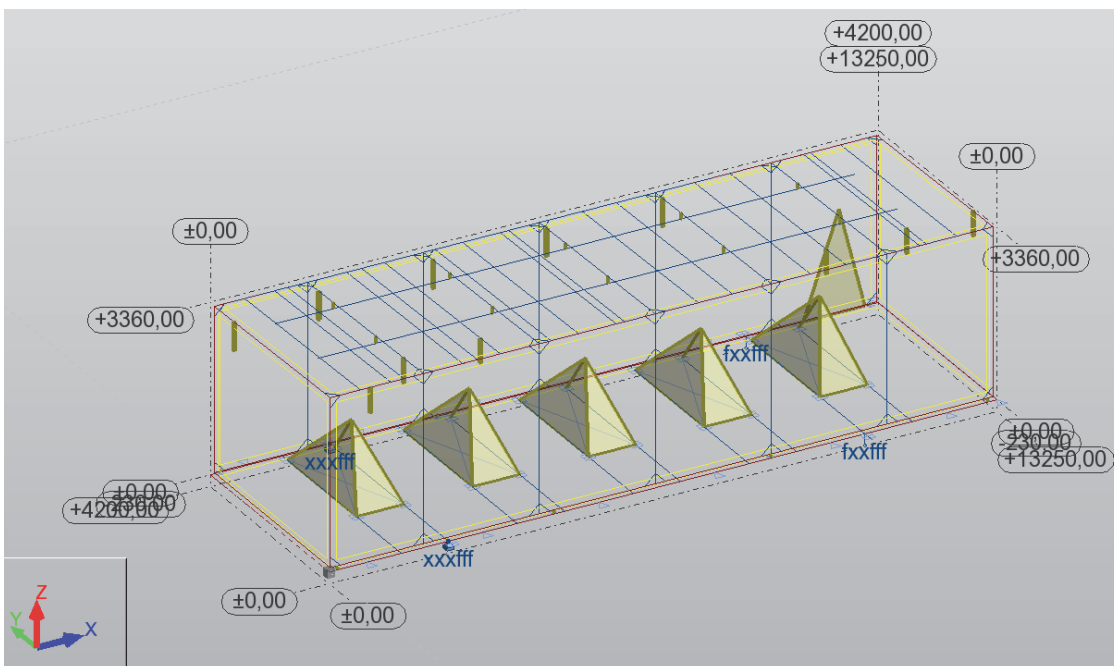


Figure 5-2 FEA model with constraints (x=fixed; f=free)

## 5.2 Results

Below the results of the structural calculation. The profiles will be checked according CSA S16-09. Stress and deformation will be displayed to show the behavior of the structure.

### 5.2.1 Unity Checks

CAN/CSA S16-09 - Member Verification (SLS; ULS) 2to17 20to27 35to50 52to71 77to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196										
Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)
4 Beam 4	HEA 240	S 355	131.79	220.67	0.85	1 Structure Selfweight	0.01	1 Structure Selfweight	0.07	1 Structure Selfweight
2 Beam 2	HEA 240	S 355	131.79	220.67	0.70	1 Structure Selfweight	0.00	1 Structure Selfweight	0.06	1 Structure Selfweight
8 dJC Bm Crn 8	IPE 140	S 355	200.41	695.65	0.13	1 Structure Selfweight	0.00	1 Structure Selfweight	0.01	1 Structure Selfweight
17 Beam 17	HEA 180	S 355	56.42	92.95	0.12	1 Structure Selfweight	0.00	1 Structure Selfweight	0.13	1 Structure Selfweight
6 Beam 6	HEA 180	S 355	56.42	92.95	0.11	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight
16 Beam 16	HEA 180	S 355	56.42	92.95	0.10	1 Structure Selfweight	0.00	1 Structure Selfweight	0.13	1 Structure Selfweight
7 Beam 7	HEA 180	S 355	56.42	92.95	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
85 dJC Beam 85	UNP 100	S 355	104.96	278.49	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
79 dJC Beam 79	UNP 100	S 355	104.96	278.49	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight

Figure 5-3 Unity Checks for top utilized profiles (>8%), sorted on overall ratio high to low

As can be seen the highest utilized members are the long beams HEA 240 4 and 2. 85% / 70% of its capacity is used and therefore suffices to the structural verification according CSA S16-09.

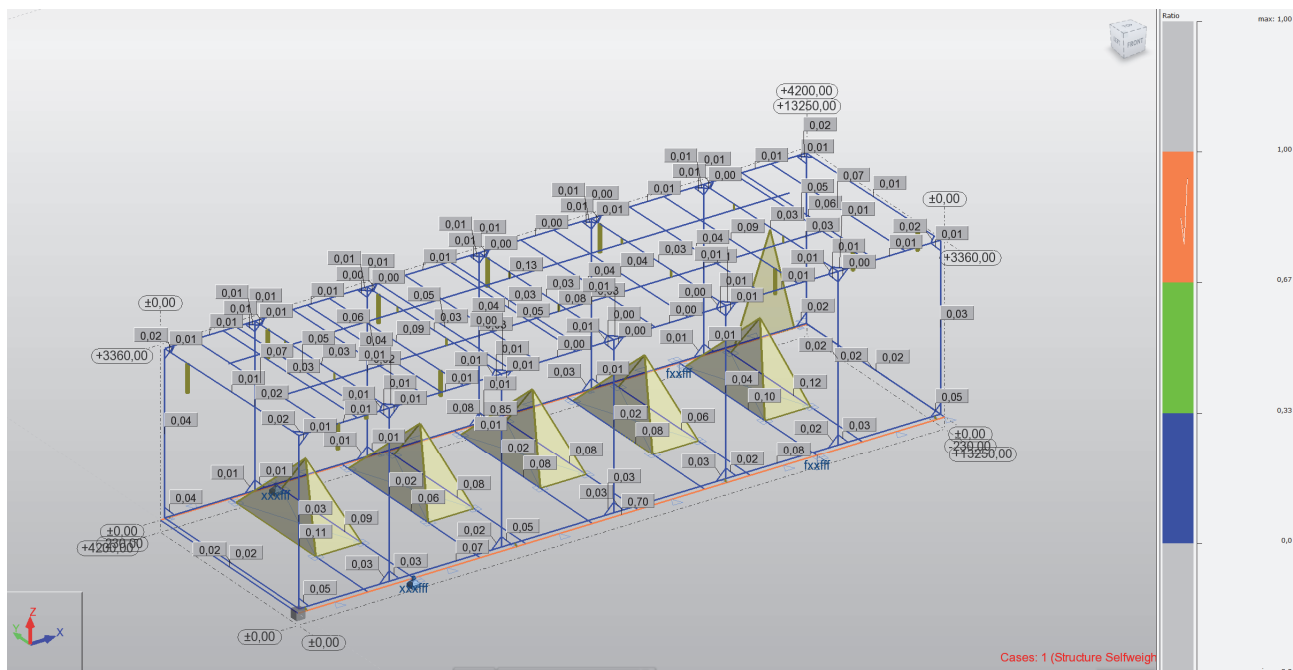


Figure 5-4 Visual presentation of unity checks (blue 0-33%; green 34-67%; orange 68-100%)

## 5.2.2 Stress

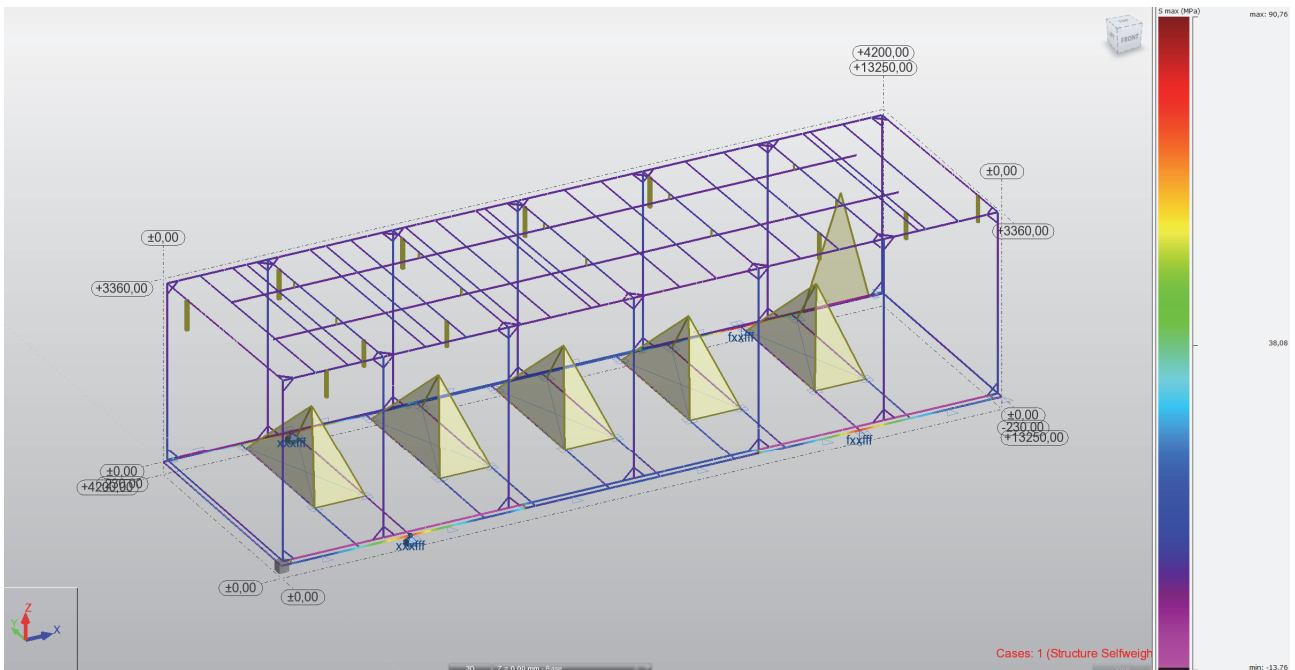


Figure 5-5 Stress peaks in profiles

As can be seen the highest stress peak is 91 MPa.  
This is within limits:  $\max 91 < 355$  MPa.

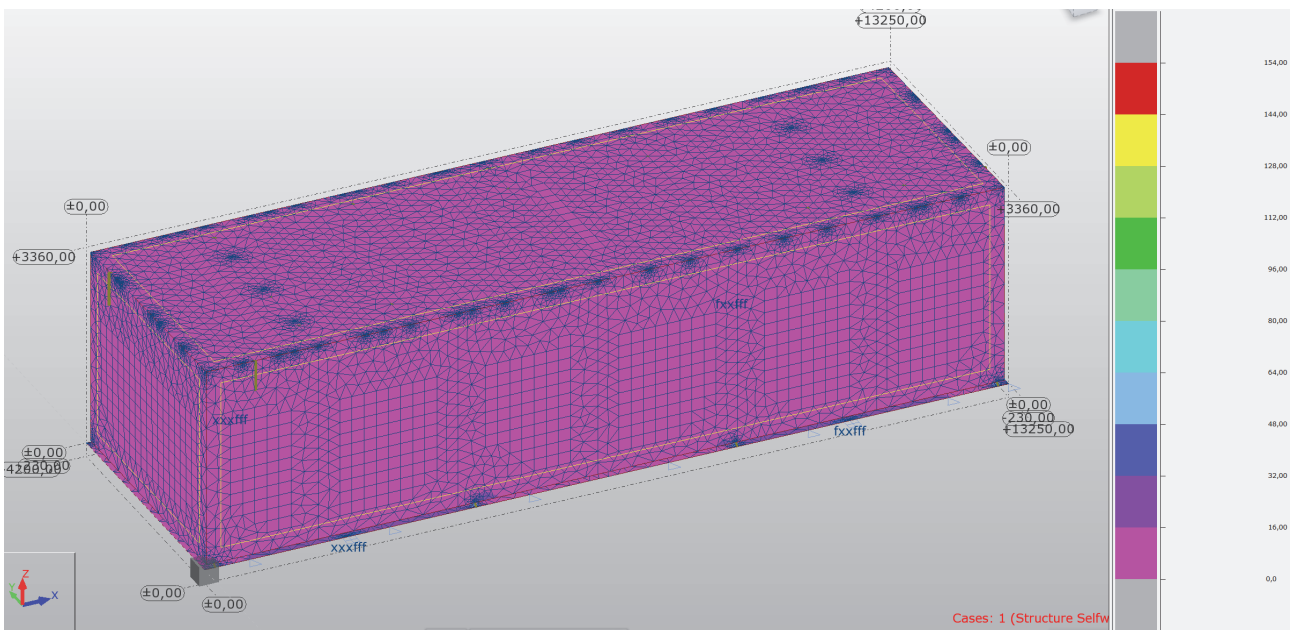


Figure 5-6 Stress in panels

As can be seen global stress values are  $\max 32$  MPa  $<$  limit of 140 MPa.

### 5.2.3 Deformation

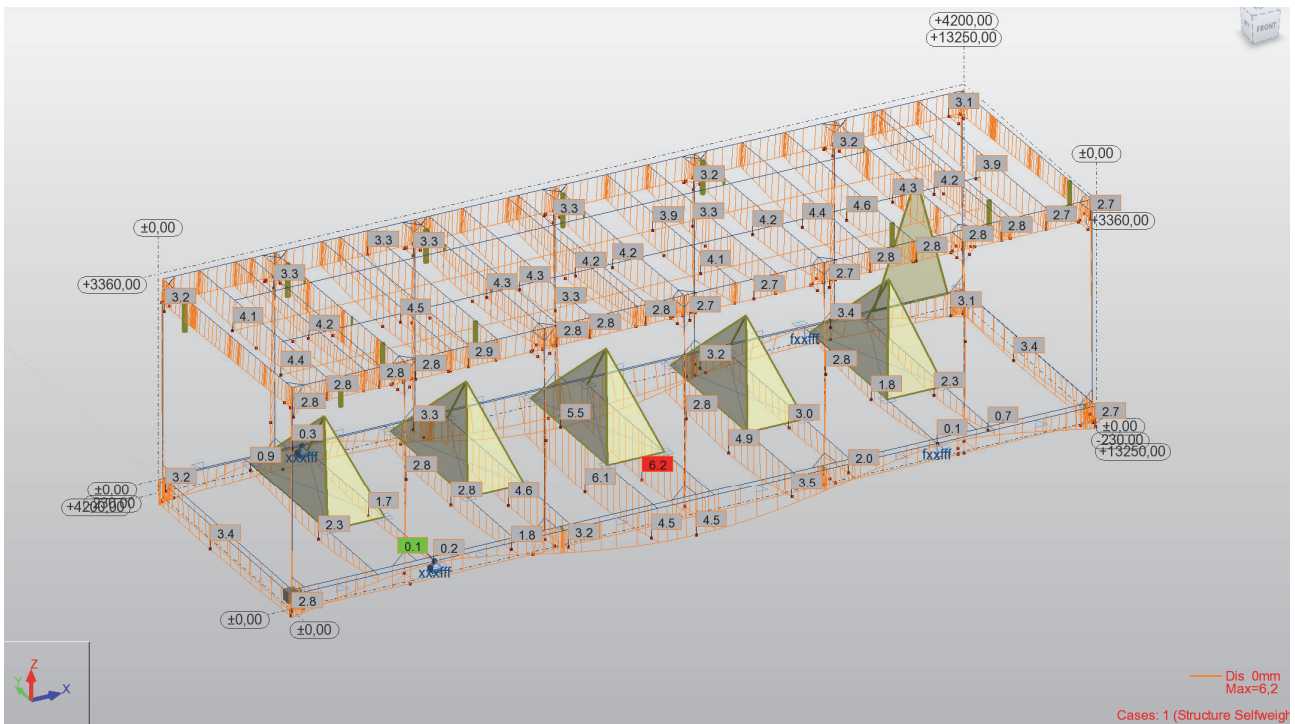


Figure 5-7 Deformation of profiles

As can be seen the largest deformation is about 6,2 mm in the floor.  
 This is within limits:  $(4200/6,2=) 1/677 < 1/300$ .



## **6 Detail Analysis – Lifting - D3 LIFT**

Design of Primary Lifting Eye for lifting a full set comprising enclosure skid and enclosure fully loaded.

Based on EN 1993-1-8 and DEP 34.00.01.30-Gen an excel sheet is used to determine the required shackle which determines the padeye dimensions.

To give the design some margin, the max weight is regarded as 30 000 kg or 30 metric tons. The current design is 25 293 kg.

The selected shackle is a Greenpin shackle with an MBL equal to 6xWLL, which complies with §4 of the TR 0875-SP020:

“Safety factor 5 shall be used for lifting lugs, relative to the minimum break load.”

DEP 34.00.01.30-Gen §3.15 determines a lift load increase due to manufacturing tolerances of **10%**

DEP 34.00.01.30-Gen §2.3.2.a determines an impact factor **1,3** for the shackle.

DEP 34.00.01.30-Gen §2.3.2.a determines an impact factor **2,0** for the lug.

This results in a sling force for the shackle of 162 kN.

This results in a sling force for the lug of 250 kN.

### **6.1 Shackle**

Please see Appendix C for the calculation sheet showing the shackle size.

### **6.2 Padeye**

Please see Appendix C for the calculation sheet showing the padeye dimensions.

These are incorporated in the production model and drawings.

### **6.3 Bolted Connection**

As the padeye requires to be detachable for transport bolted connections are used.

The 4 bolts per padeye are sheared due to the use of a spreader beam.

The used bolted connections will be metric and bearing according ISO 15048. The used bolts will be ISO 4017 full thread, class 8.8.

Bolt M16 8.8 bolt ( $f_u = 800$  MPa;  $f_y = 640$  MPa)

$F_{v,Rd} = 77,1$  kN ( $62,5 / 77,1 = 81\%$ )

This shows that ISO 4017 M16 8.8 bolts will suffice.

For practical sizing, M20 will be used in the production model.

## 7 Structural Analysis – Deformation - A3 DEF

According Technical Requisition 08750SP020-R01 the enclosure skids + enclosure sets “will be supported in the field by a platform with maximum deflection, being length/300 mm. Supplier to confirm that skid enclosure is stiff enough of deal with bending of the support platform”

The deformation of the structure will be compared to this limit.

### 7.1 FEA model

In reality the skid and enclosure set is stiffer than the support platform. It will therefore locally increase the stiffness of the platform. To compare the stiffness of the skid and enclosure to the requested platform deflection the following situation is considered.

The model of A1 OPE is copied and all load cases deleted except load case 1: selfweight. The calculation model currently weighs in at 25 293 kg.

The 14 bolted connections / modeled constraints, as in the OPE model, are assumed loose. The platform will deflect with max  $L/300$ . The stiffer skid and enclosure set has to prove to deform less, so the inner constraints will lose contact with the support platform and are not applicable for this analysis. The 4 outer constraints will remain in contact with the support platform.

The image below shows these constraints, recognizable by the support codes indicating the degrees of freedom. To comply with the setup, the two constraints on the left side are fixed in X, Y and Z direction and the constraints on the right side are free to translate in X direction.

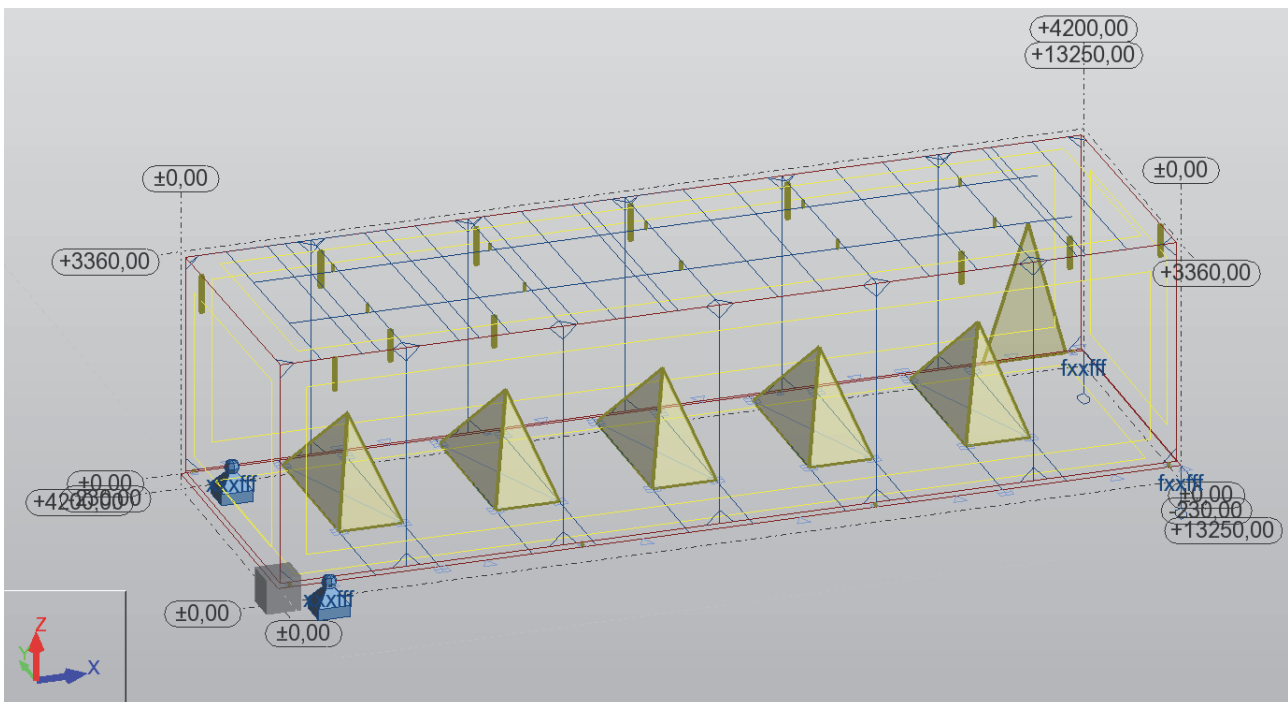


Figure 7-1 FEA model with constraints

## 7.2 Results

Below the results of the structural calculation. The profiles will be checked according CSA S16-09. Stress and deformation will be displayed to show the behavior of the structure.

### 7.2.1 Unity Checks

CAN/CSA S16-09 - Member Verification ( SLS ; ULS ) 2to17 21 23to27 35to71 77to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196

Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)
4 Beam 4	HEA 240	S 355	131.79	220.67	0.52	1 Structure Selfweight	0.01	1 Structure Selfweight	0.03	1 Structure Selfweight
8 dJC Bm Crn 8	IPE 140	S 355	200.41	695.65	0.49	1 Structure Selfweight	0.00	1 Structure Selfweight	0.04	1 Structure Selfweight
2 Beam 2	HEA 240	S 355	131.79	220.67	0.48	1 Structure Selfweight	0.01	1 Structure Selfweight	0.03	1 Structure Selfweight
11 dJC Bm Crn 11	IPE 140	S 355	200.41	695.65	0.29	1 Structure Selfweight	0.00	1 Structure Selfweight	0.03	1 Structure Selfweight
114 dJC Beam 114	RECT 120x10	S 355	8.16	97.98	0.17	1 Structure Selfweight	0.03	1 Structure Selfweight	0.01	1 Structure Selfweight
102 dJC Beam 102	RECT 120x10	S 355	8.16	97.98	0.13	1 Structure Selfweight	0.02	1 Structure Selfweight	0.01	1 Structure Selfweight
100 dJC Beam 100	RECT 120x10	S 355	8.16	97.98	0.11	1 Structure Selfweight	0.00	1 Structure Selfweight	0.01	1 Structure Selfweight

Figure 7-2 Unity Checks for top utilized profiles (>10%), sorted on overall ratio high to low

As can be seen the highest utilized members are the long beams HEA 240 4 and 2. 52% / 48% of its capacity is used and therefore suffices to the structural verification according CSA S16-09.

### 7.2.2 Stress

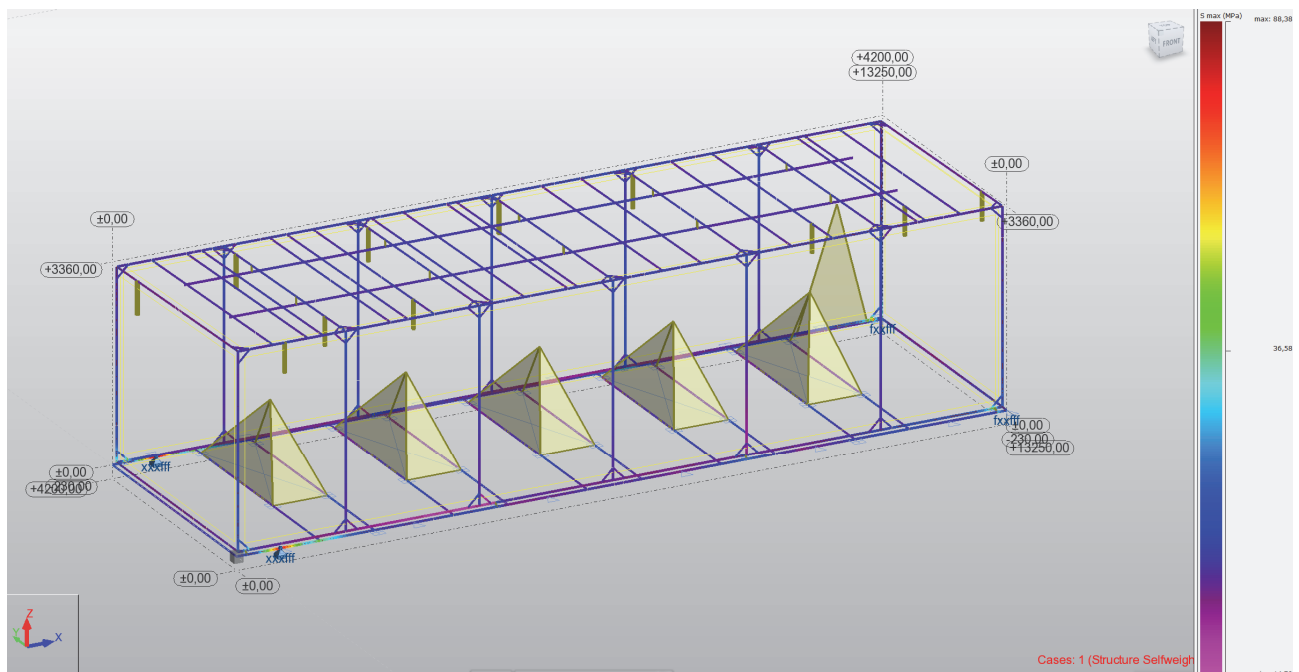


Figure 7-3 Stress peaks in profiles

As can be seen the highest stress peak is 89 MPa. This is within limits:  $\max 89 < 355 \text{ MPa}$ .



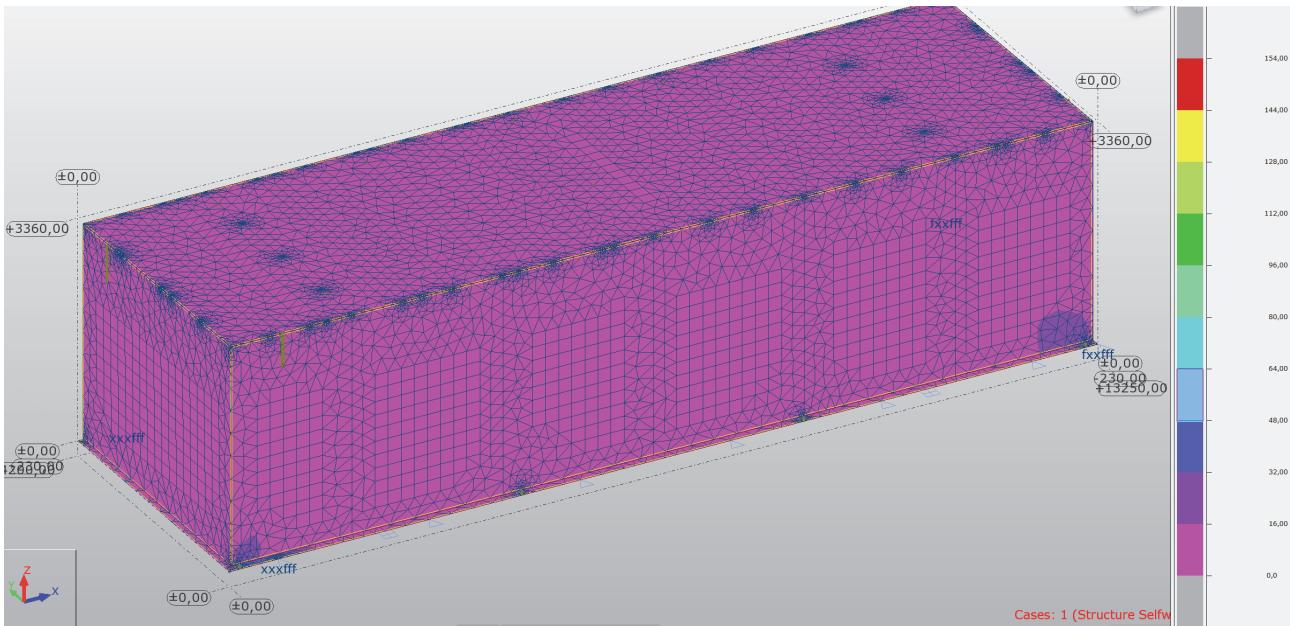


Figure 7-4 Stress in panels

As can be seen global stress values are max 32 MPa < limit of 140 MPa.

### 7.2.3 Deformation

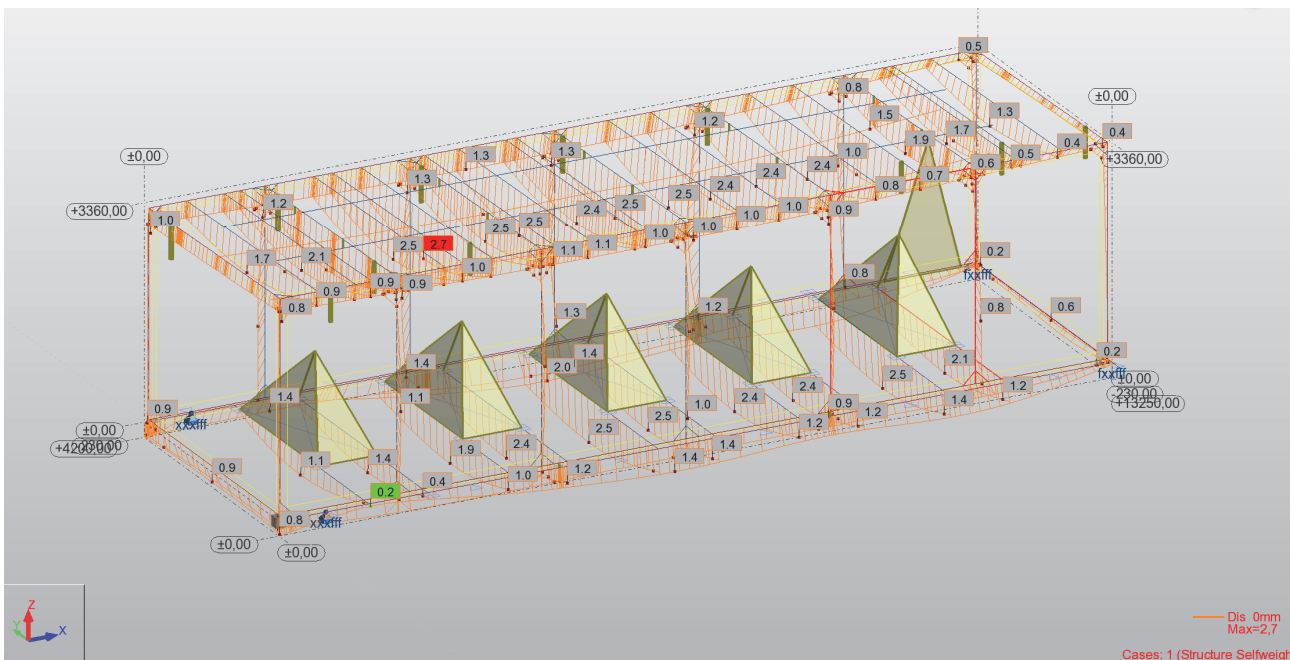


Figure 7-5 Deformation of profiles

As can be seen the largest deformation is 2,7 mm in the roof.  
This is within limits:  $(4200/2,7) = 1/1556 < 1/300$ .

Considering the largest span between the outer constraints  $L=12\ 500$  mm, the max deformation is 1,4 mm. This is  $(12\ 500 / 1,4) = 1/8928$ .

$L/300$  for this span would result in a deflection of 41,7 mm.

This shows the enclosure skid + drover enclosure set has a higher stiffness than the support platform.



## 8 Structural Analysis – Lifting - B LIFT

The enclosure skid must be able to resist the occurring forces during lifting while carrying the burner skids and other applicable equipment.

### 8.1 FEA model

The model of A1 OPE is copied and all load cases deleted except load case 1: selfweight.

The calculation model currently weighs in at 14 500 kg (7458 kg enclosure skid + 7042 kg de Jong Combustion equipment).

An extra load is applied to reach a total weight of 20 000 kg, having a total of max 30 t in mind and a drolover enclosure of 10 t.

The constraints are placed at the lifting points. The image below shows these constraints, recognizable by the support codes indicating the degrees of freedom.

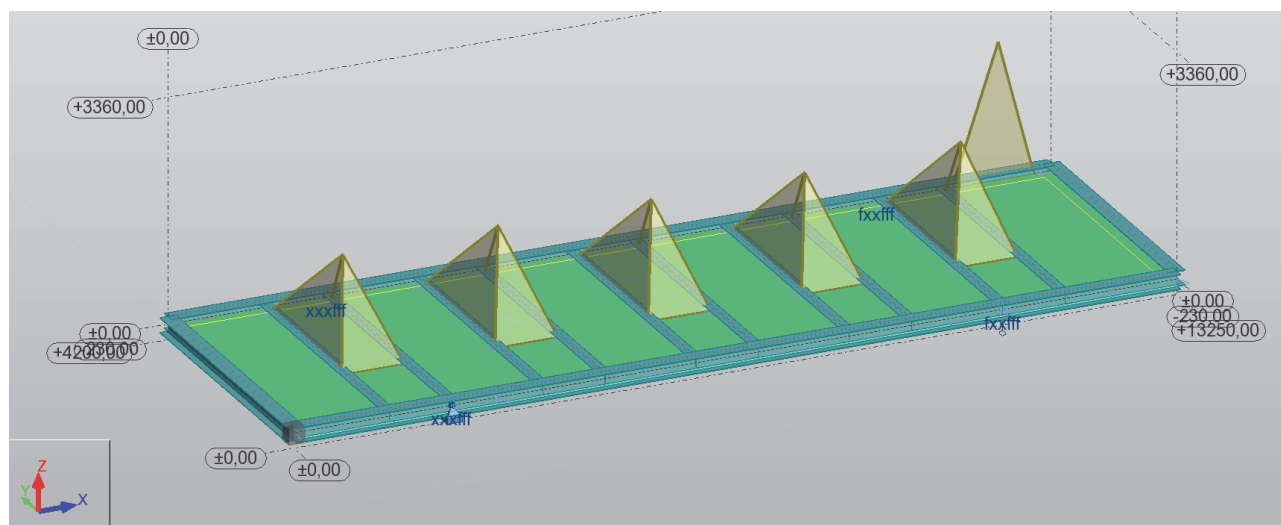


Figure 8-1 FEA model with constraints

To comply with the lifting setup, the two lifting points on the left side are fixed in X, Y and Z direction and the lifting points on the right side are free to translate in X direction.

### 8.2 Results

Below the results of the structural calculation. The profiles will be checked according CSA S16-09. Stress and deformation will be displayed to show the behavior of the structure.

#### 8.2.1 Unity Checks

CAN/CSA S16-09 - Member Verification ( SLS ; ULS ) 2to7 9 10 12to17

Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)
2 Beam 2	HEA 240	S 355	131.79	220.67	0.27	1 Structure Selfweight	0.00	1 Structure Selfweight	0.34	1 Structure Selfweight
3 Beam 3	HEA 240	S 355	41.77	69.95	0.02	1 Structure Selfweight	0.00	1 Structure Selfweight	0.03	1 Structure Selfweight
4 Beam 4	HEA 240	S 355	131.79	220.67	0.39	1 Structure Selfweight	0.00	1 Structure Selfweight	0.38	1 Structure Selfweight
5 Beam 5	HEA 240	S 355	41.77	69.95	0.02	1 Structure Selfweight	0.00	1 Structure Selfweight	0.02	1 Structure Selfweight
6 Beam 6	HEA 180	S 355	56.42	92.95	0.08	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
7 Beam 7	HEA 180	S 355	56.42	92.95	0.10	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
9 Beam 9	HEA 180	S 355	56.42	92.95	0.07	1 Structure Selfweight	0.00	1 Structure Selfweight	0.09	1 Structure Selfweight
10 Beam 10	HEA 180	S 355	56.42	92.95	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
12 Beam 12	HEA 180	S 355	56.42	92.95	0.08	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
13 Beam 13	HEA 180	S 355	56.42	92.95	0.08	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
14 Beam 14	HEA 180	S 355	56.42	92.95	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
15 Beam 15	HEA 180	S 355	56.42	92.95	0.07	1 Structure Selfweight	0.00	1 Structure Selfweight	0.09	1 Structure Selfweight
16 Beam 16	HEA 180	S 355	56.42	92.95	0.10	1 Structure Selfweight	0.00	1 Structure Selfweight	0.13	1 Structure Selfweight
17 Beam 17	HEA 180	S 355	56.42	92.95	0.10	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight

Figure 8-2 Unity Checks for all profiles

As can be seen the highest utilized members are the long beams HEA 240 4 and 2. 39% / 27% of its capacity is used and therefore suffices to the structural verification according CSA S16-09.

### 8.2.2 Stress

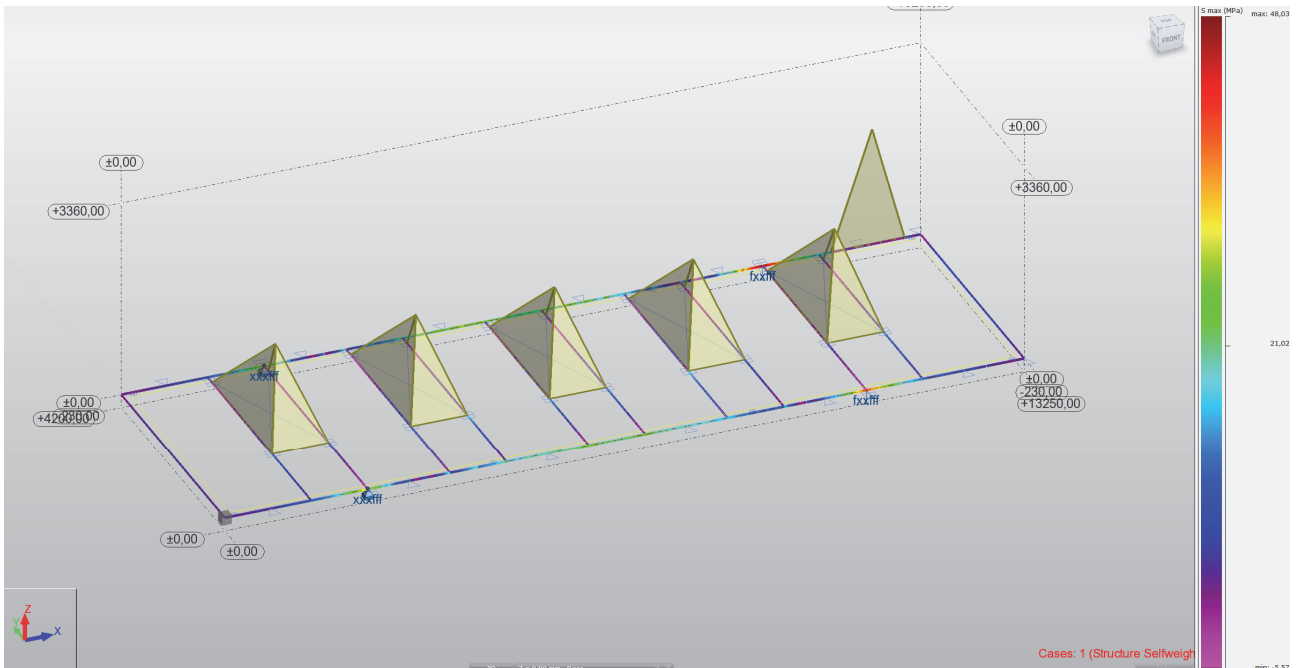


Figure 8-3 Stress peaks in profiles

As can be seen the highest stress peak is 48 MPa. This is within limits:  $\max 48 < 355 \text{ MPa}$ .

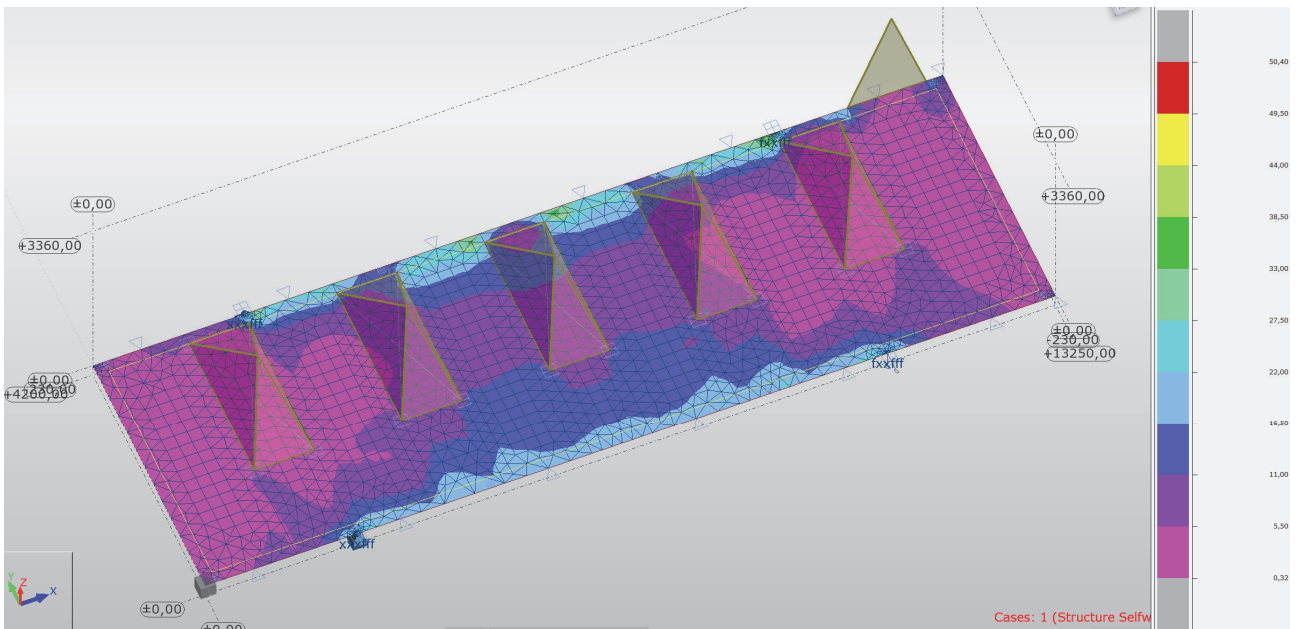


Figure 8-4 Stress in panels

As can be seen global stress values are  $\max 33 \text{ MPa} < \text{limit of } 235 \text{ MPa}$ .

### 8.2.3 Deformation

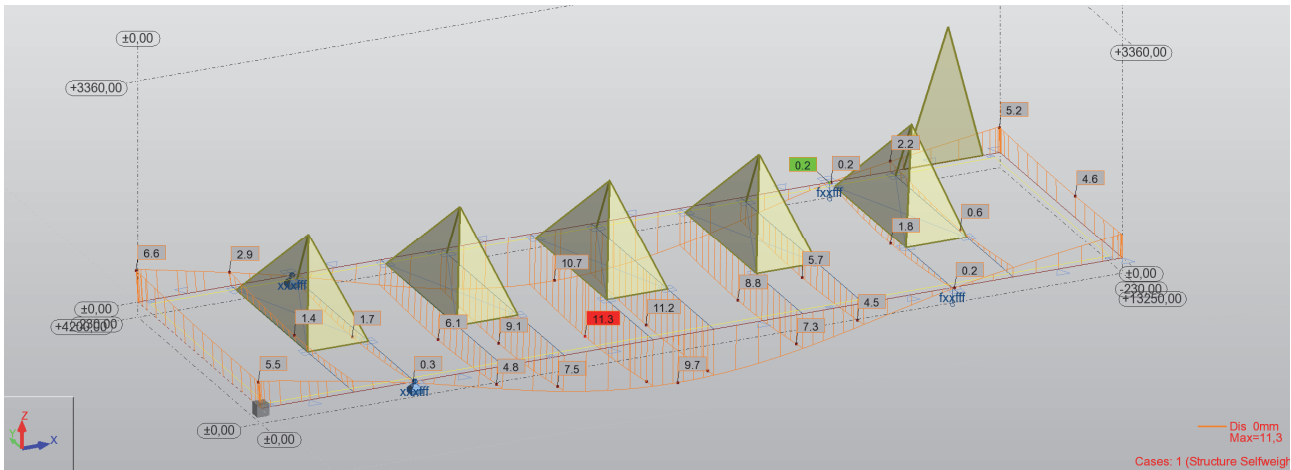


Figure 8-5 Deformation of profiles

As can be seen the largest deformation is 11,3 mm in the floor.  
 This is within limits:  $(8264/11,3=) 1/731 < 1/300$ .

## 9 Structural Analysis – Lifting - C LIFT

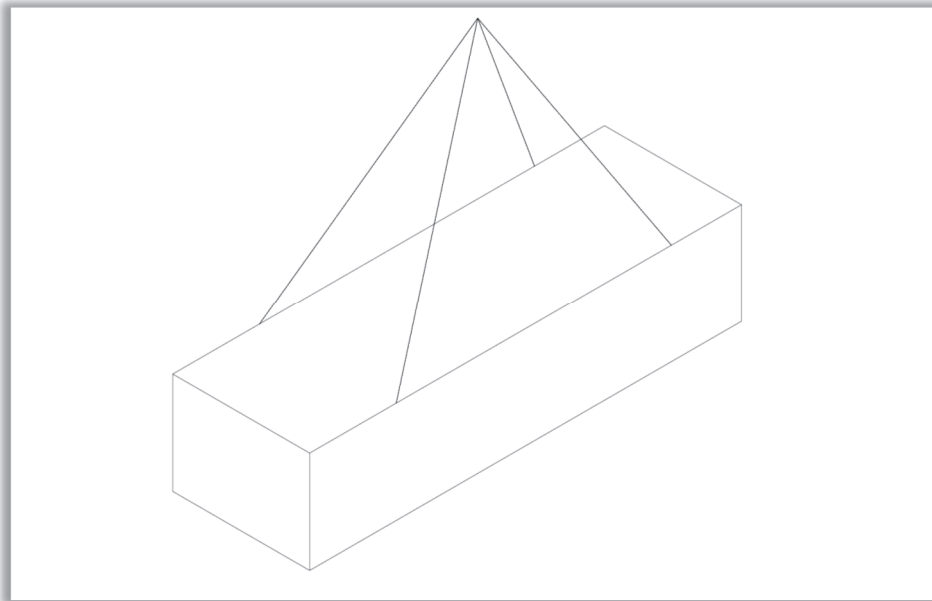
The drolover enclosure must be able to be lifted with attached applicable equipment.

### 9.1 FEA model

The model of A1 OPE is copied and all load cases deleted except load case 1: selfweight. In this load case an extra distributed load is applied to the roof area to reach a total of 10 000 kg. This equals the 10T that is used to determine the lifting point dimensions.

The calculation model currently weighs in at 7907 kg.

The drolover will be lifted as a single hook, 4 leg lift as seen below.



*Figure 9-1 Drolover lifting set up*

To comply with the lifting setup, one lifting point is fixed for X, Y and Z direction. The other lifting points allow for translation in X and Y direction, because the 4 leg lift will result in compression in the members between the lifting points.

## 9.2 Results

Below the results of the structural calculation. The profiles will be checked according CSA S16-09. Stress and deformation will be displayed to show the behavior of the structure.

### 9.2.1 Unity Checks

CAN/CSA S16-09 - Member Verification ( SLS ; ULS ) 8 11 21 23to27 35to71 77to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196

Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)
85 dJC Beam 85	UNP 100	S 355	104.96	278.49	0.08	1 Structure Selfweight	0.00	1 Structure Selfweight	0.13	1 Structure Selfweight
87 dJC Beam 87	UNP 100	S 355	104.96	278.49	0.07	1 Structure Selfweight	0.00	1 Structure Selfweight	0.07	1 Structure Selfweight
21 dJC Beam 21	UNP 100	S 355	104.96	278.49	0.07	1 Structure Selfweight	0.00	1 Structure Selfweight	0.06	1 Structure Selfweight
79 dJC Beam 79	UNP 100	S 355	104.96	278.49	0.07	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
24 dJC Beam 24	U 100x50x5	S 235	105.58	266.45	0.06	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight
25 dJC Beam 25	U 100x50x5	S 235	105.58	266.45	0.06	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight
26 dJC Beam 26	U 100x50x5	S 235	105.58	266.45	0.06	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
27 dJC Beam 27	U 100x50x5	S 235	105.58	266.45	0.06	1 Structure Selfweight	0.00	1 Structure Selfweight	0.09	1 Structure Selfweight
23 dJC Beam 23	U 100x50x5	S 235	105.58	266.45	0.05	1 Structure Selfweight	0.00	1 Structure Selfweight	0.09	1 Structure Selfweight
86 dJC Beam 86	UNP 100	S 355	104.96	278.49	0.05	1 Structure Selfweight	0.00	1 Structure Selfweight	0.09	1 Structure Selfweight
84 dJC Beam 84	UNP 100	S 355	104.96	278.49	0.05	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
82 dJC Beam 82	UNP 100	S 355	104.96	278.49	0.05	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight
83 dJC Beam 83	UNP 100	S 355	104.96	278.49	0.05	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight

Figure 9-2 Unity Checks for top utilized profiles (>4%), sorted on overall ratio high to low

As can be seen the highest utilized members are the UNP 100 beams in the roof. 8% of its capacity is used and therefore suffices to the structural verification according CSA S16-09.

### 9.2.2 Stress

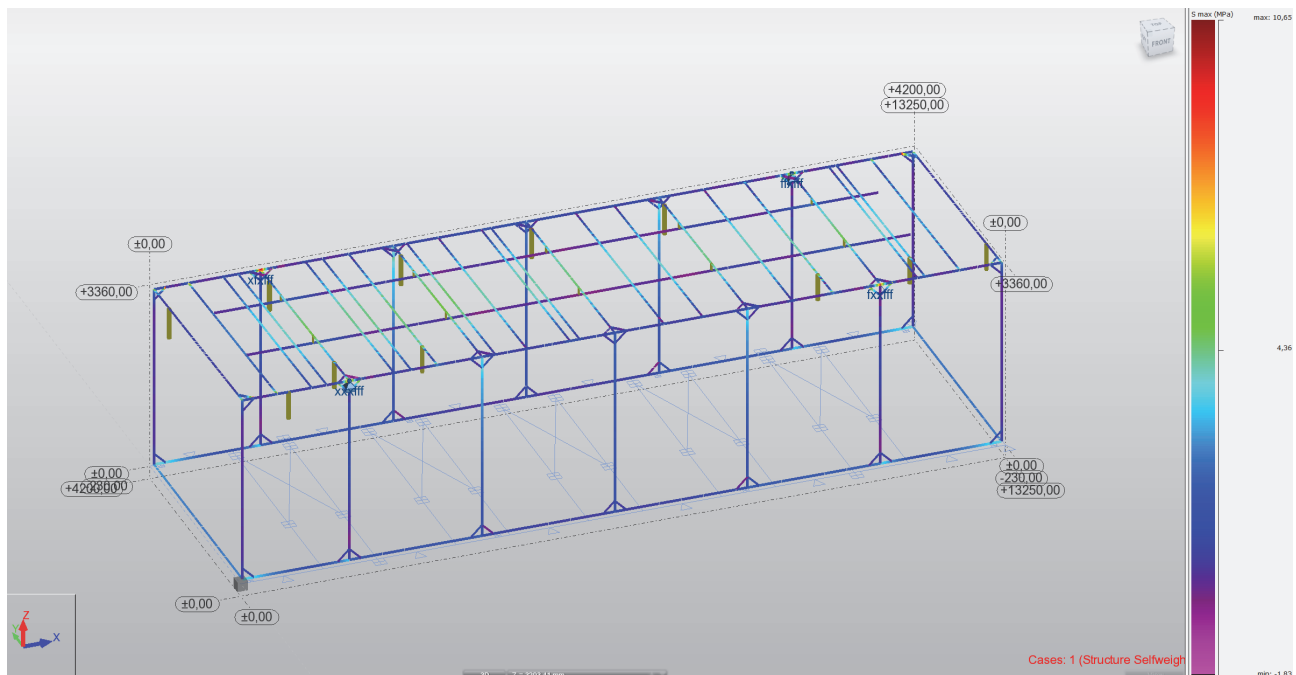


Figure 9-3 Stress peaks in profiles

As can be seen the highest stress peak is 11 MPa. This is within limits  $11 < 355$  MPa.

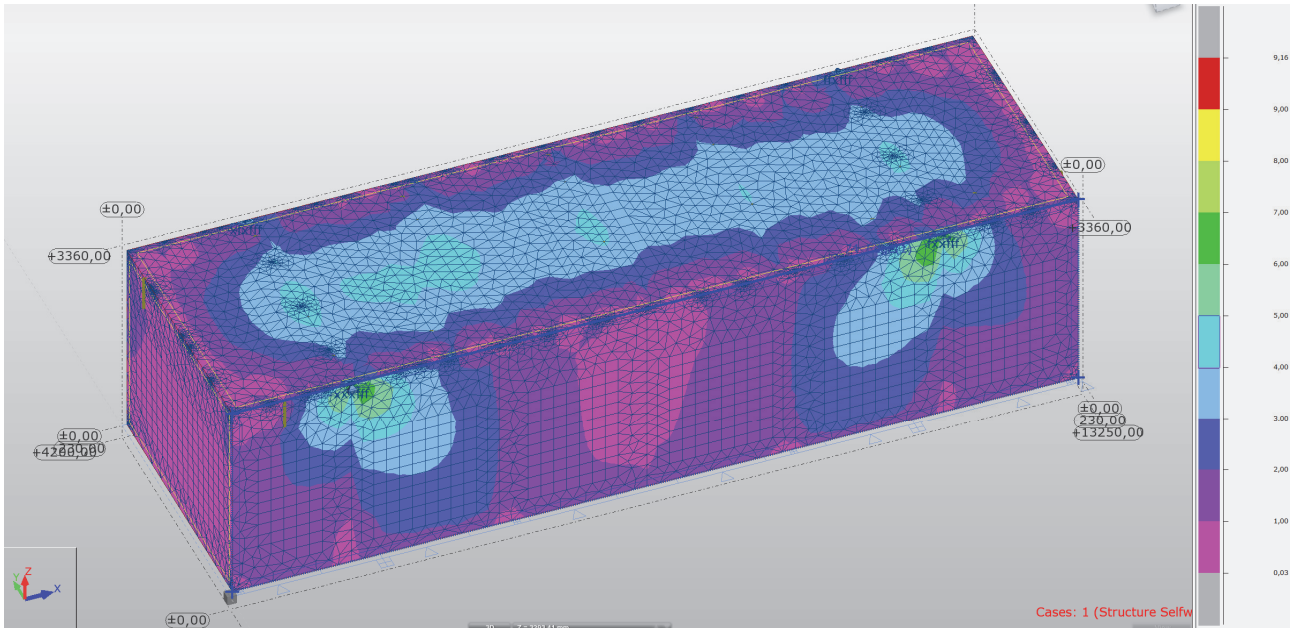


Figure 9-4 Stress in panels

As can be seen global stress values are max 10 MPa < limit of 140 MPa.

### 9.2.3 Deformation

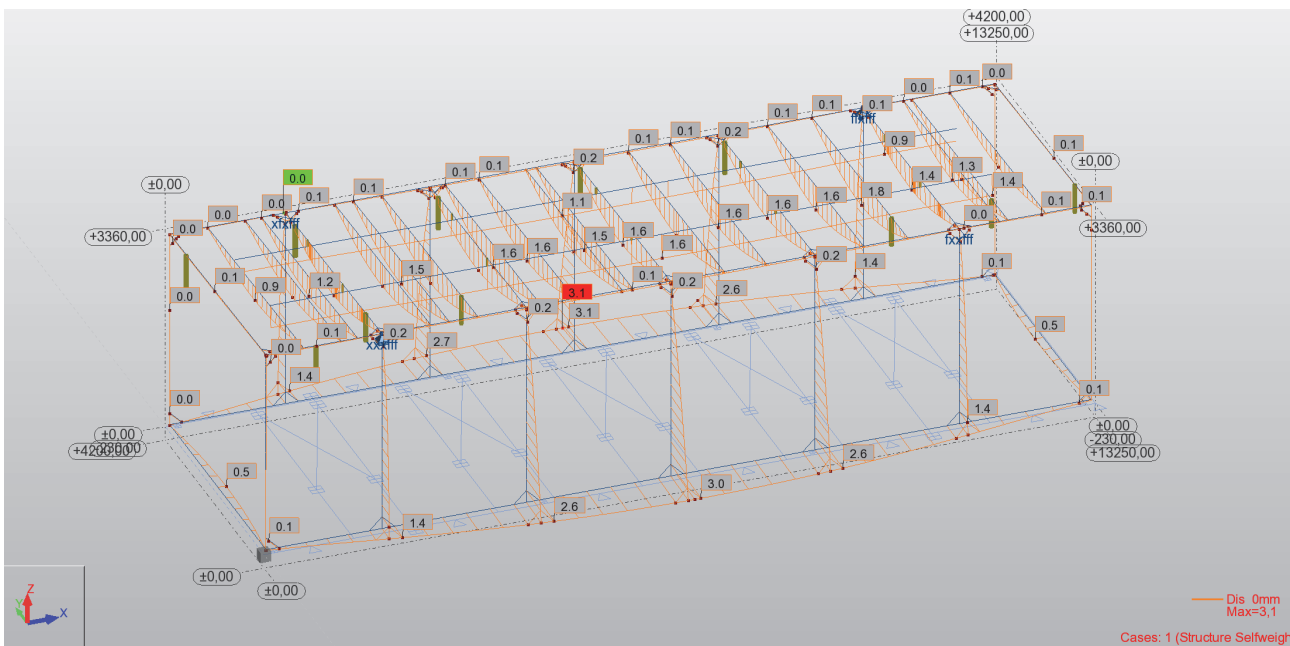


Figure 9-5 Deformation of profiles

As can be seen the largest deformation is 3,1 mm in the roof.  
This is within limits:  $(4200/3,1) = 1/1354 < 1/300$ .



## **10 Detail Analysis – Lifting - D4 LIFT**

Design of removable Secondary Lifting Eye for lifting the dropover enclosure.

To avoid confusion on which lifting eyes to use: primary padeyes connected to the enclosure skid or the lifting eyes for the dropover enclosure the dropover received the requirement that the lifting eyes must be removable.

As the to be lifted weight allows for this, removable off-the-shelve lifting eyes can be applied.

Based on EN 1993-1-8 and DEP 34.00.01.30-Gen an excel sheet is used to determine the to be used lifting eye.

To give the design some margin, the total to be lifted weight is regarded as 10 000 kg or 10 metric tons. The current design is 7 907 kg.

The selected lifting eye is a swivel lifting point able to rotate 360° and used with a lifting angle between 0 and 90°. The MBL equals 4xWLL, which does not comply with §4 of the TR 0875-SP020: "Safety factor 5 shall be used for lifting lugs, relative to the minimum break load."

Therefore an extra safety factor  $5/4 = 1,25$  is applied.

DEP 34.00.01.30-Gen §3.15 determines a lift load increase due to manufacturing tolerances of **10%**  
DEP 34.00.01.30-Gen §2.3.2.a determines an impact factor **1,3** for the shackle.

This results in a sling force for the lifting eye of 58,5 kN, determining the WLL of 6T.

Please see Appendix C for the calculation sheet.

Appendix D shows the datasheets of the selected 6T lifting point.





## **11 Conclusion**

For the structural verification of the enclosure skid and drolover enclosure several calculation models and detail calculations are made. The section below presents the conclusions of each calculation.

### **11.1 Structural Analysis - Operational - A1 OPE**

- This calculation model comprises the complete assembly of enclosure skid and drolover enclosure and is subjected to operational conditions.
- The results show that the structural unity checks according CSA S16-09 are sufficient.
- The stress values are below stated limits.
- The deformation values are below stated limits.
  
- The design is therefore structurally safe for its intended use.

### **11.2 Detail Analysis – Operational - D1 OPE**

- This detail calculation determines the bolted connection between enclosure skid and existing support structure in operational condition. The calculation is based on results from model A1 OPE.
- ASTM A325 ¾" bolts suffice for this connection

### **11.3 Detail Analysis – Operational - D2 OPE**

- This detail calculation determines the bolted connection between enclosure skid and drolover enclosure in operational condition. The calculation is based on results from model A1 OPE.
- ISO 4017 M16 8.8 bolts suffice for this connection. M20 will be used for practical reasons.

### **11.4 Structural Analysis - Lifting – A2 LIFT**

- This calculation model comprises the complete assembly of enclosure skid and drolover enclosure, based on a maximum of 30 t and is subjected to lifting conditions.
- The results show that the structural unity checks according CSA S16-09 are sufficient.
- The stress values are below stated limits.
- The deformation values are below stated limits.
  
- The design is therefore structurally safe for its intended use.

### **11.5 Detail Analysis – Lifting - D3 LIFT**

- This detail calculation determines the required lifting shackle for lifting the 30 t with single spreader beam. A 17,0 t bow shackle is selected.
- The padeye dimensions are determined based on lifting shackle.
- The bolted connections between enclosure skid and removable lifting eyes are determined as 4 x ISO 4017 M16 8.8. M20 will be used for practical reasons.

### **11.6 Structural Analysis – Deformation - A3 DEF**

- This calculation model comprises the complete assembly of enclosure skid and drolover enclosure and is subjected to a max possible span between constraints with regard to the onsite support structure.
- The results show that the structural unity checks according CSA S16-09 are sufficient.
- The stress values are below stated limits.
- The deformation values are below stated limits. The results show the enclosure skid + drolover enclosure set has a higher stiffness than the support platform.
  
- The design is therefore structurally safe for its intended use.

### **11.7 Structural Analysis – Lifting - B LIFT**

- This calculation model comprises the enclosure skid, based on a maximum of 20 t and is subjected to lifting conditions.





- The results show that the structural unity checks according CSA S16-09 are sufficient.
- The stress values are below stated limits
- The deformation values are below stated limits
  
- The design is therefore structurally safe for its intended use.

### **11.8 Structural Analysis – Lifting - C LIFT**

- This calculation model comprises the drolover enclosure, based on a maximum of 10 t and is subjected to lifting conditions.
- The results show that the structural unity checks according CSA S16-09 are sufficient.
- The stress values are below stated limits.
- The deformation values are below stated limits.
  
- The design is therefore structurally safe for its intended use.

### **11.9 Detail Analysis – Lifting - D4 LIFT**

- This detail calculation determines the required lifting shackle for lifting the 10 t with single spreader beam. A 6,0 t 3d lifting eye is selected.



# Appendices



## Appendix A Load Combination Table

Load Case	Description
1	Structure Selfweight
2	Snow
3	Roof load
4	Floor load
5	Crane loads
6	Wind1 - long side
7	Wind2 - short side
8	Modal
9	Seismic - NBCC 2010 Direction_X
10	Seismic - NBCC 2010 Direction_Y
11	Seismic - NBCC 2010 Direction_Z

ULS and SLS code combinations according NBCC 2010

Case	Load Case	Coefficient		Load Case	Coefficient		Load Case	Coefficient		Load Case	Coefficient		Load Case	Coefficient		Load Case	Coefficient	
ULS/1	1	1.40																
ULS/2	1	1.25	+	3	1.50	+	5	1.50	+	4	1.50							
ULS/3	1	1.25	+	6	0.40	+	3	1.50	+	5	1.50	+	4	1.50				
ULS/4	1	1.25	+	3	1.50	+	5	1.50	+	7	0.40	+	4	1.50				
ULS/5	1	1.25	+	3	1.50													
ULS/6	1	1.25	+	6	0.40	+	3	1.50										
ULS/7	1	1.25	+	3	1.50	+	7	0.40										
ULS/8	1	1.25	+	5	1.50													
ULS/9	1	1.25	+	6	0.40	+	5	1.50										
ULS/10	1	1.25	+	5	1.50	+	7	0.40										
ULS/11	1	1.25	+	3	1.50	+	5	1.50										
ULS/12	1	1.25	+	6	0.40	+	3	1.50	+	5	1.50							
ULS/13	1	1.25	+	3	1.50	+	5	1.50	+	7	0.40							
ULS/14	1	1.25	+	4	1.50													
ULS/15	1	1.25	+	6	0.40	+	4	1.50										
ULS/16	1	1.25	+	7	0.40	+	4	1.50										
ULS/17	1	1.25	+	3	1.50	+	4	1.50										
ULS/18	1	1.25	+	6	0.40	+	3	1.50	+	4	1.50							
ULS/19	1	1.25	+	3	1.50	+	7	0.40	+	4	1.50							
ULS/20	1	1.25	+	5	1.50	+	4	1.50										
ULS/21	1	1.25	+	6	0.40	+	5	1.50	+	4	1.50							
ULS/22	1	1.25	+	5	1.50	+	7	0.40	+	4	1.50							
ULS/23	1	0.90	+	3	1.50	+	5	1.50	+	4	1.50							
ULS/24	1	0.90	+	6	0.40	+	3	1.50	+	5	1.50	+	4	1.50				
ULS/25	1	0.90	+	3	1.50	+	5	1.50	+	7	0.40	+	4	1.50				
ULS/26	1	0.90																
ULS/27	1	0.90	+	3	1.50													
ULS/28	1	0.90	+	6	0.40	+	3	1.50										
ULS/29	1	0.90	+	3	1.50	+	7	0.40										
ULS/30	1	0.90	+	5	1.50													
ULS/31	1	0.90	+	6	0.40	+	5	1.50										
ULS/32	1	0.90	+	5	1.50	+	7	0.40										
ULS/33	1	0.90	+	3	1.50	+	5	1.50										
ULS/34	1	0.90	+	6	0.40	+	3	1.50	+	5	1.50							



ULS/35	1	0.90	+	3	1.50	+	5	1.50	+	7	0.40							
ULS/36	1	0.90	+	4	1.50													
ULS/37	1	0.90	+	6	0.40	+	4	1.50										
ULS/38	1	0.90	+	7	0.40	+	4	1.50										
ULS/39	1	0.90	+	3	1.50	+	4	1.50										
ULS/40	1	0.90	+	6	0.40	+	3	1.50	+	4	1.50							
ULS/41	1	0.90	+	3	1.50	+	7	0.40	+	4	1.50							
ULS/42	1	0.90	+	5	1.50	+	4	1.50										
ULS/43	1	0.90	+	6	0.40	+	5	1.50	+	4	1.50							
ULS/44	1	0.90	+	5	1.50	+	7	0.40	+	4	1.50							
ULS/45	1	1.25	+	2	0.50	+	3	1.50	+	5	1.50	+	4	1.50				
ULS/46	1	1.25	+	2	0.50	+	3	1.50										
ULS/47	1	1.25	+	2	0.50	+	5	1.50										
ULS/48	1	1.25	+	2	0.50	+	3	1.50	+	5	1.50							
ULS/49	1	1.25	+	2	0.50	+	4	1.50										
ULS/50	1	1.25	+	2	0.50	+	3	1.50	+	4	1.50							
ULS/51	1	1.25	+	2	0.50	+	5	1.50	+	4	1.50							
ULS/52	1	0.90	+	2	0.50	+	3	1.50	+	5	1.50	+	4	1.50				
ULS/53	1	0.90	+	2	0.50	+	3	1.50										
ULS/54	1	0.90	+	2	0.50	+	5	1.50										
ULS/55	1	0.90	+	2	0.50	+	3	1.50	+	5	1.50							
ULS/56	1	0.90	+	2	0.50	+	4	1.50										
ULS/57	1	0.90	+	2	0.50	+	3	1.50	+	4	1.50							
ULS/58	1	0.90	+	2	0.50	+	5	1.50	+	4	1.50							
ULS/59	1	1.25	+	6	1.40	+	3	0.50	+	5	0.50	+	4	0.50				
ULS/60	1	1.25	+	3	0.50	+	5	0.50	+	7	1.40	+	4	0.50				
ULS/61	1	1.25	+	6	1.40													
ULS/62	1	1.25	+	7	1.40													
ULS/63	1	1.25	+	6	1.40	+	3	0.50										
ULS/64	1	1.25	+	3	0.50	+	7	1.40										
ULS/65	1	1.25	+	6	1.40	+	5	0.50										
ULS/66	1	1.25	+	5	0.50	+	7	1.40										
ULS/67	1	1.25	+	6	1.40	+	3	0.50	+	5	0.50							
ULS/68	1	1.25	+	3	0.50	+	5	0.50	+	7	1.40							
ULS/69	1	1.25	+	6	1.40	+	4	0.50										
ULS/70	1	1.25	+	7	1.40	+	4	0.50										
ULS/71	1	1.25	+	6	1.40	+	3	0.50	+	4	0.50							
ULS/72	1	1.25	+	3	0.50	+	7	1.40	+	4	0.50							
ULS/73	1	1.25	+	6	1.40	+	5	0.50	+	4	0.50							
ULS/74	1	1.25	+	5	0.50	+	7	1.40	+	4	0.50							
ULS/75	1	0.90	+	6	1.40	+	3	0.50	+	5	0.50	+	4	0.50				
ULS/76	1	0.90	+	3	0.50	+	5	0.50	+	7	1.40	+	4	0.50				
ULS/77	1	0.90	+	6	1.40													
ULS/78	1	0.90	+	7	1.40													
ULS/79	1	0.90	+	6	1.40	+	3	0.50										
ULS/80	1	0.90	+	3	0.50	+	7	1.40										
ULS/81	1	0.90	+	6	1.40	+	5	0.50										
ULS/82	1	0.90	+	5	0.50	+	7	1.40										
ULS/83	1	0.90	+	6	1.40	+	3	0.50	+	5	0.50							
ULS/84	1	0.90	+	3	0.50	+	5	0.50	+	7	1.40							
ULS/85	1	0.90	+	6	1.40	+	4	0.50										
ULS/86	1	0.90	+	7	1.40	+	4	0.50										
ULS/87	1	0.90	+	6	1.40	+	3	0.50	+	4	0.50							
ULS/88	1	0.90	+	3	0.50	+	7	1.40	+	4	0.50							
ULS/89	1	0.90	+	6	1.40	+	5	0.50	+	4	0.50							
ULS/90	1	0.90	+	5	0.50	+	7	1.40	+	4	0.50							
ULS/91	1	1.25	+	6	1.40	+	2	0.50										
ULS/92	1	1.25	+	2	0.50	+	7	1.40										



ULS/93	1	0.90	+	6	1.40	+	2	0.50									
ULS/94	1	0.90	+	2	0.50	+	7	1.40									
ULS/95	1	1.25	+	2	1.50	+	3	0.50	+	5	0.50	+	4	0.50			
ULS/96	1	1.25	+	2	1.50												
ULS/97	1	1.25	+	2	1.50	+	3	0.50									
ULS/98	1	1.25	+	2	1.50	+	5	0.50									
ULS/99	1	1.25	+	2	1.50	+	3	0.50	+	5	0.50						
ULS/100	1	1.25	+	2	1.50	+	4	0.50									
ULS/101	1	1.25	+	2	1.50	+	3	0.50	+	4	0.50						
ULS/102	1	1.25	+	2	1.50	+	5	0.50	+	4	0.50						
ULS/103	1	0.90	+	2	1.50	+	3	0.50	+	5	0.50	+	4	0.50			
ULS/104	1	0.90	+	2	1.50												
ULS/105	1	0.90	+	2	1.50	+	3	0.50									
ULS/106	1	0.90	+	2	1.50	+	5	0.50									
ULS/107	1	0.90	+	2	1.50	+	3	0.50	+	5	0.50						
ULS/108	1	0.90	+	2	1.50	+	4	0.50									
ULS/109	1	0.90	+	2	1.50	+	3	0.50	+	4	0.50						
ULS/110	1	0.90	+	2	1.50	+	5	0.50	+	4	0.50						
ULS/111	1	1.25	+	6	0.40	+	2	1.50									
ULS/112	1	1.25	+	2	1.50	+	7	0.40									
ULS/113	1	0.90	+	6	0.40	+	2	1.50									
ULS/114	1	0.90	+	2	1.50	+	7	0.40									
ULS/115	1	1.00	+	2	0.25	+	3	0.50	+	9	1.00	+	5	0.50	+	4	0.50
ULS/116	1	1.00	+	3	0.50	+	9	1.00	+	5	0.50	+	4	0.50			
ULS/117	1	1.00	+	2	0.25	+	9	1.00									
ULS/118	1	1.00	+	9	1.00												
ULS/119	1	1.00	+	2	0.25	+	3	0.50	+	9	1.00						
ULS/120	1	1.00	+	3	0.50	+	9	1.00									
ULS/121	1	1.00	+	2	0.25	+	9	1.00	+	5	0.50						
ULS/122	1	1.00	+	9	1.00	+	5	0.50									
ULS/123	1	1.00	+	2	0.25	+	3	0.50	+	9	1.00	+	5	0.50			
ULS/124	1	1.00	+	3	0.50	+	9	1.00	+	5	0.50						
ULS/125	1	1.00	+	2	0.25	+	9	1.00	+	4	0.50						
ULS/126	1	1.00	+	9	1.00	+	4	0.50									
ULS/127	1	1.00	+	2	0.25	+	3	0.50	+	9	1.00	+	4	0.50			
ULS/128	1	1.00	+	3	0.50	+	9	1.00	+	4	0.50						
ULS/129	1	1.00	+	2	0.25	+	9	1.00	+	5	0.50	+	4	0.50			
ULS/130	1	1.00	+	9	1.00	+	5	0.50	+	4	0.50						
ULS/131	1	1.00	+	2	0.25	+	3	0.50	+	10	1.00	+	5	0.50	+	4	0.50
ULS/132	1	1.00	+	3	0.50	+	10	1.00	+	5	0.50	+	4	0.50			
ULS/133	1	1.00	+	2	0.25	+	10	1.00									
ULS/134	1	1.00	+	10	1.00												
ULS/135	1	1.00	+	2	0.25	+	3	0.50	+	10	1.00						
ULS/136	1	1.00	+	3	0.50	+	10	1.00									
ULS/137	1	1.00	+	2	0.25	+	10	1.00	+	5	0.50						
ULS/138	1	1.00	+	10	1.00	+	5	0.50									
ULS/139	1	1.00	+	2	0.25	+	3	0.50	+	10	1.00	+	5	0.50			
ULS/140	1	1.00	+	3	0.50	+	10	1.00	+	5	0.50						
ULS/141	1	1.00	+	2	0.25	+	10	1.00	+	4	0.50						
ULS/142	1	1.00	+	10	1.00	+	4	0.50									
ULS/143	1	1.00	+	2	0.25	+	3	0.50	+	10	1.00	+	4	0.50			
ULS/144	1	1.00	+	3	0.50	+	10	1.00	+	4	0.50						
ULS/145	1	1.00	+	2	0.25	+	10	1.00	+	5	0.50	+	4	0.50			
ULS/146	1	1.00	+	10	1.00	+	5	0.50	+	4	0.50						
ULS/147	1	1.00	+	2	0.25	+	3	0.50	+	11	1.00	+	5	0.50	+	4	0.50
ULS/148	1	1.00	+	3	0.50	+	11	1.00	+	5	0.50	+	4	0.50			
ULS/149	1	1.00	+	2	0.25	+	11	1.00									
ULS/150	1	1.00	+	11	1.00												



ULS/151	1	1.00	+	2	0.25	+	3	0.50	+	11	1.00						
ULS/152	1	1.00	+	3	0.50	+	11	1.00									
ULS/153	1	1.00	+	2	0.25	+	11	1.00	+	5	0.50						
ULS/154	1	1.00	+	11	1.00	+	5	0.50									
ULS/155	1	1.00	+	2	0.25	+	3	0.50	+	11	1.00	+	5	0.50			
ULS/156	1	1.00	+	3	0.50	+	11	1.00	+	5	0.50						
ULS/157	1	1.00	+	2	0.25	+	11	1.00	+	4	0.50						
ULS/158	1	1.00	+	11	1.00	+	4	0.50									
ULS/159	1	1.00	+	2	0.25	+	3	0.50	+	11	1.00	+	4	0.50			
ULS/160	1	1.00	+	3	0.50	+	11	1.00	+	4	0.50						
ULS/161	1	1.00	+	2	0.25	+	11	1.00	+	5	0.50	+	4	0.50			
ULS/162	1	1.00	+	11	1.00	+	5	0.50	+	4	0.50						
ULS/163	1	1.00	+	2	0.25	+	3	0.50	+	9	-1.00	+	5	0.50	+	4	0.50
ULS/164	1	1.00	+	3	0.50	+	9	-1.00	+	5	0.50	+	4	0.50			
ULS/165	1	1.00	+	2	0.25	+	9	-1.00									
ULS/166	1	1.00	+	9	-1.00												
ULS/167	1	1.00	+	2	0.25	+	3	0.50	+	9	-1.00						
ULS/168	1	1.00	+	3	0.50	+	9	-1.00									
ULS/169	1	1.00	+	2	0.25	+	9	-1.00	+	5	0.50						
ULS/170	1	1.00	+	9	-1.00	+	5	0.50									
ULS/171	1	1.00	+	2	0.25	+	3	0.50	+	9	-1.00	+	5	0.50			
ULS/172	1	1.00	+	3	0.50	+	9	-1.00	+	5	0.50						
ULS/173	1	1.00	+	2	0.25	+	9	-1.00	+	4	0.50						
ULS/174	1	1.00	+	9	-1.00	+	4	0.50									
ULS/175	1	1.00	+	2	0.25	+	3	0.50	+	9	-1.00	+	4	0.50			
ULS/176	1	1.00	+	3	0.50	+	9	-1.00	+	4	0.50						
ULS/177	1	1.00	+	2	0.25	+	9	-1.00	+	5	0.50	+	4	0.50			
ULS/178	1	1.00	+	9	-1.00	+	5	0.50	+	4	0.50						
ULS/179	1	1.00	+	2	0.25	+	3	0.50	+	10	-1.00	+	5	0.50	+	4	0.50
ULS/180	1	1.00	+	3	0.50	+	10	-1.00	+	5	0.50	+	4	0.50			
ULS/181	1	1.00	+	2	0.25	+	10	-1.00									
ULS/182	1	1.00	+	10	-1.00												
ULS/183	1	1.00	+	2	0.25	+	3	0.50	+	10	-1.00						
ULS/184	1	1.00	+	3	0.50	+	10	-1.00									
ULS/185	1	1.00	+	2	0.25	+	10	-1.00	+	5	0.50						
ULS/186	1	1.00	+	10	-1.00	+	5	0.50									
ULS/187	1	1.00	+	2	0.25	+	3	0.50	+	10	-1.00	+	5	0.50			
ULS/188	1	1.00	+	3	0.50	+	10	-1.00	+	5	0.50						
ULS/189	1	1.00	+	2	0.25	+	10	-1.00	+	4	0.50						
ULS/190	1	1.00	+	10	-1.00	+	4	0.50									
ULS/191	1	1.00	+	2	0.25	+	3	0.50	+	10	-1.00	+	4	0.50			
ULS/192	1	1.00	+	3	0.50	+	10	-1.00	+	4	0.50						
ULS/193	1	1.00	+	2	0.25	+	10	-1.00	+	5	0.50	+	4	0.50			
ULS/194	1	1.00	+	10	-1.00	+	5	0.50	+	4	0.50						
ULS/195	1	1.00	+	2	0.25	+	3	0.50	+	11	-1.00	+	5	0.50	+	4	0.50
ULS/196	1	1.00	+	3	0.50	+	11	-1.00	+	5	0.50	+	4	0.50			
ULS/197	1	1.00	+	2	0.25	+	11	-1.00									
ULS/198	1	1.00	+	11	-1.00												
ULS/199	1	1.00	+	2	0.25	+	3	0.50	+	11	-1.00						
ULS/200	1	1.00	+	3	0.50	+	11	-1.00									
ULS/201	1	1.00	+	2	0.25	+	11	-1.00	+	5	0.50						
ULS/202	1	1.00	+	11	-1.00	+	5	0.50									
ULS/203	1	1.00	+	2	0.25	+	3	0.50	+	11	-1.00	+	5	0.50			
ULS/204	1	1.00	+	3	0.50	+	11	-1.00	+	5	0.50						
ULS/205	1	1.00	+	2	0.25	+	11	-1.00	+	4	0.50						
ULS/206	1	1.00	+	11	-1.00	+	4	0.50									
ULS/207	1	1.00	+	2	0.25	+	3	0.50	+	11	-1.00	+	4	0.50			
ULS/208	1	1.00	+	3	0.50	+	11	-1.00	+	4	0.50						



ULS/209	1	1.00	+	2	0.25	+	11	-1.00	+	5	0.50	+	4	0.50			
ULS/210	1	1.00	+	11	-1.00	+	5	0.50	+	4	0.50						
SLS/1	1	1.00	+	3	1.00	+	5	1.00	+	4	1.00						
SLS/2	1	1.00															
SLS/3	1	1.00	+	3	1.00												
SLS/4	1	1.00	+	5	1.00												
SLS/5	1	1.00	+	3	1.00	+	5	1.00									
SLS/6	1	1.00	+	4	1.00												
SLS/7	1	1.00	+	3	1.00	+	4	1.00									
SLS/8	1	1.00	+	5	1.00	+	4	1.00									
SLS/9	1	1.00	+	6	1.00												
SLS/10	1	1.00	+	7	1.00												
SLS/11	1	1.00	+	2	1.00												
SLS/12	1	1.00	+	6	1.00	+	3	1.00	+	5	1.00	+	4	1.00			
SLS/13	1	1.00	+	3	1.00	+	5	1.00	+	7	1.00	+	4	1.00			
SLS/14	1	1.00	+	6	1.00	+	3	1.00									
SLS/15	1	1.00	+	3	1.00	+	7	1.00									
SLS/16	1	1.00	+	6	1.00	+	5	1.00									
SLS/17	1	1.00	+	5	1.00	+	7	1.00									
SLS/18	1	1.00	+	6	1.00	+	3	1.00	+	5	1.00						
SLS/19	1	1.00	+	3	1.00	+	5	1.00	+	7	1.00						
SLS/20	1	1.00	+	6	1.00	+	4	1.00									
SLS/21	1	1.00	+	7	1.00	+	4	1.00									
SLS/22	1	1.00	+	6	1.00	+	3	1.00	+	4	1.00						
SLS/23	1	1.00	+	3	1.00	+	7	1.00	+	4	1.00						
SLS/24	1	1.00	+	6	1.00	+	5	1.00	+	4	1.00						
SLS/25	1	1.00	+	5	1.00	+	7	1.00	+	4	1.00						
SLS/26	1	1.00	+	2	1.00	+	3	1.00	+	5	1.00	+	4	1.00			
SLS/27	1	1.00	+	2	1.00	+	3	1.00									
SLS/28	1	1.00	+	2	1.00	+	5	1.00									
SLS/29	1	1.00	+	2	1.00	+	3	1.00	+	5	1.00						
SLS/30	1	1.00	+	2	1.00	+	4	1.00									
SLS/31	1	1.00	+	2	1.00	+	3	1.00	+	4	1.00						
SLS/32	1	1.00	+	2	1.00	+	5	1.00	+	4	1.00						
SLS/33	1	1.00	+	6	1.00	+	2	1.00									
SLS/34	1	1.00	+	2	1.00	+	7	1.00									
SLS/35	1	1.00	+	6	1.00	+	2	1.00	+	3	1.00	+	5	1.00	+	4	1.00
SLS/36	1	1.00	+	2	1.00	+	3	1.00	+	5	1.00	+	7	1.00	+	4	1.00
SLS/37	1	1.00	+	6	1.00	+	2	1.00	+	3	1.00						
SLS/38	1	1.00	+	2	1.00	+	3	1.00	+	7	1.00						
SLS/39	1	1.00	+	6	1.00	+	2	1.00	+	5	1.00						
SLS/40	1	1.00	+	2	1.00	+	5	1.00	+	7	1.00						
SLS/41	1	1.00	+	6	1.00	+	2	1.00	+	3	1.00	+	5	1.00			
SLS/42	1	1.00	+	2	1.00	+	3	1.00	+	5	1.00	+	7	1.00			
SLS/43	1	1.00	+	6	1.00	+	2	1.00	+	4	1.00						
SLS/44	1	1.00	+	2	1.00	+	7	1.00	+	4	1.00						
SLS/45	1	1.00	+	6	1.00	+	2	1.00	+	3	1.00	+	4	1.00			
SLS/46	1	1.00	+	2	1.00	+	3	1.00	+	7	1.00	+	4	1.00			
SLS/47	1	1.00	+	6	1.00	+	2	1.00	+	5	1.00	+	4	1.00			
SLS/48	1	1.00	+	2	1.00	+	5	1.00	+	7	1.00	+	4	1.00			



## **Appendix B**

## **Padeye design sheet – Full set**

Excel printout



**Pad Eye calculation (EN 1993-1-8 + DEP 34.00.01.30-Gen)**

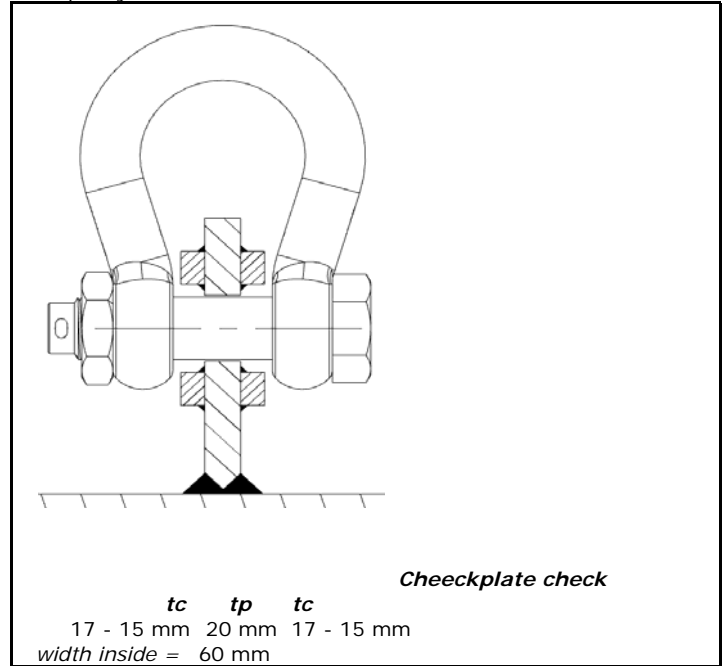
According EN 1993-1-8: 2006 - Table 3.9: automatic calculation of initial padeye dimensions

Blue is input value

Orange is primary dimension for design

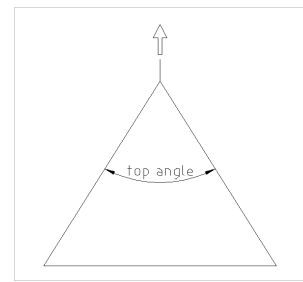
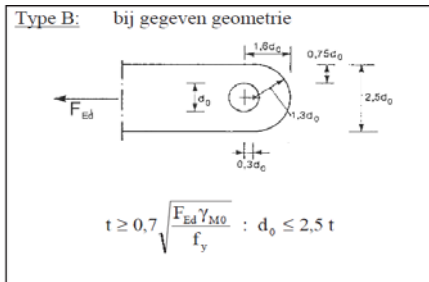
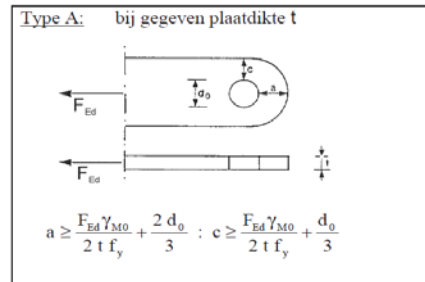
**Project Information**

Client	de Jong Combustion
Project	Carmon Creek
Project no.	405109540
Padeye position	Primary lifting
Total Weight	30 000 kg
Applicable lifting points	3
Weight increase	10 %
F <sub>z</sub> per shackle	107 910 N
impact factor, shackle	1,3
impact factor, lug	2,0
MAX Top Angle - 2 slings	60 °
F <sub>sling</sub> , shackle	161 985 N
F <sub>sling</sub> , lug	249 207 N
f <sub>y,d</sub> (Yield strength of used material)	355 N/mm <sup>2</sup>
γ <sub>MO</sub> (Material factor EN 1993-1-1 §6.1)	1,00



**GREENPIN BOW Shackle determination**

WLL	16,51 t
Applicable BOW-shackle	17,00 t
Shackle pin diameter d	42,0 mm



**Initial Dimensions**

Hole diameter d0; nom	45 mm	Depends on shackle, max difference hole-pin of 6% (DNV)
Minimum Strip Thickness	20 mm	Based on type A and B minimum thickness
Minimum Strip Width	145 mm	Based on type A and B minimum width
c <sub>p</sub>	50 mm	
a <sub>p</sub>	50 mm	

**Verification Type**

Type A - Strip with given thickness		Current value	
a <sub>p</sub>	48 mm ≤	50 mm	OK
c <sub>p</sub>	33 mm ≤	50 mm	OK

Type B - Strip with given geometry		Current value	
t	19 mm ≤	20 mm	OK
d <sub>g,nom</sub>	50 mm ≥	45 mm	OK
offset centre dim [0,3d <sub>0</sub> ]	14 mm		
c <sub>p</sub> [0,75d <sub>0</sub> ]	34 mm ≤	50 mm	OK
a <sub>p</sub> [1,1d <sub>0</sub> ]	50 mm ≤	50 mm	OK
Edge [1,6d <sub>0</sub> ]	72 mm ≤	72,5 mm	OK
Width strip [2,5d <sub>0</sub> ]	113 mm ≤	145 mm	OK

**BOW-shackle verification 17 metric tons**

Maximum hole difference of 4mm per DEP 34.00.01.30-Gen §2.3.2.1

difference hole and pin	d <sub>pin</sub> (mm)	d <sub>0</sub> (mm)	difference	
	42	45	3,0 mm	OK

Needed fillet welded cheek plates to obtain min 75% of inside shackle width

a <sub>shackle</sub> (mm)	min (mm)	t <sub>padeye</sub> (mm)	2 x cheek plates of tc=
6,0	60,0	54,0	20 17 mm MAX
8,0	60,0	52,0	20 15 mm MIN

Remaining space inside BOW shackle

f <sub>shackle</sub> (mm)	
length inside of shackle	146,0 mm
lost length by padeye ap	50 mm
Remaining space	96,0 mm



## **Appendix C**

Excel printout

## **Padeye design sheet – Dropover Enclosure**

**Pad Eye calculation (EN 1993-1-8 + DEP 34.00.01.30-Gen)**

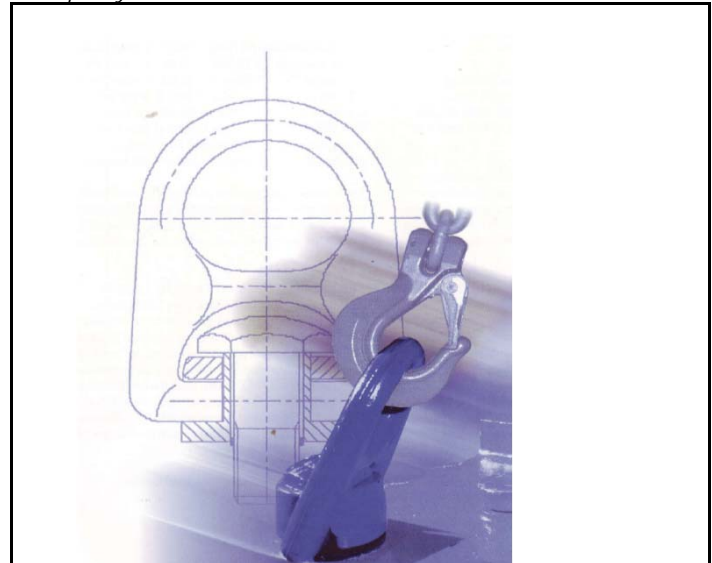
According EN 1993-1-8: 2006 - Table 3.9: automatic calculation of initial padeye dimensions

Blue is input value

Orange is primary dimension for design

**Project Information**

Client	de Jong Combustion
Project	Carmon Creek
Project no.	405109540
Padeye position	Hood lifting 3D Lifting Eye
Total Weight	10 000 kg
Applicable lifting points	3
Weight increase	10 %
F <sub>z</sub> per shackle	35 970 N
impact factor, shackle	1,3
impact factor, lug	2,0
eye safetyfactor 4 vs req 5	1,25
MAX Top Angle - 2 slings	0 °
F <sub>sling</sub> , 3D shackle	58 451 N
F <sub>sling</sub> , bolted connection	89 925 N
f <sub>y,d</sub> (Yield strength of used material)	355 N/mm <sup>2</sup>
γ <sub>M0</sub> (Material factor EN 1993-1-1 §6.1)	1,00

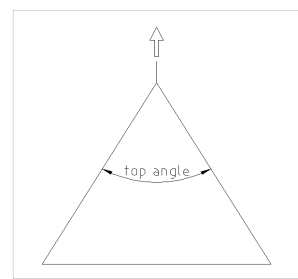
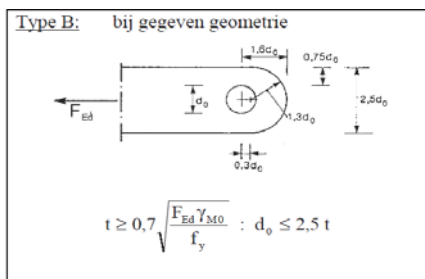
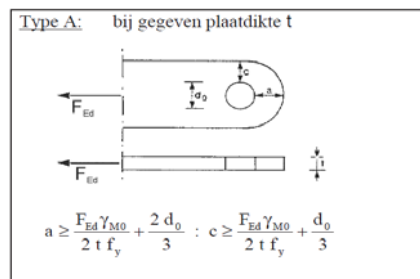


Checkplate check

tc tp tc  
7 - 6 mm 15 mm 7 - 6 mm  
width inside = 36 mm

**Eickhoff 3D Lift Eye WLL determination**

<b>WLL</b>	<b>5,96 t</b>
Applicable BOW-shackle	6,50 t
Shackle pin diameter d	25,0 mm



**Initial Dimensions**

Hole diameter d <sub>0</sub> ; nom	27 mm	Depends on shackle, max difference hole-pin of 6% (DNV)
Minimum Strip Thickness	15 mm	Based on type A and B minimum thickness
Minimum Strip Width	90 mm	Based on type A and B minimum width
c <sub>p</sub>	31,5 mm	
a <sub>p</sub>	31,5 mm	

**Verification Type**

Type A - Strip with given thickness			Current value	
a <sub>p</sub>	27 mm	≤	31,5 mm	OK
c <sub>p</sub>	18 mm	≤	31,5 mm	OK

Type B - Strip with given geometry			Current value	
t	12 mm	≤	15 mm	OK
d <sub>g,nom</sub>	38 mm	≥	27 mm	OK
offset centre dim [0,3d <sub>0</sub> ]	9 mm			
c <sub>p</sub> [0,75d <sub>0</sub> ]	21 mm	≤	31,5 mm	OK
a <sub>p</sub> [1,1d <sub>0</sub> ]	30 mm	≤	31,5 mm	OK
Edge [1,6d <sub>0</sub> ]	44 mm	≤	45 mm	OK
Width strip [2,5d <sub>0</sub> ]	68 mm	≤	90 mm	OK

**BOW-shackle verification 6,5 metric tons**

Maximum hole difference of 4mm per DEP 34.00.01.30-Gen §2.3.2.f					
	d <sub>pin</sub> (mm)	d <sub>0</sub> (mm)	difference		
difference hole and pin	25	27	2,0 mm	OK	
Needed fillet welded cheek plates to obtain min 75% of inside shackle width					
	a <sub>shackle</sub> (mm)	min (mm)	t <sub>padeye</sub> (mm)	2 x cheek plates of tc=	
	6,0	36,0	30,0	15	7 mm MAX
	8,0	36,0	28,0	15	6 mm MIN
Remaining space inside BOW shackle					
	f <sub>shackle</sub> (mm)				
length inside of shackle	83,0 mm				
lost length by padeye a <sub>p</sub>	31,5 mm				
Remaining space	51,5 mm				

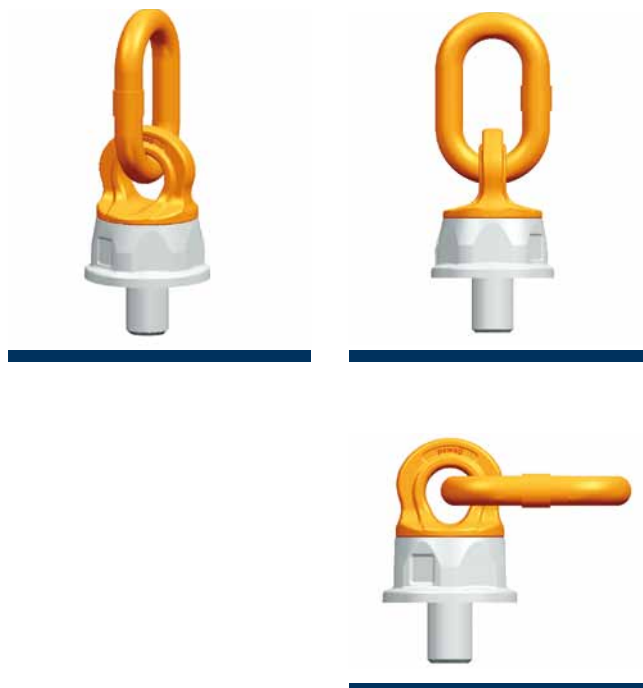


## **Appendix D      3D lifting point datasheet**

## PLDW pewag winner profilift delta

Ball-bearing 360° under load rotatable lifting point. High resistant lifting eye 180° movable. The special screws are 100% crack-tested as well as protected against corrosion, and marked with WLL and thread size. Each lifting point is marked with an individual serial number, that allows traceability. The table with the load capacities depending on the method of lifting as lifting gear, number of legs and angle of inclination is a part of the user manual and packed together with each lifting point.

The pewag winner profilift delta lifting points are marked with a WLL for the most inappropriate field of application, which explains the increased WLL in the upright loaded position, with a 4-fold safety against break in all directions of load.



Method of lifting										
Number of legs	1	1	2	2	2	2	3+4	3+4	2	3+4
Angle of inclination	0°	90°	0°	90°	0°-45°	45°-60°	0°-45°	45°-60°	asymm.	asymm.

Code	Thread [mm]	Fastening torque [Nm]	Load capacity [kg]									
			600	300	1.200	600	400	300	600	400	300	300
PLDW 0,3 t	M8	10	600	300	1.200	600	400	300	600	400	300	300
PLDW 0,5 t	M10	10	1.000	500	2.000	1.000	700	500	1.000	750	500	500
PLDW 0,7 t	M12	15	1.400	700	2.800	1.400	950	700	1.400	1.000	700	700
PLDW 1 t*	M14	25	2.000	1.000	4.000	2.000	1.400	1.000	2.100	1.500	1.000	1.000
PLDW 1,5 t	M16	30	2.600	1.500	5.200	3.000	2.100	1.500	3.100	2.100	1.500	1.500
PLDW 2,5 t	M20	80	4.500	2.500	9.000	5.000	3.500	2.500	5.300	3.500	2.500	2.500
PLDW 4 t	M24	150	7.000	4.000	14.000	8.000	5.500	4.000	8.400	6.000	4.000	4.000
PLDW 6 t	M30	230	10.000	6.000	20.000	12.000	8.400	6.000	12.600	9.000	6.000	6.000
PLDW 8 t	M36	450	12.500	8.000	25.000	16.000	11.200	8.000	16.800	12.000	8.000	8.000
PLDW 10 t	M42	600	16.000	10.000	32.000	20.000	14.000	10.000	21.000	15.000	10.000	10.000
PLDW 12,5 t	M48	600	16.000	12.500	32.000	25.000	17.500	12.500	26.200	18.000	12.500	12.500

\* Special models only available on request!

**Safety factor 4**

Attention: Subject to technical changes!

Availability on request!

### Permissible usage

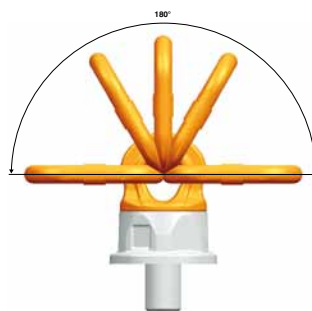
Load capacity acc. to the inspection certificate respectively table of WLL in the mentioned directions of pull – see picture 1.

### Non permissible usage

Make sure when choosing the assembly that improper load can not arise e.g. if:

- The direction of pull is obstructed
- Direction of pull is not in the foreseen area (see picture 2)
- Loading ring rests against edges or load

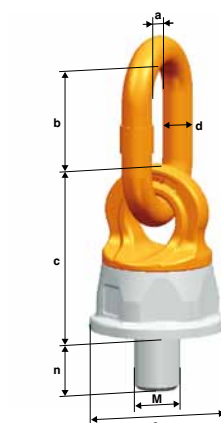
For more details please have a look into our detailed user manual.




Picture 1



Picture 2



Code	Thread [mm]	Load capacity [kg]	a [mm]	b [mm]	c [mm]	Ø d [mm]	Ø e [mm]	n [mm]	 [mm]	Weight [kg/pc.]
PLDW 0,3t	M8	300	30	38	54	13	38	20	34	0,47
PLDW 0,5t	M10	500	30	38	54	13	38	20	34	0,47
PLDW 0,7t	M12	700	35	48	54	13	38	22	34	0,47
PLDW 1t *	M14	1.000	35	48	54	13	38	22	34	0,47
PLDW 1,5t	M16	1.500	35	48	54	13	38	33	34	0,49
PLDW 2,5t	M20	2.500	35	55	75	16	55	33	46	1,10
PLDW 4t	M24	4.000	40	66	82	17	63	40	50	1,50
PLDW 6t	M30	6.000	50	70	92	23	72	40	60	2,50
PLDW 8t	M36	8.000	50	91	124	23	92	55	75	4,30
PLDW 10t	M42	10.000	65	91	124	27	92	60	75	5,10
PLDW 12,5t	M48	12.500	65	116	124	27	92	68	75	5,40

\* Only on request!

Attention: Subject to technical changes!

Availability on request!



## **Appendix F      FEA Output Report (Autodesk Robot)**



**Alara-Lukagro BV**  
Huijgensweg 3  
2964LL GROOT-AMMERS  
The Netherlands  
T: 0184-661700  
F: 0184-662721

Customer : De Jong Combustion BV  
Ordernumber : 405109540  
Customerprojectnr : PO 613087500/85679  
Project : Carmon Creek  
Description : A1 OPE - Main Skid & Dropover Enclosure - Operational condition  
Revision : R00

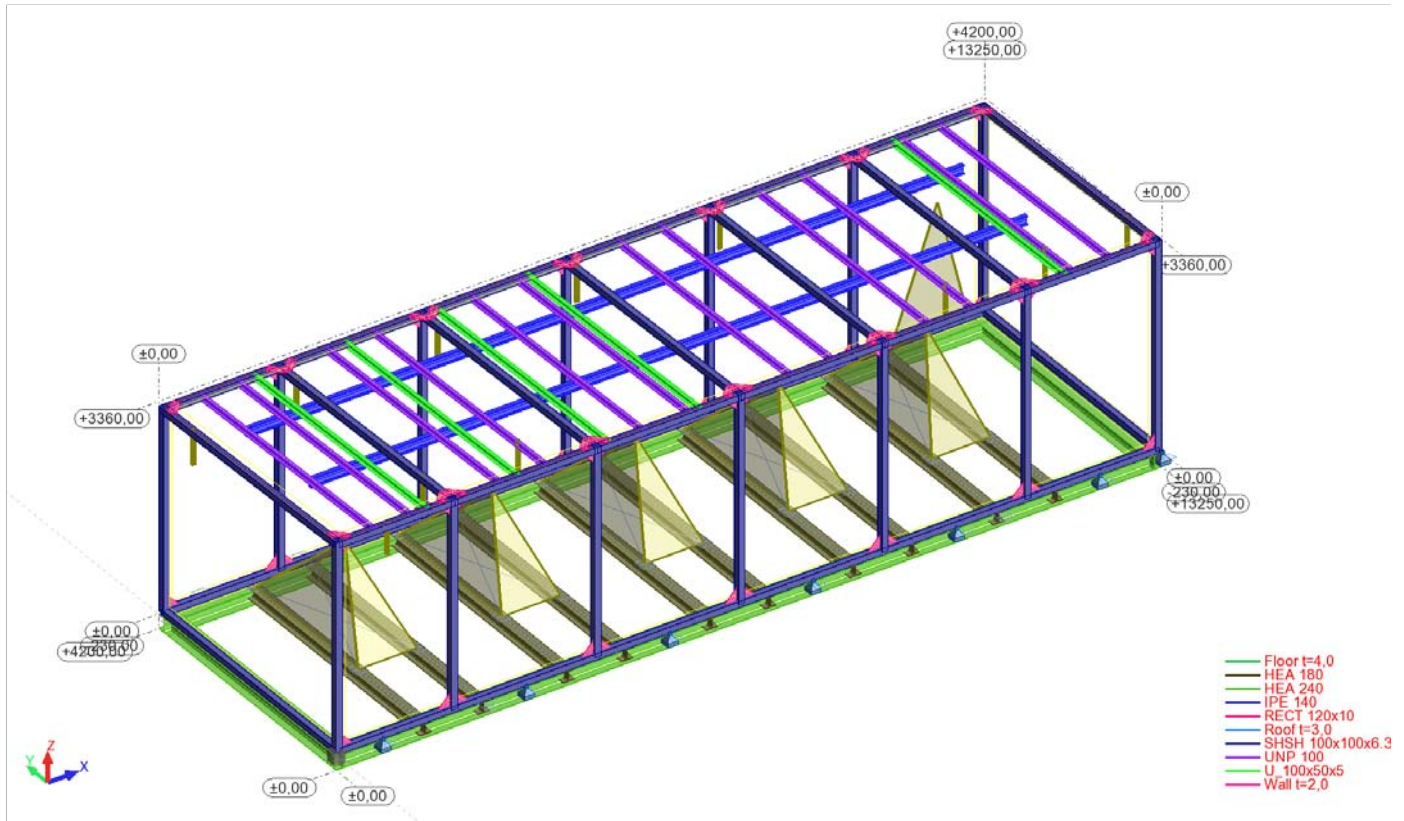
**Project : 405109540.6000\_A1\_OPE\_REV\_01\_4 Operational**

**Made by : BvH**



Structure View	3
Data - Bars	4
Data - Panels	8
Data - Supports	9
Data - Sections	9
Section properties	10
Loads - Cases	12
Loads - Values	12
Reactions ULS: global extremes	13
Displacements SLS: global extremes	13
Member Forces ULS: envelope	14
Member Verification	46

Structure View



## Data - Bars

Bar	Node 1	Node 2	Section	Material	Length (mm)	Gamma (Deg)	Type	Structure object	Offset name	Values of automatic offsets
23	111	112	U_100x50-x5	S 23-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
24	113	114	U_100x50-x5	S 23-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
25	115	116	U_100x50-x5	S 23-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
26	117	118	U_100x50-x5	S 23-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
27	119	120	U_100x50-x5	S 23-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
2	5	72	HEA 240	S 3-55	13250,00	0,0	dJC_-Beam	Beam	Bovenflens-Links	B :X=0,0 Y=120,00 Z=-115,00 E : X=0,0 Y=120,00 Z=-115,00 Local
3	72	71	HEA 240	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens-Links	B :X=0,0 Y=120,00 Z=-115,00 E : X=0,0 Y=120,00 Z=-115,00 Local
4	71	8	HEA 240	S 3-55	13250,00	0,0	dJC_-Beam	Beam	Bovenflens-Links	B :X=0,0 Y=120,00 Z=-115,00 E : X=0,0 Y=120,00 Z=-115,00 Local
5	8	5	HEA 240	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens-Links	B :X=0,0 Y=120,00 Z=-115,00 E : X=0,0 Y=120,00 Z=-115,00 Local
6	9	10	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
7	11	12	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
8	2	4	IPE 140	S 3-55	11500,00	0,0	dJC_-Bm_-Crm	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-70,00 E : X=0,0 Y=0,0 Z=-70,0-0 Local
9	15	16	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
15	27	28	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
16	29	30	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
17	31	32	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
21	182	183	UNP 100	S 3-55	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
179	267	257	RECT 120-x10	S 3-55	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
10	17	18	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
11	1	3	IPE 140	S 3-55	11500,00	0,0	dJC_-Bm_-Crm	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-70,00 E : X=0,0 Y=0,0 Z=-70,0-0 Local
12	21	22	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
13	23	24	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
14	25	26	HEA 180	S 3-55	4200,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-85,50 E : X=0,0 Y=0,0 Z=-85,5-0 Local
80	156	157	UNP 100	S 3-55	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
81	158	159	UNP 100	S 3-55	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
111	216	214	RECT 120-x10	S 3-55	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
112	217	218	RECT 120-x10	S 3-55	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
113	219	217	RECT 120-x10	S 3-55	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
114	220	221	RECT 120-x10	S 3-55	282,84	0,0	dJC_-Beam	Beam	N/A	N/A

Bar	Node 1	Node 2	Section	Material	Length (mm)	Gamma (Deg)	Type	Structure object	Offset name	Values of automatic offsets
131	222	223	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
133	225	226	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
175	265	251	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
176	266	253	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
177	266	254	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
178	267	256	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
77	180	181	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
78	152	153	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
79	154	155	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
180	268	259	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
181	268	260	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
183	263	262	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
184	224	223	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
185	269	226	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
186	227	269	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
187	270	229	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
188	230	270	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
189	271	232	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
190	233	271	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
191	272	235	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
192	236	272	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
193	273	238	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
194	239	273	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
196	241	242	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
82	160	161	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
134	227	225	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
83	162	163	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
135	228	229	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
136	230	228	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
84	164	165	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
85	166	167	UNP 100	S 35-5	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local

Bar	Node 1	Node 2	Section	Material	Length (mm)	Gamma (Deg)	Type	Structure object	Offset name	Values of automatic offsets
137	231	232	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
138	233	231	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
86	168	169	UNP 100	S 35-5	4100,60	0,0	dJC_Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
87	170	171	UNP 100	S 35-5	4100,60	0,0	dJC_Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
139	234	235	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
140	236	234	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
88	185	184	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
89	186	187	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
141	237	238	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
90	188	186	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
142	239	237	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
91	189	190	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
144	241	240	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
145	243	244	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
92	191	189	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
93	192	193	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
147	246	247	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
94	194	192	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
148	248	246	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
95	195	196	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
149	249	250	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
150	251	249	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
96	197	195	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
151	252	253	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
97	198	199	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
98	200	198	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
152	254	252	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
100	202	201	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
153	255	256	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A
102	203	204	RECT 120-x10	S 35-5	282,84	0,0	dJC_Beam	Beam	N/A	N/A
154	257	255	RECT 120-x10	S 35-5	282,84	-0,0	dJC_Beam	Beam	N/A	N/A



Bar	Node 1	Node 2	Section	Material	Length (mm)	Gamma (Deg)	Type	Structure object	Offset name	Values of automatic offsets
104	205	206	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
155	258	259	RECT 120-x10	S 35-5	282,84	-0,0	dJC_-Beam	Beam	N/A	N/A
156	260	258	RECT 120-x10	S 35-5	282,84	-0,0	dJC_-Beam	Beam	N/A	N/A
105	207	205	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
106	208	209	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
158	262	261	RECT 120-x10	S 35-5	282,84	-0,0	dJC_-Beam	Beam	N/A	N/A
107	210	208	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
171	245	244	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
108	211	212	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
172	264	247	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
109	213	211	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
173	264	248	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
110	214	215	RECT 120-x10	S 35-5	282,84	0,0	dJC_-Beam	Beam	N/A	N/A
174	265	250	RECT 120-x10	S 35-5	282,86	90,0	dJC_-Beam	Beam	N/A	N/A
35	75	76	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
36	77	78	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
37	79	80	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
38	81	82	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
39	83	84	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
40	85	86	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
41	87	88	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
42	89	90	SHSH 100-x100x6.3	S 42-0	3240,00	0,0	dJC_-Col	Column	N/A	N/A
43	91	92	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
51	77	101	SHSH 100-x100x6.3	S 4-20	13150,00	0,0	dJC_-Beam	Beam	N/A	N/A
57	94	82	SHSH 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B : X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
44	93	94	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
45	95	96	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
46	97	98	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
47	99	100	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
48	101	102	SHSH 100-x100x6.3	S 42-0	3310,00	0,0	dJC_-Col	Column	N/A	N/A
49	89	75	SHSH 100-x100x6.3	S 4-20	13150,00	0,0	dJC_-Beam	Beam	N/A	N/A

Bar	Node 1	Node 2	Section	Material	Length (mm)	Gamma (Deg)	Type	Structure object	Offset name	Values of automatic offsets
50	75	77	S SHS H 100-x100x6.3	S 42-0	4100,00	0,0	dJC_-Beam	Beam	N/A	N/A
52	101	89	S SHS H 100-x100x6.3	S 42-0	4100,00	0,0	dJC_-Beam	Beam	N/A	N/A
53	102	90	S SHS H 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
54	100	88	S SHS H 100-x100x6.3	S 42-0	4100,60	-0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
56	96	84	S SHS H 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
58	92	80	S SHS H 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
59	78	76	S SHS H 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
70	92	78	S SHS H 100-x100x6.3	S 42-0	1850,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
71	80	76	S SHS H 100-x100x6.3	S 42-0	1850,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
55	98	86	S SHS H 100-x100x6.3	S 42-0	4100,60	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
60	102	100	S SHS H 100-x100x6.3	S 42-0	2100,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
61	90	88	S SHS H 100-x100x6.3	S 42-0	2100,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
62	100	98	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
63	88	86	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
64	98	96	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
65	86	84	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
66	96	94	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
67	84	82	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
68	94	92	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local
69	82	80	S SHS H 100-x100x6.3	S 42-0	2300,00	0,0	dJC_-Beam	Beam	Bovenflens	B :X=0,0 Y=0,0 Z=-50,00 E : X=0,0 Y=0,0 Z=-50,0-0 Local

## Data - Panels

Panel	Thic-knes s	Material	Meshing type	Reinfo-rcement type	Area (mm2)
19	Flo-ort=4,0	S 2-35	Del-aun-ay	N/A	55649998,65
72	Wal-lt=2,0	D-C-01	Del-aun-ay	N/A	13427500,00
73	Wal-lt=2,0	D-C-01	Del-aun-ay	N/A	13427500,00
74	Wal-lt=2,0	D-C-01	Del-aun-ay	N/A	43526500,00
75	Wal-lt=2,0	D-C-01	Del-aun-ay	N/A	42606000,00

76	Roo- ft=- 3,0	D- C- 01	Del- aun- ay	N/A	53922857,35
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## Data - Supports

Support name	List of nodes	List of edges	List of objects	Support conditions
Scharnierend	71 72 100-0to1011			UXUY UZ

## Data - Sections

Section name	Bar list			AX (mm2)	AY (mm2)	AZ (mm2)	IX (mm4)	IY (mm4)	IZ (mm4)
H-E-A-2-4-0	2to5	7680,00	5760,00	1725,00	421000,00	77630000,00	27690000,00		
I-P-E-1-4-0	8 11	1643,00	1007,40	658,00	23990,00	5410000,00	449000,00		
U-N-P-1-0-0	21 77to87	1345,00	799,00	549,00	25210,00	2053000,00	291600,00		
U-1-00-x-50-x5	23to27	950,00	500,00	450,00	7522,77	1432916,67	225005,48		
H-E-A-1-8-0	6 7 9 10 12to17	4530,00	3420,00	1026,00	148900,00	25100000,00	9250000,00		
R-E-C-T-1-2-0-x-1-0	88to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196	1200,00	1000,00	1000,00	37899,23	1440000,00	10000,00		

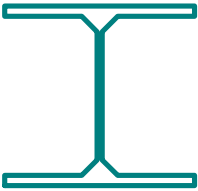


S-							
H-							
S-							
H							
1-							
0-							
0-		35to71	2318,65	1159,30	1159,30	5341795,00	3355722,00
x-							
1-							
0-							
0-							
x-							
6-							
.3							

Section properties

Section properties:

HEA 240



HY=240,0, HZ=230,0 [mm]

AX=7680,00 [mm<sup>2</sup>]

IX=421000,00, IY=77630000,00, IZ=27690000,00 [mm<sup>4</sup>]

Material=S 355

IPE 140



HY=73,0, HZ=140,0 [mm]

AX=1643,00 [mm<sup>2</sup>]

IX=23990,00, IY=5410000,00, IZ=449000,00 [mm<sup>4</sup>]

Material=S 355

UNP 100



HY=50,0, HZ=100,0 [mm]

AX=1345,00 [mm<sup>2</sup>]

IX=25210,00, IY=2053000,00, IZ=291600,00 [mm<sup>4</sup>]

Material=S 355

U\_100x50x5



HY=50,0, HZ=100,0 [mm]  
AX=950,00 [mm<sup>2</sup>]  
IX=7522,77, IY=1432916,67, IZ=225005,48 [mm<sup>4</sup>]  
Material=S 235

HEA 180



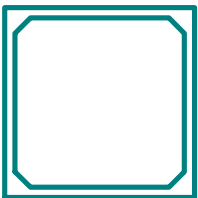
HY=180,0, HZ=171,0 [mm]  
AX=4530,00 [mm<sup>2</sup>]  
IX=148900,00, IY=25100000,00, IZ=9250000,00 [mm<sup>4</sup>]  
Material=S 355

RECT 120x10



HY=10,0, HZ=120,0 [mm]  
AX=1200,00 [mm<sup>2</sup>]  
IX=37899,23, IY=1440000,00, IZ=10000,00 [mm<sup>4</sup>]  
Material=S 355

SHSH 100x100x6.3



HY=100,0, HZ=100,0 [mm]  
AX=2318,65 [mm<sup>2</sup>]  
IX=5341795,00, IY=3355722,00, IZ=3355722,00 [mm<sup>4</sup>]  
Material=S 420

## Loads - Cases

Case	Label	Case name	Nature	Analysis type
1	G-1	Structure Selfweight	dead	Static - Linear
2	S-N1	Snow	snow	Static - Linear
3	L1	Roof loads	live	Static - Linear
4	L2	Floor loads	live	Static - Linear
5	L3	Crane loads	live	Static - Linear
6	W-IN-D1	Wind 1	wind	Static - Linear
7	W-IN-D2	Wind 2	wind	Static - Linear
8	M-O-D	Modal		Modal
9	S-EI-X	Seismic - NBCC 2010 Direction_X	Earthquake/Accidental	Dynamics - Seismic
10	S-EI-Y	Seismic - NBCC 2010 Direction_Y	Earthquake/Accidental	Dynamics - Seismic
11	S-EI-Z	Seismic - NBCC 2010 Direction_Z	Earthquake/Accidental	Dynamics - Seismic
12		ULS		Static - Linear
13		ULS+		Static - Linear
14		ULS-		Static - Linear
15		SLS		Static - Linear
16		SLS+		Static - Linear
17		SLS-		Static - Linear

## Loads - Values

Case	Load type	List	Load values
1	self-weight	2to17 19 21 23to27 35to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196	PZ Negative Factor=1,00
1	Body forces		AZ=-1,00 relative
1	(FE) uniform	72to75	PZ=-0,000166(N/mm2)
1	(FE) uniform	19	PZ=-0,000372(N/mm2)
1	(FE) uniform	76	PZ=-0,000122(N/mm2)
2	(FE) uniform	76	PZ=-0,002800(N/mm2)

Case	Load type	List	Load values
3	(FE) u-niform	76	PZ=-0,001000(N/mm2)
4	(FE) u-niform	19	PZ=-0,004800(N/mm2)
5	nodal force	65	FX=13,000000(N) FY=13,000000(N) FZ=-281,000000(N)
5	nodal force	66	FX=184,000000(N) FY=184,000000(N) FZ=-4043,000000(N)
6	(FE) pl-anar	74	PY1=0,001138(N/mm2) PY2=0,001138(N/mm2) PY3=0,001086(N/mm2) N1X=50,00(mm) N1Y=50,00(mm) N1Z=3360,00(mm) N2X=13200,00(mm) N2Y=50,00(mm) N2Z=3360,00(mm) N3X=13200,00(mm) N3Y=50,00(mm) N3Z=50,00(mm)
6	(FE) pl-anar	75	PY1=0,000711(N/mm2) PY2=0,000711(N/mm2) PY3=0,000679(N/mm2) N1X=50,00(mm) N1Y=4150,00(mm) N1Z=3290,00(mm) N2X=13200,00(mm) N2Y=4150,00(mm) N2Z=3290,00(mm) N3X=13200,00(mm) N3Y=4150,00(mm) N3Z=50,00(mm)
6	(FE) u-niform	76	PZ=0,000996(N/mm2)
7	(FE) pl-anar	73	PX1=-0,001138(N/mm2) PX2=-0,001138(N/mm2) PX3=-0,001086(N/mm2) N1X=13200,00(mm) N1Y=57,36(mm) N1Z=3359,87(mm) N2X=13200,00(mm) N2Y=4150,00(mm) N2Z=3290,00(mm) N3X=13200,00(mm) N3Y=4150,00(mm) N3Z=50,00(mm)
7	(FE) pl-anar	72	PX1=-0,000711(N/mm2) PX2=-0,000711(N/mm2) PX3=-0,000679(N/mm2) N1X=13200,00(mm) N1Y=57,36(mm) N1Z=3359,87(mm) N2X=13200,00(mm) N2Y=4150,00(mm) N2Z=3290,00(mm) N3X=13200,00(mm) N3Y=4150,00(mm) N3Z=50,00(mm)
7	(FE) u-niform	76	PZ=0,000996(N/mm2)

## Reactions ULS: global extremes

	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>M-AX</b>	69920,554392	81622,442883	82833,960229	0,00	0,00	0,00
<b>Node</b>	1006	1008	1000	1009	1002	1011
<b>Case</b>	ULS/95	ULS/45	ULS/45	ULS/45	ULS/51	ULS/-24
<b>Mode</b>						
<b>MI-N</b>	-	-	-	-	-	-
	78611,759740	83385,064801	22445,964468	0,00	0,00	0,00
<b>Node</b>	1001	1000	72	1004	71	1002
<b>Case</b>	ULS/99	ULS/45	6	ULS/45	ULS/45	ULS/-45
<b>Mode</b>						

## Displacements SLS: global extremes

	UX (mm)	UY (mm)	UZ (mm)	RX (Rad)	RY (Rad)	RZ (Rad)
<b>MAX</b>	10,0	7,6	2,7	0,008	0,014	0,010
<b>Node</b>	1057	7795	5814	5577	4775	7765

	UX (mm)	UY (mm)	UZ (mm)	RX (Rad)	RY (Rad)	RZ (Rad)
<b>Case</b>	9	10	6	SLS/26	SLS/27	10
<b>Mode</b>	SRSS	SRSS				SRSS
<b>MIN</b>	-2,6	-3,7	-11,4	-0,008	-0,014	-0,004
<b>Node</b>	1479	2016	7554	7013	6100	2795
<b>Case</b>	SLS/42	SLS/29	SLS/26	SLS/29	SLS/26	SLS/- 27
<b>Mode</b>						

## Member Forces ULS: envelope

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>2 / M-AX</b>	2559,915451	26581,100167	22231,306709	87,37	1063,59	8309,37
<b>Node</b>	72	5	72	72	72	5
<b>Case</b>	6	ULS/45	6	ULS- /112	ULS- /15	ULS- /45
<b>Mode</b>						
<b>2 / MI-N</b>	-	-	-	-	-	-
7848,501209	25421,207169	41955,061181	218,42	340,63	691,90	
<b>Node</b>	72	72	72	72	72	5
<b>Case</b>	ULS/45	ULS/85	ULS/95	ULS- /89	ULS- /114	6
<b>Mode</b>						
<b>3 / M-AX</b>	19237,788837	2286,028310	13508,053495	123,60	4506,00	2682,68
<b>Node</b>	71	72	72	71	71	71
<b>Case</b>	6	ULS/73	ULS/16	ULS- /14	ULS- /91	ULS- /91
<b>Mode</b>						
<b>3 / MI-N</b>	-	-	-	-	-	-
81824,064329	1958,906185	11981,231346	151,50	6590,16	2843,56	
<b>Node</b>	71	71	71	72	72	72
<b>Case</b>	ULS/14	ULS/16	ULS/45	ULS- /21	ULS- /73	ULS- /81
<b>Mode</b>						
<b>4 / M-AX</b>	1350,421109	46850,362468	37308,328043	109,69	1110,49	8170,58
<b>Node</b>	71	71	71	71	8	71
<b>Case</b>	7	ULS/16	ULS/11- 1	ULS- /14	ULS- /15	ULS- /22
<b>Mode</b>						
<b>4 / MI-N</b>	-	-	-	-	-	-
13347,794923	18397,457131	6335,792033	151,33	62,53	877,40	
<b>Node</b>	71	8	71	71	71	71
<b>Case</b>	ULS/50	ULS/16	7	ULS- /93	4	6
<b>Mode</b>						
<b>5 / M-AX</b>	2824,066901	1537,148432	11639,751507	179,06	102,34	5460,16
<b>Node</b>	8	8	8	5	5	5

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	2	ULS/21	ULS/45	ULS-/45	6	ULS-/50
<b>Mode</b>						
<b>5 / MIN</b>	-	-	-	-	-	-
	27716,824184	2539,926948	11029,133366	146,53	1553,70	1014,52
<b>Node</b>	5	5	5	8	8	5
<b>Case</b>	ULS/45	ULS/50	ULS/14	ULS-/45	ULS-/45	6
<b>Mode</b>						
<b>6 / M-AX</b>	6045,775437	255,891702	22890,851191	5,73	438,38	163,38
<b>Node</b>	10	9	9	9	10	10
<b>Case</b>	6	ULS/16	ULS/50	ULS-/107	ULS-/107	6
<b>Mode</b>						
<b>6 / MIN</b>	-	-	-	-	-	-
	32119,292283	182,311404	21012,905281	11,74	2076,20	668,46
<b>Node</b>	10	10	10	10	10	10
<b>Case</b>	ULS/45	ULS/85	ULS/21	ULS-/95	ULS-/15	ULS-/45
<b>Mode</b>						
<b>7 / M-AX</b>	1850,342993	265,042847	22396,127865	21,97	158,09	724,97
<b>Node</b>	11	11	11	12	12	12
<b>Case</b>	6	ULS/45	ULS/15	ULS-/45	6	ULS-/45
<b>Mode</b>						
<b>7 / MIN</b>	-	-	-	-	-	-
	28894,079083	471,055359	20714,846507	9,84	1855,86	58,42
<b>Node</b>	12	12	12	11	12	11
<b>Case</b>	ULS/21	ULS/50	ULS/45	ULS-/95	ULS-/50	6
<b>Mode</b>						
<b>8 / MAX</b>	0,001033	0,006041	0,007874	0,00	0,00	0,00
<b>Node</b>	4	2	4	2	4	2
<b>Case</b>	10	ULS/13-3	10	ULS-/138	ULS-/188	ULS-/113
<b>Mode</b>	SRSS		SRSS			
<b>8 / MIN</b>	-	-	-	-	-	-
	0,000687	0,006041	0,004662	0,00	0,00	0,00
<b>Node</b>	4	2	4	2	4	2
<b>Case</b>	ULS/17-9	ULS/18-0	ULS/18-9	ULS-/189	10	ULS-/4
<b>Mode</b>					SRS-S	
<b>9 / M-AX</b>	635,910964	396,163236	22857,138398	1,85	78,23	99,22
<b>Node</b>	16	16	15	16	16	16
<b>Case</b>	7	ULS/50	ULS/45	6	2	6
<b>Mode</b>						
<b>9 / MIN</b>	-	-	-	-	-	-
	29335,513911	99,457172	20619,199659	17,96	1852,07	1032,53
<b>Node</b>	16	15	16	16	16	16
<b>Case</b>	ULS/45	ULS/22	ULS/15	ULS-/45	ULS-/16	ULS-/45
<b>Mode</b>						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>1-0 / M-A-X</b>	4313,559380	226,175921	22438,122042	24,04	213,39	1306,46
<b>Node</b>	17	17	17	18	18	17
<b>Case</b>	ULS/10-7	ULS/45	ULS/15	ULS-/45	6	ULS-/45
<b>Mode</b>						
<b>1-0 / M-IN</b>	29840,583757	524,504127	20729,513395	3,93	2016,00	155,16
<b>Node</b>	18	18	18	18	17	18
<b>Case</b>	ULS/45	ULS/50	ULS/45	6	ULS-/45	6
<b>Mode</b>						
<b>11 / MAX</b>	0,000938	0,006313	0,012922	0,00	0,00	0,00
<b>Node</b>	1	1	3	1	1	3
<b>Case</b>	10	ULS/14-0	10	ULS-/141	ULS-/183	ULS-/87
<b>Mode</b>	SRSS		SRSS			
<b>11 / MIN</b>	0,000300	0,006313	0,007125	0,00	0,00	0,00
<b>Node</b>	1	1	1	1	1	1
<b>Case</b>	ULS/17-9	ULS/18-9	ULS/17-9	ULS-/185	10	ULS-/86
<b>Mode</b>					SRS-S	
<b>1-2 / M-AX</b>	2900,858540	490,996607	22743,340278	10,47	254,61	91,96
<b>Node</b>	22	22	21	21	22	22
<b>Case</b>	6	ULS/45	ULS/50	ULS-/95	2	6
<b>Mode</b>						
<b>1-2 / M-IN</b>	35863,394493	288,278603	20568,696418	23,49	1695,04	958,29
<b>Node</b>	22	21	22	22	22	22
<b>Case</b>	ULS/45	ULS/45	ULS/21	ULS-/45	ULS-/15	ULS-/45
<b>Mode</b>						
<b>13 / M-A-X</b>	746,056592	196,559998	22121,842991	19,01	93,78	793,41
<b>Node</b>	23	23	23	24	23	24
<b>Case</b>	6	ULS/45	ULS/16	ULS-/45	2	ULS-/45
<b>Mode</b>						
<b>1-3 / M-IN</b>	27316,920754	361,673891	21189,265732	6,25	1932,48	34,37
<b>Node</b>	24	24	24	23	24	24
<b>Case</b>	ULS/45	ULS/50	ULS/45	ULS-/95	ULS-/14	6
<b>Mode</b>						
<b>14 / M-A-X</b>	2884,022900	429,754227	22473,556360	2,49	81,21	113,20

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	25	26	25	26	26	25
<b>Case</b>	2	ULS/50	ULS/45	6	6	7
<b>Mode</b>						
<b>1-4 / M-IN</b>	26599,614159	171,523024	20730,616737	18,94	1808,53	1193,18
<b>Node</b>	26	25	26	26	26	25
<b>Case</b>	ULS/3	ULS/45	ULS/16	ULS-/45	ULS-/16	ULS-/45
<b>Mode</b>						
<b>1-5 / M-AX</b>	1706,710005	145,311605	22553,758935	17,35	69,83	1078,28
<b>Node</b>	27	27	27	28	27	27
<b>Case</b>	2	ULS/45	ULS/45	ULS-/45	7	ULS-/45
<b>Mode</b>						
<b>1-5 / M-IN</b>	27400,382336	378,153853	20671,635179	2,29	1767,32	113,15
<b>Node</b>	28	28	28	28	28	27
<b>Case</b>	ULS/45	ULS/50	ULS/16	6	ULS-/16	7
<b>Mode</b>						
<b>1-6 / M-AX</b>	2025,966586	502,929080	23593,602486	15,67	219,92	43,99
<b>Node</b>	29	30	29	29	30	29
<b>Case</b>	7	ULS/50	ULS/45	ULS-/45	2	7
<b>Mode</b>						
<b>1-6 / M-IN</b>	37477,028390	414,964813	20672,762776	19,08	1544,46	826,48
<b>Node</b>	30	29	30	30	30	30
<b>Case</b>	ULS/45	ULS/45	ULS/16	ULS-/45	ULS-/16	ULS-/45
<b>Mode</b>						
<b>1-7 / M-AX</b>	17817,210990	15,872043	24554,392721	21,67	22,73	383,72
<b>Node</b>	31	32	31	31	32	32
<b>Case</b>	ULS/45	6	ULS/16	ULS-/3	7	ULS-/45
<b>Mode</b>						
<b>1-7 / M-IN</b>	16544,108822	712,206335	23110,511038	0,93	3644,49	287,25
<b>Node</b>	32	31	32	32	31	31
<b>Case</b>	ULS/16	ULS/3	ULS/45	6	ULS-/45	ULS-/21
<b>Mode</b>						
<b>2-1 / M-AX</b>	18669,502558	1308,831353	5891,200294	7,12	280,61	51,15



Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	183	183	182	182	183	182
<b>Case</b>	ULS/99	ULS/95	ULS/10-1	ULS-/95	6	6
<b>Mode</b>						
<b>2-1 / M-IN</b>	3864,112570	1348,713976	5888,576694	7,24	1396,52	217,66
<b>Node</b>	183	182	183	183	182	182
<b>Case</b>	ULS/85	ULS/95	ULS/95	ULS-/95	ULS-/101	ULS-/95
<b>Mode</b>						
<b>23 / MAX</b>	5680,959330	192,151123	3369,594282	0,17	226,63	29,57
<b>Node</b>	112	112	111	111	112	111
<b>Case</b>	ULS/97	ULS/61	ULS/97	ULS-/22	ULS-/81	ULS-/93
<b>Mode</b>						
<b>23 / MIN</b>	3692,996366	118,871738	3368,627105	0,62	454,11	36,21
<b>Node</b>	112	111	112	111	111	112
<b>Case</b>	ULS/89	ULS/62	ULS/97	ULS-/93	ULS-/101	ULS-/69
<b>Mode</b>						
<b>24 / M-AX</b>	2810,811986	196,732613	3921,704683	0,54	148,15	8,73
<b>Node</b>	114	114	113	113	114	113
<b>Case</b>	ULS/10-5	ULS/95	ULS/97	ULS-/95	ULS-/81	6
<b>Mode</b>						
<b>24 / MIN</b>	1658,874052	254,411297	3944,725926	0,45	363,74	45,65
<b>Node</b>	114	113	114	114	114	113
<b>Case</b>	ULS/73	ULS/95	ULS/97	ULS-/95	ULS-/101	ULS-/95
<b>Mode</b>						
<b>25 / MAX</b>	6887,102679	992,497464	3626,694040	0,93	268,49	48,75
<b>Node</b>	116	116	115	115	116	116
<b>Case</b>	ULS/97	ULS/10-1	ULS/95	ULS-/95	ULS-/81	ULS-/81
<b>Mode</b>						
<b>25 / MIN</b>	3898,965108	960,712016	3661,928089	0,98	457,81	148,66
<b>Node</b>	116	115	116	116	116	116
<b>Case</b>	ULS/89	ULS/10-1	ULS/99	ULS-/95	ULS-/101	ULS-/101
<b>Mode</b>						
<b>26 / MAX</b>	4656,106319	248,727824	3942,167829	0,68	227,49	39,47
<b>Node</b>	118	117	117	118	118	118
<b>Case</b>	ULS/97	ULS/97	ULS/95	ULS-/97	ULS-/81	ULS-/97
<b>Mode</b>						
<b>26 / MIN</b>	3007,153023	261,102269	3943,696598	0,69	419,94	26,53
<b>Node</b>	118	118	118	117	118	118
<b>Case</b>	ULS/89	ULS/97	ULS/97	ULS-/111	ULS-/101	ULS-/89
<b>Mode</b>						
<b>27 / MAX</b>	5887,787036	166,933787	3711,850969	0,83	184,13	46,23

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	120	119	119	119	120	120
<b>Case</b>	ULS/97	ULS/10-3	ULS/97	ULS-177	ULS-181	ULS-195
<b>Mode</b>						
<b>27 / MIN</b>	-2696,307724	-251,374485	-3710,242903	-0,40	-501,97	-51,08
<b>Node</b>	120	119	120	119	120	119
<b>Case</b>	ULS/89	ULS/61	ULS/97	ULS-195	ULS-1101	ULS-177
<b>Mode</b>						
<b>3-5 / M-A-X</b>	17088,452108	767,314421	2805,469569	56,77	65,91	1346,81
<b>Node</b>	75	75	75	76	75	76
<b>Case</b>	ULS/95	7	ULS/95	ULS-197	7	ULS-197
<b>Mode</b>						
<b>3-5 / M-IN</b>	7788,269642	5131,696417	1056,460118	90,96	634,61	1046,55
<b>Node</b>	76	75	76	76	75	75
<b>Case</b>	ULS/10-1	ULS/95	ULS/95	ULS-190	ULS-195	ULS-195
<b>Mode</b>						
<b>3-6 / M-A-X</b>	14780,379478	4376,369599	3807,513685	106,72	319,80	368,30
<b>Node</b>	77	78	77	78	77	78
<b>Case</b>	ULS/95	ULS/99	ULS/95	ULS-186	6	ULS-189
<b>Mode</b>						
<b>3-6 / M-IN</b>	7876,851394	1768,020941	1682,947446	62,51	768,36	1343,92
<b>Node</b>	78	77	77	78	77	78
<b>Case</b>	ULS/10-1	ULS/81	6	ULS-199	ULS-195	ULS-197
<b>Mode</b>						
<b>3-7 / M-AX</b>	4786,950019	2892,950841	173,219002	50,66	44,99	3817,66
<b>Node</b>	80	80	79	80	79	80
<b>Case</b>	ULS/97	ULS/81	ULS/77	ULS-191	ULS-195	ULS-1101
<b>Mode</b>						
<b>37 / MIN</b>	-646,700875	-1880,500892	-676,624021	-0,06	-68,07	-2368,68
<b>Node</b>	80	79	80	79	80	80
<b>Case</b>	7	ULS/91	ULS/95	5	ULS-145	ULS-181
<b>Mode</b>						
<b>3-8 / M-AX</b>	8570,913006	2942,680252	1186,266126	9,72	87,95	4808,62
<b>Node</b>	81	82	81	82	81	82

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/95	ULS/85	ULS/97	7	7	ULS- /99
<b>Mode</b>						
<b>3-8 / M-IN</b>	-	-	-	-	-	-
	1209,428307	2261,166007	355,157572	81,04	472,74	2252,29
<b>Node</b>	81	81	82	82	81	82
<b>Case</b>	7	ULS/91	ULS/45	ULS- /111	ULS- /99	ULS- /85
<b>Mode</b>						
<b>3-9 / M-AX</b>	-	-	-	-	-	-
	5769,715681	3195,081779	137,805992	20,31	21,29	4455,24
<b>Node</b>	84	84	84	84	84	84
<b>Case</b>	ULS/99	ULS/85	ULS/77	ULS- /111	ULS- /77	ULS- /99
<b>Mode</b>						
<b>39 / MIN</b>	-	-	-	0,01	-	-
	866,422590	1896,909927	367,830894	0,01	52,32	2705,15
<b>Node</b>	84	83	84	83	84	84
<b>Case</b>	7	ULS/91	ULS/45	9	ULS- /45	ULS- /85
<b>Mode</b>				SRS- S		
<b>4-0 / M-A-X</b>	-	-	-	-	-	-
	26254,807660	3050,023212	364,257681	10,98	285,04	5157,66
<b>Node</b>	85	86	86	85	85	86
<b>Case</b>	ULS/99	ULS/85	ULS/45	ULS- /93	ULS- /99	ULS- /99
<b>Mode</b>						
<b>4-0 / M-IN</b>	-	-	-	-	-	-
	3787,977168	2265,277056	2053,843009	14,65	56,53	2406,38
<b>Node</b>	85	85	85	85	85	86
<b>Case</b>	7	ULS/11- 1	ULS/99	ULS- /74	7	ULS- /85
<b>Mode</b>						
<b>4-1 / M-A-X</b>	-	-	-	-	-	-
	4699,291765	3035,280611	770,645305	23,51	102,60	4234,42
<b>Node</b>	88	88	88	88	88	88
<b>Case</b>	ULS/99	ULS/77	ULS/95	ULS- /78	ULS- /45	ULS- /95
<b>Mode</b>						
<b>41 / MIN</b>	-	-	-	-	-	-
	879,869736	1932,887853	138,525627	24,49	44,88	2568,99
<b>Node</b>	88	87	88	88	87	88
<b>Case</b>	7	ULS/91	7	ULS- /59	ULS- /95	ULS- /77
<b>Mode</b>						
<b>4-2 / M-A-X</b>	-	-	-	-	-	-
	17340,534517	949,073904	1036,834764	69,15	722,87	1323,78
<b>Node</b>	89	90	90	89	89	90

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/95	7	ULS/95	ULS-/89	ULS-/91	ULS-/99
<b>Mode</b>						
<b>4-2 / MIN</b>	-7649,706330	-6065,018828	-3392,281619	-124,59	-95,26	-1137,29
<b>Node</b>	90	89	89	89	89	89
<b>Case</b>	ULS/95	ULS/91	ULS/91	ULS-/92	7	ULS-/95
<b>Mode</b>						
<b>43 / MAX</b>	4319,740426	4775,285991	200,597687	94,94	44,20	564,81
<b>Node</b>	92	92	92	92	91	92
<b>Case</b>	ULS/99	ULS/91	6	ULS-/89	ULS-/91	7
<b>Mode</b>						
<b>4-3 / MIN</b>	-1111,718348	-2808,208706	-660,589882	-26,76	-63,72	-3951,11
<b>Node</b>	92	91	92	92	92	92
<b>Case</b>	6	ULS/81	ULS/95	ULS-/97	ULS-/45	ULS-/111
<b>Mode</b>						
<b>4-4 / MAX</b>	9505,319356	4825,985960	1088,570983	61,58	112,52	692,74
<b>Node</b>	93	94	93	93	93	94
<b>Case</b>	ULS/99	ULS/91	ULS/99	ULS-/97	6	7
<b>Mode</b>						
<b>4-4 / MIN</b>	-2015,502734	-3196,400815	-316,392995	-173,37	-472,60	-4137,66
<b>Node</b>	94	93	94	93	93	94
<b>Case</b>	ULS/85	ULS/77	ULS/95	ULS-/89	ULS-/99	ULS-/111
<b>Mode</b>						
<b>45 / MAX</b>	5225,669739	5082,078815	4,714562	33,35	24,90	710,07
<b>Node</b>	96	96	96	96	95	96
<b>Case</b>	ULS/99	ULS/91	7	ULS-/69	ULS-/95	7
<b>Mode</b>						
<b>45 / MIN</b>	-2206,743512	-2963,111076	-343,795259	-1,37	-42,15	-4303,30
<b>Node</b>	96	95	96	96	96	96
<b>Case</b>	ULS/85	ULS/77	ULS/95	ULS-/107	ULS-/95	ULS-/111
<b>Mode</b>						
<b>4-6 / MAX</b>	23729,556006	4789,873074	323,644835	51,84	310,85	769,12
<b>Node</b>	97	98	97	97	97	98
<b>Case</b>	ULS/99	ULS/91	6	ULS-/89	ULS-/99	7

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Mode</b>						
<b>4-6 / MIN</b>	-	-	-	-	-	-
3490,643850	3291,574543	2213,275143	37,39	46,44	4417,60	
<b>Node</b>	97	97	97	97	97	98
<b>Case</b>	6	ULS/77	ULS/99	ULS-/97	6	ULS-/111
<b>Mode</b>						
<b>47 / MAX</b>	4625,898480	4904,528652	787,703355	6,16	93,89	772,94
<b>Node</b>	100	100	100	100	100	100
<b>Case</b>	ULS/99	ULS/91	ULS/95	10	ULS-/45	7
<b>Mode</b>				SRS-S		
<b>4-7 / MIN</b>	-	-	-	-	-	-
1418,531668	2969,467520	394,630156	28,34	46,02	4279,74	
<b>Node</b>	100	99	100	100	100	100
<b>Case</b>	ULS/85	ULS/77	ULS/77	ULS-/73	ULS-/77	ULS-/111
<b>Mode</b>						
<b>4-8 / MAX</b>	16685,674792	4544,866141	2201,023485	136,78	743,65	388,27
<b>Node</b>	101	102	101	101	101	102
<b>Case</b>	ULS/95	ULS/99	ULS/77	ULS-/92	ULS-/95	ULS-/85
<b>Mode</b>						
<b>4-8 / MIN</b>	-	-	-	-	-	-
7676,373817	3054,713092	3195,541825	49,47	476,14	1356,00	
<b>Node</b>	101	101	101	102	101	102
<b>Case</b>	6	ULS/81	ULS/95	ULS-/85	6	ULS-/99
<b>Mode</b>						
<b>4-9 / MAX</b>	3720,687722	14802,862237	16569,598715	1798,39	750,54	1427,16
<b>Node</b>	89	75	75	89	89	75
<b>Case</b>	ULS/92	ULS/71	ULS/95	ULS-/95	ULS-/91	ULS-/92
<b>Mode</b>						
<b>4-9 / MIN</b>	-	-	-	-	-	-
1529,395002	19464,327216	18266,345888	1577,46	93,80	2246,67	
<b>Node</b>	75	89	89	75	89	89
<b>Case</b>	7	ULS/85	ULS/91	ULS-/99	7	ULS-/74
<b>Mode</b>						
<b>5-0 / MAX</b>	12396,819175	1966,925118	3585,006872	14,03	566,83	1491,54
<b>Node</b>	75	75	75	75	77	75

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/85	ULS/70	ULS/85	ULS- /91	ULS- /77	ULS- /92
<b>Mode</b>						
<b>5-0 / M-IN</b>	-	-	-	-	-	-
	13500,593194	1914,757525	4564,193638	5,46	561,32	562,84
<b>Node</b>	77	77	77	77	77	77
<b>Case</b>	ULS/81	ULS/94	ULS/95	ULS- /174	ULS- /95	ULS- /85
<b>Mode</b>						
<b>5-1 / M-A-X</b>						
	3860,652059	15340,233357	21461,462400	495,19	766,84	1327,01
<b>Node</b>	101	77	101	77	77	77
<b>Case</b>	ULS/92	ULS/81	ULS/95	ULS- /77	ULS- /95	ULS- /92
<b>Mode</b>						
<b>5-1 / M-IN</b>	-	-	-	-	-	-
	2191,374537	20396,775450	19487,071785	502,98	502,59	2220,94
<b>Node</b>	101	101	77	101	101	101
<b>Case</b>	ULS/77	ULS/67	ULS/95	ULS- /77	ULS- /77	ULS- /86
<b>Mode</b>						
<b>5-2 / M-A-X</b>						
	14644,606516	3119,929176	4615,618571	6,25	742,15	337,35
<b>Node</b>	89	89	101	101	101	101
<b>Case</b>	ULS/85	ULS/92	ULS/95	ULS- /126	ULS- /77	ULS- /99
<b>Mode</b>						
<b>5-2 / M-IN</b>	-	-	-	-	-	-
	17361,874038	3087,559301	4769,131423	27,85	546,28	2355,17
<b>Node</b>	101	101	101	89	101	89
<b>Case</b>	ULS/91	ULS/86	ULS/77	ULS- /83	ULS- /95	ULS- /74
<b>Mode</b>						
<b>5-3 / M-A-X</b>						
	2705,385877	7187,654556	8449,467641	255,82	1459,33	1626,56
<b>Node</b>	90	102	90	90	102	102
<b>Case</b>	6	ULS/99	ULS/95	ULS- /99	ULS- /95	ULS- /99
<b>Mode</b>						
<b>5-3 / M-IN</b>	-	-	-	-	-	-
	11178,612347	6869,955754	8467,763403	276,57	338,16	373,47
<b>Node</b>	90	90	102	102	90	102
<b>Case</b>	ULS/95	ULS/99	ULS/99	ULS- /99	6	6
<b>Mode</b>						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
5-4 / M-A-X	13354,046479	2428,622472	8248,937385	128,09	1214,34	486,36
<b>Node</b>	100	100	100	88	88	88
<b>Case</b>	ULS/59	ULS/95	ULS/95	ULS-/97	ULS-/77	ULS-/95
<b>Mode</b>						
5-4 / M-IN	-	-	-	-	-	-
8273,763274	2502,806850	8636,930794	144,56	2023,11	187,09	
<b>Node</b>	88	88	88	100	88	100
<b>Case</b>	ULS/85	ULS/95	ULS/99	ULS-/97	ULS-/95	ULS-/77
<b>Mode</b>						
5-5 / M-A-X	15178,655512	173,126348	8107,944381	18,21	1029,57	88,51
<b>Node</b>	98	86	98	98	86	86
<b>Case</b>	ULS/65	ULS/97	ULS/95	ULS-/22	ULS-/85	ULS-/43
<b>Mode</b>						
5-5 / M-IN	-	-	-	-	-	-
6670,213020	794,989053	9876,489381	76,70	2157,34	32,78	
<b>Node</b>	86	86	86	86	86	98
<b>Case</b>	ULS/93	ULS/43	ULS/99	ULS-/22	ULS-/99	ULS-/91
<b>Mode</b>						
5-6 / M-A-X	16599,748490	1578,044519	7857,045166	62,79	1186,30	107,05
<b>Node</b>	96	84	96	84	84	96
<b>Case</b>	ULS/65	ULS/45	ULS/95	ULS-/52	ULS-/77	ULS-/77
<b>Mode</b>						
5-6 / M-IN	-	-	-	-	-	-
7857,634921	1207,931170	9490,741960	14,76	1961,96	231,83	
<b>Node</b>	84	96	84	96	84	84
<b>Case</b>	ULS/93	ULS/95	ULS/95	ULS-/89	ULS-/95	ULS-/95
<b>Mode</b>						
5-7 / M-A-X	11937,870658	1116,368512	6306,129677	46,66	865,97	171,22
<b>Node</b>	94	82	94	82	82	82
<b>Case</b>	ULS/65	ULS/10-3	ULS/95	ULS-/43	6	ULS-/61
<b>Mode</b>						
5-7 / M-IN	-	-	-	-	-	-
8563,794493	1036,363260	8012,686226	24,48	1729,37	197,64	

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	94	82	82	94	82	82
<b>Case</b>	ULS/10-9	ULS/61	ULS/99	ULS-122	ULS-199	ULS-1103
<b>Mode</b>						
<b>5-8 / M-A-X</b>	14444,053627	1916,902876	7410,540202	97,56	948,28	218,11
<b>Node</b>	92	80	92	92	80	92
<b>Case</b>	ULS/69	ULS/95	ULS/10-1	ULS-197	6	ULS-177
<b>Mode</b>						
<b>5-8 / M-IN</b>	5326,484149	1933,851923	8441,856284	92,73	1907,67	347,53
<b>Node</b>	80	92	80	80	92	92
<b>Case</b>	6	ULS/95	ULS/97	ULS-1111	ULS-191	ULS-195
<b>Mode</b>						
<b>5-9 / M-A-X</b>	2605,753787	6969,233692	8543,419264	264,46	1489,73	388,64
<b>Node</b>	76	76	76	78	78	78
<b>Case</b>	6	ULS/97	ULS/10-1	ULS-197	ULS-1101	6
<b>Mode</b>						
<b>5-9 / M-IN</b>	11282,483223	7153,224416	8700,441363	248,39	323,38	1639,60
<b>Node</b>	76	78	78	76	76	78
<b>Case</b>	ULS/10-1	ULS/97	ULS/10-1	ULS-197	6	ULS-197
<b>Mode</b>						
<b>6-0 / M-A-X</b>	5130,540896	3239,100130	2114,571824	905,94	228,68	379,25
<b>Node</b>	100	102	100	100	100	102
<b>Case</b>	ULS/91	7	ULS/10-1	ULS-191	ULS-1101	7
<b>Mode</b>						
<b>6-0 / M-IN</b>	5694,054628	15393,549610	336,642814	2584,41	308,11	1550,63
<b>Node</b>	102	102	100	102	102	102
<b>Case</b>	ULS/99	ULS/95	7	ULS-199	ULS-195	ULS-195
<b>Mode</b>						
<b>6-1 / M-A-X</b>	5226,916199	15414,991109	2298,445866	2550,20	241,43	1546,96
<b>Node</b>	88	90	88	90	88	90
<b>Case</b>	ULS/95	ULS/95	ULS/10-1	ULS-199	ULS-1101	ULS-195
<b>Mode</b>						



Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
6-1 / M-IN	-	-	-	-	-	-
5441,391116	3257,556091	865,098988	469,81	331,78	381,05	
<b>Node</b>	90	90	88	88	90	90
<b>Case</b>	ULS/99	7	ULS/81	ULS-/101	ULS-/95	7
<b>Mode</b>						
6-2 / M-AX	-	-	-	-	-	-
9237,007360	4461,209614	1378,845105	1366,84	89,10	350,27	
<b>Node</b>	98	100	98	98	98	98
<b>Case</b>	ULS/73	ULS/81	ULS/95	ULS-/101	ULS-/45	ULS-/81
<b>Mode</b>						
6-2 / M-IN	-	-	-	-	-	-
1411,169863	4853,920536	1474,695882	1621,74	12,46	983,22	
<b>Node</b>	98	98	100	100	98	98
<b>Case</b>	ULS/10-5	ULS/65	ULS/95	ULS-/95	7	ULS-/101
<b>Mode</b>						
6-3 / M-AX	-	-	-	-	-	-
4159,917710	3869,316233	1742,485046	1600,97	139,95	927,50	
<b>Node</b>	86	86	86	88	86	86
<b>Case</b>	ULS/22	ULS/10	ULS/95	ULS-/95	ULS-/45	ULS-/101
<b>Mode</b>						
6-3 / M-IN	-	-	-	-	-	-
8481,380310	2875,320037	1684,461820	1462,28	74,32	334,65	
<b>Node</b>	86	86	88	86	86	86
<b>Case</b>	ULS/93	ULS/11-3	ULS/95	ULS-/97	6	ULS-/32
<b>Mode</b>						
6-4 / M-AX	-	-	-	-	-	-
10364,297339	5257,067953	1385,675833	1343,00	103,20	414,87	
<b>Node</b>	96	98	96	96	98	98
<b>Case</b>	ULS/73	ULS/65	ULS/91	ULS-/99	ULS-/59	ULS-/81
<b>Mode</b>						
6-4 / M-IN	-	-	-	-	-	-
1861,093199	5800,560210	1265,513492	1275,68	14,17	989,87	
<b>Node</b>	96	96	98	98	96	98
<b>Case</b>	ULS/10-5	ULS/65	ULS/91	ULS-/95	7	ULS-/101
<b>Mode</b>						
6-5 / M-AX	-	-	-	-	-	-
3631,691085	3491,700785	1945,789948	1388,70	199,48	918,04	

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	86	84	84	86	84	86
<b>Case</b>	ULS/22	ULS/10	ULS/45	ULS-/97	ULS-/45	ULS-/101
<b>Mode</b>						
<b>6-5 / M-IN</b>	9159,352745	3527,701572	1896,500593	1368,15	86,41	317,09
<b>Node</b>	84	86	86	84	84	86
<b>Case</b>	ULS/93	ULS/10	ULS/45	ULS-/97	6	ULS-/82
<b>Mode</b>						
<b>6-6 / M-A-X</b>	9721,887675	6441,734674	1065,675265	1509,80	107,64	318,92
<b>Node</b>	96	94	94	94	96	96
<b>Case</b>	ULS/73	ULS/10-1	ULS/59	ULS-/95	ULS-/91	ULS-/81
<b>Mode</b>						
<b>6-6 / M-IN</b>	2893,480930	3340,662681	1458,612831	1055,80	94,81	1209,83
<b>Node</b>	94	94	96	96	94	94
<b>Case</b>	ULS/99	ULS/81	ULS/11-1	ULS-/111	ULS-/97	ULS-/101
<b>Mode</b>						
<b>6-7 / M-A-X</b>	4044,775249	2649,145628	1195,189318	1024,18	172,03	1153,76
<b>Node</b>	84	82	84	84	84	82
<b>Case</b>	ULS/22	ULS/66	ULS/77	ULS-/97	ULS-/45	ULS-/101
<b>Mode</b>						
<b>6-7 / M-IN</b>	8888,832302	5521,692257	1817,560430	1688,74	91,42	360,16
<b>Node</b>	84	82	84	82	84	82
<b>Case</b>	ULS/93	ULS/10-9	ULS/95	ULS-/99	6	ULS-/81
<b>Mode</b>						
<b>6-8 / M-A-X</b>	8937,684080	3484,587387	1182,223697	1264,98	103,54	277,78
<b>Node</b>	94	94	92	92	94	92
<b>Case</b>	ULS/89	ULS/81	ULS/11-1	ULS-/95	ULS-/85	ULS-/61
<b>Mode</b>						
<b>6-8 / M-IN</b>	2516,735520	5020,081120	1170,319206	1153,29	46,53	1015,34
<b>Node</b>	94	92	94	94	94	94
<b>Case</b>	ULS/97	ULS/61	ULS/91	ULS-/101	ULS-/99	ULS-/101
<b>Mode</b>						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
6-9 / M-A-X	3981,688260	2986,772243	1433,645660	1211,72	76,90	904,38
Node	80	82	80	82	80	82
Case	ULS/10-1	ULS/10-9	ULS/95	ULS-/97	ULS-/95	ULS-/97
Mode						
6-9 / M-IN	8792,689868	2052,986465	963,409441	1257,50	85,13	269,71
Node	82	82	82	80	82	82
Case	ULS/93	ULS/66	ULS/10-1	ULS-/95	ULS-/93	ULS-/89
Mode						
7-0 / M-A-X	4644,897555	15553,141932	408,342146	2611,11	154,48	326,21
Node	92	78	78	78	92	78
Case	ULS/11-1	ULS/10-1	ULS/86	ULS-/97	ULS-/101	6
Mode						
7-0 / M-IN	5589,422616	3155,605476	1922,612397	936,49	314,42	1581,78
Node	78	78	92	92	78	78
Case	ULS/97	6	ULS/10-1	ULS-/91	ULS-/95	ULS-/101
Mode						
7-1 / M-A-X	4979,611429	2758,759010	670,332573	599,30	186,24	1573,58
Node	80	76	80	80	80	76
Case	ULS/10-1	6	6	ULS-/103	ULS-/101	ULS-/101
Mode						
7-1 / M-IN	5513,434150	15640,602164	2227,846734	2596,40	335,35	258,72
Node	76	76	80	76	76	76
Case	ULS/97	ULS/10-1	ULS/10-1	ULS-/97	ULS-/95	6
Mode						
77 / MAX	5300,501373	229,440445	4559,504855	2,83	220,94	27,03
Node	181	181	180	180	181	180
Case	ULS/95	ULS/10-1	ULS/10-1	ULS-/95	ULS-/77	6
Mode						
77 / MIN	2557,782764	233,197652	4553,437011	2,65	637,47	49,29
Node	181	180	181	181	180	181
Case	ULS/77	ULS/95	ULS/99	ULS-/95	ULS-/101	ULS-/95
Mode						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>78 / MAX</b>	4556,330058	438,894899	5451,269020	3,60	278,02	23,15
Node	153	153	152	152	153	153
Case	ULS/10-9	ULS/95	ULS/95	ULS-/95	ULS-/81	ULS-/77
Mode						
<b>78 / MIN</b>	-3480,511905	-473,473534	-5460,666936	-3,41	-623,84	-80,80
Node	153	152	153	153	153	152
Case	ULS/65	ULS/95	ULS/99	ULS-/95	ULS-/101	ULS-/95
Mode						
<b>79 / MAX</b>	9761,320020	301,294018	7002,797681	1,56	273,13	41,34
Node	154	154	154	155	155	155
Case	ULS/97	ULS/97	ULS/95	ULS-/97	ULS-/81	ULS-/97
Mode						
<b>79 / MIN</b>	-3212,605595	-294,980316	-6274,808258	-1,47	-994,92	-20,72
Node	155	155	155	154	154	155
Case	ULS/89	ULS/97	ULS/97	ULS-/111	ULS-/101	ULS-/89
Mode						
<b>80 / MAX</b>	8761,080990	194,637342	6451,997303	2,45	317,75	12,01
Node	157	157	156	156	157	157
Case	ULS/97	ULS/95	ULS/95	ULS-/95	ULS-/81	ULS-/77
Mode						
<b>80 / MIN</b>	-3718,638542	-178,796040	-6463,160830	-2,56	-907,50	-49,27
Node	157	156	157	157	157	157
Case	ULS/89	ULS/95	ULS/97	ULS-/95	ULS-/101	ULS-/95
Mode						
<b>81 / MAX</b>	2496,590665	172,210900	4756,659705	1,62	211,29	36,15
Node	158	158	158	159	159	158
Case	ULS/77	ULS/97	ULS/95	ULS-/97	ULS-/81	ULS-/97
Mode						
<b>81 / MIN</b>	-1765,380561	-188,172684	-4746,979050	-1,62	-339,98	-14,60
Node	159	159	159	158	159	159
Case	ULS/3	ULS/97	ULS/10-1	ULS-/97	ULS-/101	ULS-/89
Mode						
<b>82 / MAX</b>	10324,363067	366,679737	7489,049076	2,16	427,43	25,77
Node	161	161	160	160	161	161
Case	ULS/97	ULS/10-1	ULS/95	ULS-/101	ULS-/81	ULS-/81
Mode						
<b>82 / MIN</b>	-5477,442679	-366,250088	-7481,417146	-2,06	-1098,90	-56,74
Node	161	160	161	161	161	160
Case	ULS/89	ULS/10-1	ULS/97	ULS-/101	ULS-/101	ULS-/97
Mode						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>83 / MAX</b>	9039,706555	449,027803	7162,335193	3,13	393,77	73,07
<b>Node</b>	163	162	162	163	163	163
<b>Case</b>	ULS/97	ULS/10-1	ULS/95	ULS-/97	ULS-/89	ULS-/97
<b>Mode</b>						
<b>83 / MIN</b>	4953,068278	458,916144	7169,853640	2,88	1002,94	20,74
<b>Node</b>	163	163	163	162	163	163
<b>Case</b>	ULS/89	ULS/97	ULS/97	ULS-/101	ULS-/97	ULS-/89
<b>Mode</b>						
<b>84 / MAX</b>	9801,838230	439,338437	7285,785450	2,35	396,12	27,00
<b>Node</b>	165	165	164	164	165	165
<b>Case</b>	ULS/97	ULS/97	ULS/95	ULS-/111	ULS-/89	ULS-/89
<b>Mode</b>						
<b>84 / MIN</b>	5081,562562	451,995541	7324,216702	2,35	1053,02	70,38
<b>Node</b>	165	164	165	165	165	164
<b>Case</b>	ULS/89	ULS/97	ULS/97	ULS-/97	ULS-/97	ULS-/97
<b>Mode</b>						
<b>85 / MAX</b>	12412,647428	512,109052	8341,452142	3,61	359,31	77,51
<b>Node</b>	166	166	166	167	167	167
<b>Case</b>	ULS/97	ULS/10-1	ULS/95	ULS-/95	ULS-/81	ULS-/95
<b>Mode</b>						
<b>85 / MIN</b>	4484,264667	478,932745	7612,014007	3,75	1277,04	17,30
<b>Node</b>	167	167	167	166	166	166
<b>Case</b>	ULS/89	ULS/95	ULS/97	ULS-/95	ULS-/101	ULS-/78
<b>Mode</b>						
<b>86 / MAX</b>	3622,006086	299,890375	4780,238098	2,57	140,88	71,80
<b>Node</b>	168	168	168	169	169	169
<b>Case</b>	ULS/91	ULS/95	ULS/95	ULS-/95	6	ULS-/95
<b>Mode</b>						
<b>86 / MIN</b>	716,269403	314,822197	4262,594711	2,90	538,45	45,76
<b>Node</b>	169	169	169	168	168	168
<b>Case</b>	6	ULS/95	ULS/95	ULS-/95	ULS-/101	ULS-/77
<b>Mode</b>						
<b>8-7 / MAX</b>	19160,064364	1120,942463	6480,217009	7,20	293,50	187,53
<b>Node</b>	171	170	170	171	171	170
<b>Case</b>	ULS/97	ULS/95	ULS/10-1	ULS-/95	6	ULS-/95
<b>Mode</b>						
<b>8-7 / MIN</b>	3989,224248	1110,368155	6494,083541	7,42	1472,21	46,66

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	170	171	171	170	171	170
<b>Case</b>	ULS/90	ULS/95	ULS/10-1	ULS-/95	ULS-/101	6
<b>Mode</b>						
<b>88 / M-AX</b>	6576,386455	31,113891	1820,975013	6,09	500,65	3,08
<b>Node</b>	184	184	185	185	185	185
<b>Case</b>	ULS/95	ULS/91	6	ULS-/81	ULS-/95	ULS-/99
<b>Mode</b>						
<b>88 / MI-N</b>	-	-	-	-	-	-
	3224,489372	61,452662	7074,784566	2,52	852,03	6,90
<b>Node</b>	184	185	184	184	184	185
<b>Case</b>	6	ULS/85	ULS/95	ULS-/101	ULS-/95	ULS-/85
<b>Mode</b>						
<b>89 / MAX</b>	88,318770	29,784176	140,443054	1,28	67,39	3,40
<b>Node</b>	186	187	186	186	186	187
<b>Case</b>	7	ULS/91	6	ULS-/97	ULS-/101	ULS-/85
<b>Mode</b>						
<b>89 / MIN</b>	-	-	-	-	-	-
	1692,287974	58,725715	417,794000	3,05	45,30	2,21
<b>Node</b>	186	186	187	186	187	187
<b>Case</b>	ULS/95	ULS/85	ULS/10-1	ULS-/89	ULS-/95	ULS-/99
<b>Mode</b>						
<b>90 / MAX</b>	1055,828750	26,972497	464,856588	6,27	97,30	4,55
<b>Node</b>	188	188	188	188	186	186
<b>Case</b>	ULS/75	ULS/95	ULS/95	ULS-/89	ULS-/95	ULS-/85
<b>Mode</b>						
<b>90 / MIN</b>	-	-	-	-	-	-
	229,466440	78,096486	117,897808	3,61	28,69	5,36
<b>Node</b>	186	188	188	188	188	188
<b>Case</b>	ULS/1	ULS/77	6	ULS-/97	ULS-/101	ULS-/77
<b>Mode</b>						
<b>91 / M-AX</b>	18154,637449	62,957765	525,085322	4,03	497,04	1,16
<b>Node</b>	190	190	189	189	189	190
<b>Case</b>	ULS/99	ULS/89	6	ULS-/85	ULS-/99	ULS-/97
<b>Mode</b>						
<b>91 / MI-N</b>	-	-	-	-	-	-
	4277,575794	23,327081	3810,490558	0,90	143,59	8,42
<b>Node</b>	190	189	190	189	190	190
<b>Case</b>	6	ULS/91	ULS/95	ULS-/99	ULS-/95	ULS-/89
<b>Mode</b>						
<b>92 / MAX</b>	305,889562	38,459292	272,866660	0,29	127,28	1,87
<b>Node</b>	191	189	191	191	191	191
<b>Case</b>	6	ULS/91	6	ULS-/97	ULS-/99	ULS-/99
<b>Mode</b>						
<b>92 / MIN</b>	-	-	-	-	-	-
	683,423404	49,479815	937,048212	2,86	132,23	6,80
<b>Node</b>	189	191	189	191	189	191
<b>Case</b>	ULS/10-1	ULS/77	ULS/99	ULS-/89	ULS-/99	ULS-/85
<b>Mode</b>						



Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>93 / MAX</b>	0,385132	41,362366	34,386916	0,81	43,31	1,39
Node	192	193	192	192	192	193
Case	10	ULS/89	7	ULS- /95	ULS- /95	ULS- /77
Mode	SRSS					
<b>93 / MIN</b>	-	-	-	-	-	-
Node	1006,739808	45,112652	257,238436	2,87	25,94	1,13
Case	192	192	193	192	193	192
Case	ULS/45	ULS/91	ULS/95	ULS- /77	ULS- /45	ULS- /95
Mode						
<b>94 / MAX</b>	259,657013	39,938009	282,270592	3,17	64,19	1,75
Node	194	192	194	194	192	192
Case	ULS/11- 2	ULS/91	ULS/95	ULS- /77	ULS- /95	ULS- /77
Mode						
<b>94 / MIN</b>	-	-	-	-	-	-
Node	88,787927	47,348197	31,718626	0,98	13,54	1,37
Case	192	194	194	194	194	192
Case	ULS/36	ULS/85	7	ULS- /95	ULS- /50	ULS- /95
Mode						
<b>95 / MAX</b>	104,517659	54,121432	220,643732	4,64	50,64	2,58
Node	195	196	195	195	195	196
Case	6	ULS/77	7	ULS- /89	ULS- /95	ULS- /95
Mode						
<b>95 / MI- N</b>	-	-	-	-	-	-
Node	1418,141928	32,752329	1294,282061	0,83	230,93	8,73
Case	195	195	196	195	196	196
Case	ULS/99	ULS/91	ULS/99	ULS- /97	ULS- /99	ULS- /77
Mode						
<b>96 / MAX</b>	314,814080	35,526449	2751,139492	1,16	189,59	1,62
Node	195	195	197	195	195	197
Case	ULS/78	ULS/91	ULS/99	ULS- /95	ULS- /99	ULS- /95
Mode						
<b>96 / MIN</b>	-	-	-	-	-	-
Node	679,290367	49,288157	429,462707	5,35	389,34	7,65
Case	195	197	197	195	197	197
Case	ULS/45	ULS/85	7	ULS- /77	ULS- /99	ULS- /77
Mode						
<b>97 / MAX</b>	1245,385297	74,732349	36,810837	3,71	39,38	4,10
Node	199	199	198	198	198	198
Case	ULS/45	ULS/77	ULS/70	ULS- /99	ULS- /95	ULS- /85
Mode						
<b>97 / MIN</b>	-	-	-	-	-	-
Node	381,136367	25,482201	98,258038	6,36	9,86	4,85
Case	198	198	199	198	198	199
Case	7	ULS/95	ULS/99	ULS- /85	7	ULS- /77
Mode						
<b>98 / MAX</b>	278,241669	54,019510	59,324592	3,54	6,89	3,02
Node	200	198	200	200	198	200
Case	7	ULS/85	ULS/97	ULS- /89	ULS- /114	ULS- /85
Mode						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>98 / MIN</b>	-	-	-	-	-	-
	799,156697	33,930743	54,469222	1,58	11,87	2,24
<b>Node</b>	198	200	198	200	198	200
<b>Case</b>	ULS/95	ULS/91	ULS/22	ULS-/97	ULS-/21	ULS-/99
<b>Mode</b>						
<b>100 / M-AX</b>	-	-	-	-	-	-
	6120,633593	55,189845	8295,546647	2,55	491,16	3,47
<b>Node</b>	202	201	202	201	201	201
<b>Case</b>	ULS/95	ULS/85	ULS/95	ULS-/99	ULS-/95	ULS-/99
<b>Mode</b>						
<b>100 / MIN</b>	-	-	-	-	-	-
	4798,517651	37,889391	3850,254487	5,81	1014,13	5,99
<b>Node</b>	202	202	202	201	202	201
<b>Case</b>	ULS/77	ULS/91	6	ULS-/85	ULS-/95	ULS-/85
<b>Mode</b>						
<b>102 / M-AX</b>	-	-	-	-	-	-
	6469,795925	45,647672	767,483194	3,79	462,72	2,94
<b>Node</b>	204	203	204	203	203	203
<b>Case</b>	ULS/95	ULS/95	7	ULS-/85	ULS-/95	ULS-/95
<b>Mode</b>						
<b>102 / MI-N</b>	-	-	-	-	-	-
	761,707664	36,360870	7326,275208	3,24	882,21	9,74
<b>Node</b>	204	203	204	204	204	204
<b>Case</b>	7	6	ULS/95	ULS-/99	ULS-/95	ULS-/95
<b>Mode</b>						
<b>104 / MAX</b>	-	-	-	-	-	-
	749,506800	23,470829	1,221539	0,56	39,52	1,13
<b>Node</b>	205	206	205	205	205	206
<b>Case</b>	6	ULS/91	10	7	ULS-/71	6
<b>Mode</b>			SRSS			
<b>104 / MIN</b>	-	-	-	-	-	-
	1294,700142	32,969793	248,455875	3,32	29,12	1,20
<b>Node</b>	205	205	206	205	206	206
<b>Case</b>	ULS/45	ULS/89	ULS/45	ULS-/111	ULS-/45	ULS-/101
<b>Mode</b>						
<b>105 / MAX</b>	-	-	-	-	-	-
	932,360946	12,125250	264,557068	5,04	62,70	3,60
<b>Node</b>	207	205	207	207	205	205
<b>Case</b>	ULS/99	6	ULS/45	ULS-/111	ULS-/45	ULS-/111
<b>Mode</b>						
<b>105 / MIN</b>	-	-	-	-	-	-
	1440,374370	51,060731	0,009259	0,69	30,82	5,25
<b>Node</b>	205	207	207	207	207	207
<b>Case</b>	ULS/85	ULS/91	11	7	ULS-/69	ULS-/95
<b>Mode</b>			SRSS			
<b>106 / MAX</b>	-	-	-	-	-	-
	18670,520403	114,205359	497,989917	3,47	455,39	8,00
<b>Node</b>	209	208	209	209	208	208
<b>Case</b>	ULS/99	ULS/99	6	6	ULS-/95	ULS-/95
<b>Mode</b>						
<b>106 / MIN</b>	-	-	-	-	-	-
	3234,560003	27,176359	2851,900840	10,16	62,63	24,18
<b>Node</b>	209	208	209	209	208	209



Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	7	6	ULS/95	ULS-/95	7	ULS-/99
<b>Mode</b>						
<b>107 / MAX</b>	35,338770	26,964690	236,574782	2,35	141,10	0,72
<b>Node</b>	210	208	210	210	210	208
<b>Case</b>	5	ULS/91	7	ULS-/95	ULS-/99	7
<b>Mode</b>						
<b>107 / MI-N</b>	-	-	-	-	-	-
	516,828318	29,910098	1093,858069	1,91	162,76	4,44
<b>Node</b>	208	210	208	210	208	208
<b>Case</b>	ULS/18	ULS/81	ULS/99	ULS-/77	ULS-/99	ULS-/111
<b>Mode</b>						
<b>108 / MAX</b>	429,222771	27,177114	83,704617	0,51	57,93	1,16
<b>Node</b>	211	212	211	211	211	211
<b>Case</b>	6	ULS/91	6	7	ULS-/95	ULS-/99
<b>Mode</b>						
<b>108 / MIN</b>	-	-	-	-	-	-
	1078,264210	30,008411	331,855564	3,25	32,17	1,48
<b>Node</b>	211	211	212	211	212	212
<b>Case</b>	ULS/45	ULS/85	ULS/45	ULS-/99	ULS-/45	ULS-/99
<b>Mode</b>						
<b>109 / MAX</b>	142,922004	26,289159	349,396206	4,78	73,25	3,49
<b>Node</b>	213	211	213	213	211	211
<b>Case</b>	ULS/82	ULS/77	ULS/45	ULS-/99	ULS-/95	ULS-/95
<b>Mode</b>						
<b>109 / MIN</b>	-	-	-	-	-	-
	316,315608	36,856890	91,278982	0,69	22,85	5,68
<b>Node</b>	211	213	213	213	213	213
<b>Case</b>	ULS/18	ULS/91	6	7	ULS-/50	ULS-/99
<b>Mode</b>						
<b>110 / MAX</b>	207,081437	33,688693	204,070915	2,67	75,19	0,37
<b>Node</b>	214	215	214	214	214	214
<b>Case</b>	7	ULS/89	6	ULS-/85	ULS-/45	7
<b>Mode</b>						
<b>110 / M-IN</b>	-	-	-	-	-	-
	1408,104932	21,644133	1474,888514	1,22	262,08	5,35
<b>Node</b>	214	214	215	215	215	215
<b>Case</b>	ULS/95	ULS/91	ULS/99	ULS-/99	ULS-/99	ULS-/91
<b>Mode</b>						
<b>111 / M-AX</b>	355,840946	22,298030	2921,169004	2,10	185,98	0,84
<b>Node</b>	214	214	216	216	214	216
<b>Case</b>	6	ULS/85	ULS/99	ULS-/99	ULS-/95	7
<b>Mode</b>						
<b>111 / MI-N</b>	-	-	-	-	-	-
	1084,785318	31,501225	676,145018	3,26	414,19	5,54
<b>Node</b>	214	216	216	214	216	216
<b>Case</b>	ULS/45	ULS/91	7	ULS-/85	ULS-/99	ULS-/91
<b>Mode</b>						
<b>112 / MAX</b>	1238,674749	51,476422	102,124238	1,00	41,51	3,50
<b>Node</b>	218	218	217	217	217	217

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/99	ULS/91	ULS/78	7	ULS-/45	ULS-/95
<b>Mode</b>						
<b>112 / MIN</b>	-	-	-	-	-	-
	726,376187	11,525079	132,452139	5,03	19,25	5,41
<b>Node</b>	217	217	218	217	217	218
<b>Case</b>	ULS/85	6	ULS/3	ULS-/111	7	ULS-/95
<b>Mode</b>						
<b>113 / MAX</b>	394,729932	33,627553	114,703841	3,26	19,09	1,30
<b>Node</b>	219	217	219	219	217	219
<b>Case</b>	7	ULS/89	ULS/21	ULS-/111	ULS-/69	ULS-/89
<b>Mode</b>						
<b>113 / MIN</b>	-	-	-	-	-	-
	990,240449	23,482091	96,964928	0,46	14,05	0,93
<b>Node</b>	217	219	217	219	219	219
<b>Case</b>	ULS/45	ULS/91	ULS/94	7	ULS-/20	ULS-/97
<b>Mode</b>						
<b>114 / M-AX</b>	7501,706210	19,477969	8308,795913	4,21	509,44	4,70
<b>Node</b>	220	221	220	220	221	220
<b>Case</b>	ULS/11-1	6	ULS/95	ULS-/95	ULS-/111	7
<b>Mode</b>						
<b>114 / MIN</b>	-	-	-	-	-	-
	1061,237703	56,434220	1446,760191	2,45	992,89	11,20
<b>Node</b>	220	220	220	220	220	220
<b>Case</b>	7	ULS/91	7	6	ULS-/95	ULS-/95
<b>Mode</b>						
<b>131 / M-AX</b>	1272,921191	39,467887	297,493453	1,97	33,18	19,42
<b>Node</b>	223	223	222	223	223	223
<b>Case</b>	ULS/95	ULS/81	ULS/45	6	ULS-/77	ULS-/101
<b>Mode</b>						
<b>131 / MIN</b>	-	-	-	-	-	-
	513,971332	88,752369	401,169953	11,75	76,38	4,71
<b>Node</b>	222	222	223	223	223	222
<b>Case</b>	6	ULS/10-1	ULS/95	ULS-/101	ULS-/95	ULS-/95
<b>Mode</b>						
<b>133 / M-AX</b>	2491,738816	45,889037	581,768180	6,73	61,28	12,22
<b>Node</b>	226	226	226	226	226	226
<b>Case</b>	ULS/95	ULS/85	ULS/81	ULS-/77	ULS-/81	ULS-/95
<b>Mode</b>						
<b>133 / MI-N</b>	-	-	-	-	-	-
	1481,233493	32,867774	550,612887	12,39	34,04	8,28
<b>Node</b>	225	225	226	226	225	226
<b>Case</b>	ULS/77	ULS/99	ULS/10-1	ULS-/95	ULS-/75	ULS-/77
<b>Mode</b>						
<b>134 / M-AX</b>	1185,411565	18,159606	377,676136	10,26	51,68	8,42
<b>Node</b>	225	225	225	227	225	227
<b>Case</b>	ULS/97	ULS/11-3	ULS/95	ULS-/101	ULS-/45	ULS-/95

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Mode</b>						
<b>134 / MIN</b>	-	-	-	-	-	-
	846,506519	45,313911	493,105868	6,82	61,53	8,64
<b>Node</b>	225	227	225	227	225	227
<b>Case</b>	ULS/89	ULS/61	ULS/77	ULS-/81	ULS-/77	ULS-/77
<b>Mode</b>						
<b>135 / M-AX</b>	-	-	-	-	-	-
	3265,418998	41,135449	804,651065	6,91	80,60	16,87
<b>Node</b>	229	229	228	229	229	229
<b>Case</b>	ULS/95	ULS/81	ULS/11-1	ULS-/85	ULS-/91	ULS-/99
<b>Mode</b>						
<b>135 / M-IN</b>	-	-	-	-	-	-
	2031,421311	55,464111	145,715100	16,75	103,68	9,00
<b>Node</b>	228	228	229	229	228	229
<b>Case</b>	ULS/77	ULS/10-1	ULS/16	ULS-/99	ULS-/111	ULS-/85
<b>Mode</b>						
<b>136 / MAX</b>	-	-	-	-	-	-
	808,069427	32,432568	97,191024	14,39	63,05	13,31
<b>Node</b>	230	228	228	230	230	230
<b>Case</b>	ULS/97	ULS/97	ULS/44	ULS-/99	ULS-/91	ULS-/97
<b>Mode</b>						
<b>136 / MI-N</b>	-	-	-	-	-	-
	1104,475530	44,899500	859,103786	6,25	109,85	7,58
<b>Node</b>	228	230	228	230	228	230
<b>Case</b>	ULS/89	ULS/89	ULS/91	ULS-/85	ULS-/93	ULS-/89
<b>Mode</b>						
<b>137 / M-AX</b>	-	-	-	-	-	-
	1364,460854	46,979154	875,637444	7,48	95,89	13,85
<b>Node</b>	232	232	232	232	232	232
<b>Case</b>	ULS/95	ULS/89	ULS/93	ULS-/85	ULS-/91	ULS-/97
<b>Mode</b>						
<b>137 / MI-N</b>	-	-	-	-	-	-
	1999,563853	38,797611	139,371362	14,29	89,01	8,96
<b>Node</b>	231	231	232	232	231	232
<b>Case</b>	ULS/77	ULS/97	ULS/22	ULS-/99	ULS-/93	ULS-/89
<b>Mode</b>						
<b>138 / M-AX</b>	-	-	-	-	-	-
	760,710238	30,342120	188,397154	13,01	81,41	11,89
<b>Node</b>	233	231	231	233	233	233
<b>Case</b>	ULS/95	ULS/10-1	ULS/22	ULS-/99	ULS-/91	ULS-/97
<b>Mode</b>						
<b>138 / MI-N</b>	-	-	-	-	-	-
	1508,164889	46,097322	828,020459	7,36	105,09	8,99
<b>Node</b>	231	233	231	233	231	233
<b>Case</b>	ULS/77	ULS/81	ULS/93	ULS-/85	ULS-/93	ULS-/89
<b>Mode</b>						
<b>139 / MAX</b>	-	-	-	-	-	-
	958,747216	45,702988	811,926107	6,66	87,17	15,40
<b>Node</b>	235	235	235	235	235	235
<b>Case</b>	ULS/99	ULS/89	ULS/91	ULS-/85	ULS-/91	ULS-/97
<b>Mode</b>						
<b>139 / MI-N</b>	-	-	-	-	-	-
	1816,199102	42,442192	209,122839	16,06	80,36	8,23

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	234	234	234	235	234	235
<b>Case</b>	ULS/85	ULS/97	ULS/22	ULS-/99	ULS-/93	ULS-/89
<b>Mode</b>						
<b>140 / M-AX</b>	2172,154076	40,784506	272,742189	15,88	61,18	14,97
<b>Node</b>	236	234	236	236	236	236
<b>Case</b>	ULS/95	ULS/97	ULS/45	ULS-/99	ULS-/83	ULS-/97
<b>Mode</b>						
<b>140 / MI-N</b>	-	-	-	-	-	-
	1304,687005	44,749422	881,726546	6,59	109,83	8,17
<b>Node</b>	234	236	234	236	234	236
<b>Case</b>	ULS/77	ULS/89	ULS/91	ULS-/85	ULS-/91	ULS-/89
<b>Mode</b>						
<b>141 / MAX</b>	382,181067	39,782210	651,165734	6,51	77,78	7,92
<b>Node</b>	237	238	238	238	237	238
<b>Case</b>	ULS/10-5	ULS/81	ULS/91	ULS-/81	ULS-/45	ULS-/101
<b>Mode</b>						
<b>141 / MI-N</b>	-	-	-	-	-	-
	1628,439662	17,881167	513,667308	10,51	42,61	7,70
<b>Node</b>	237	237	237	238	237	238
<b>Case</b>	ULS/73	ULS/91	ULS/45	ULS-/101	6	ULS-/81
<b>Mode</b>						
<b>142 / M-AX</b>	2878,193417	43,867264	642,690032	14,59	31,35	14,96
<b>Node</b>	239	237	239	239	239	239
<b>Case</b>	ULS/95	ULS/95	ULS/10-1	ULS-/95	ULS-/81	ULS-/95
<b>Mode</b>						
<b>142 / MIN</b>	-	-	-	-	-	-
	964,256443	44,724143	578,890947	7,04	71,97	8,59
<b>Node</b>	237	239	237	239	237	239
<b>Case</b>	6	ULS/77	ULS/91	ULS-/77	ULS-/59	ULS-/77
<b>Mode</b>						
<b>144 / M-AX</b>	1067,310839	87,947556	451,360412	11,61	24,01	19,17
<b>Node</b>	241	240	241	241	241	241
<b>Case</b>	ULS/95	ULS/95	ULS/95	ULS-/95	6	ULS-/95
<b>Mode</b>						
<b>144 / MIN</b>	-	-	-	-	-	-
	237,232283	35,823734	271,119705	2,50	76,82	4,75
<b>Node</b>	240	241	240	241	241	240
<b>Case</b>	6	ULS/77	ULS/45	7	ULS-/95	ULS-/95
<b>Mode</b>						
<b>145 / M-AX</b>	1423,551762	88,954871	368,398296	11,82	20,33	4,70
<b>Node</b>	244	243	243	244	244	243
<b>Case</b>	ULS/95	ULS/10-1	ULS/95	ULS-/101	7	ULS-/101
<b>Mode</b>						
<b>145 / MIN</b>	-	-	-	-	-	-
	159,010293	57,138270	470,324379	2,37	83,90	19,45
<b>Node</b>	243	243	244	244	244	244

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	7	ULS/81	ULS/95	6	ULS-/95	ULS-/101
<b>Mode</b>						
<b>147 / M-AX</b>	2368,479878	67,194606	213,117681	12,43	44,31	2,09
<b>Node</b>	247	247	246	247	246	247
<b>Case</b>	ULS/95	ULS/91	ULS/95	ULS-/111	ULS-/61	7
<b>Mode</b>						
<b>147 / MIN</b>	-	-	-	-	-	-
	348,295242	29,436315	538,391364	2,03	46,16	13,05
<b>Node</b>	247	246	247	247	247	247
<b>Case</b>	7	ULS/77	ULS/10-1	7	ULS-/71	ULS-/111
<b>Mode</b>						
<b>148 / MAX</b>	1175,924678	28,903838	435,241311	1,60	64,35	1,37
<b>Node</b>	246	246	246	248	246	248
<b>Case</b>	ULS/11-1	ULS/65	ULS/59	7	ULS-/59	ULS-/82
<b>Mode</b>						
<b>148 / MI-N</b>	-	-	-	-	-	-
	406,538341	62,968261	262,632148	10,58	18,75	12,29
<b>Node</b>	248	248	248	248	248	248
<b>Case</b>	ULS/90	ULS/93	ULS/10-1	ULS-/111	6	ULS-/91
<b>Mode</b>						
<b>149 / M-AX</b>	2924,342981	54,478961	802,956572	14,60	91,88	2,79
<b>Node</b>	250	250	249	250	249	250
<b>Case</b>	ULS/95	ULS/91	ULS/99	ULS-/95	ULS-/85	7
<b>Mode</b>						
<b>149 / MI-N</b>	-	-	-	-	-	-
	436,726894	38,648439	783,048526	2,69	106,85	15,13
<b>Node</b>	250	249	250	250	249	250
<b>Case</b>	7	ULS/89	ULS/69	7	ULS-/99	ULS-/111
<b>Mode</b>						
<b>150 / M-AX</b>	1445,681327	23,668796	790,541954	2,19	104,98	2,06
<b>Node</b>	249	249	249	251	249	251
<b>Case</b>	ULS/91	ULS/81	ULS/89	7	ULS-/89	7
<b>Mode</b>						
<b>150 / MI-N</b>	-	-	-	-	-	-
	202,576658	72,810547	280,721559	12,90	60,22	13,11
<b>Node</b>	251	251	249	251	251	251
<b>Case</b>	7	ULS/91	ULS/97	ULS-/111	ULS-/89	ULS-/111
<b>Mode</b>						
<b>151 / M-AX</b>	2226,779104	64,889536	493,407084	13,65	98,20	2,47
<b>Node</b>	252	253	252	253	252	253
<b>Case</b>	ULS/59	ULS/91	ULS/97	ULS-/95	ULS-/89	7
<b>Mode</b>						
<b>151 / MIN</b>	-	-	-	-	-	-
	63,464520	33,620625	940,090620	2,46	98,22	14,12
<b>Node</b>	253	252	253	253	253	253
<b>Case</b>	7	ULS/81	ULS/69	7	ULS-/85	ULS-/111

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Mode</b>						
<b>152 / M-AX</b>	1430,844276	30,152726	946,882967	2,23	125,52	2,08
<b>Node</b>	252	252	252	254	252	254
<b>Case</b>	ULS/75	ULS/89	ULS/73	7	ULS-/73	7
<b>Mode</b>						
<b>152 / MI-N</b>	-	-	-	-	-	-
	335,928799	65,260385	370,317510	12,63	68,79	12,57
<b>Node</b>	254	254	254	254	254	254
<b>Case</b>	ULS/62	ULS/91	ULS/97	ULS-/111	ULS-/89	ULS-/91
<b>Mode</b>						
<b>153 / M-AX</b>	2052,832830	65,495807	301,604776	14,39	87,58	2,59
<b>Node</b>	255	256	255	256	255	256
<b>Case</b>	ULS/91	ULS/91	ULS/97	ULS-/95	ULS-/73	7
<b>Mode</b>						
<b>153 / MIN</b>	-	-	-	-	-	-
	41,153427	33,144167	843,453124	2,63	87,06	14,32
<b>Node</b>	256	255	256	256	256	256
<b>Case</b>	4	ULS/81	ULS/89	7	ULS-/89	ULS-/111
<b>Mode</b>						
<b>154 / M-AX</b>	1782,520980	39,186069	910,534608	2,56	116,91	2,49
<b>Node</b>	257	255	255	257	255	257
<b>Case</b>	ULS/95	ULS/89	ULS/85	7	ULS-/89	7
<b>Mode</b>						
<b>154 / MI-N</b>	-	-	-	-	-	-
	388,634843	59,763719	575,180343	14,39	63,18	13,93
<b>Node</b>	257	257	255	257	257	257
<b>Case</b>	7	ULS/91	ULS/99	ULS-/95	ULS-/85	ULS-/111
<b>Mode</b>						
<b>155 / M-AX</b>	1529,940396	65,294619	305,049406	10,84	76,56	1,59
<b>Node</b>	258	259	259	259	258	259
<b>Case</b>	ULS/93	ULS/91	ULS/10-1	ULS-/111	ULS-/45	7
<b>Mode</b>						
<b>155 / MIN</b>	-	-	-	-	-	-
	431,898454	24,478347	582,648633	2,02	55,52	12,47
<b>Node</b>	259	258	259	259	259	259
<b>Case</b>	ULS/20	ULS/81	ULS/81	7	ULS-/81	ULS-/91
<b>Mode</b>						
<b>156 / MAX</b>	2876,096848	32,083967	685,778385	2,68	77,48	2,77
<b>Node</b>	260	258	260	260	258	260
<b>Case</b>	ULS/95	ULS/77	ULS/10-1	7	ULS-/77	7
<b>Mode</b>						
<b>156 / MI-N</b>	-	-	-	-	-	-
	541,763746	67,635332	404,063621	14,35	42,88	15,42
<b>Node</b>	260	260	258	260	260	260
<b>Case</b>	7	ULS/91	ULS/95	ULS-/95	ULS-/18	ULS-/111
<b>Mode</b>						
<b>158 / MAX</b>	1048,149268	58,687767	475,627664	2,51	21,11	4,43

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Node</b>	262	261	262	262	261	261
<b>Case</b>	ULS/95	ULS/77	ULS/95	7	7	ULS-/95
<b>Mode</b>						
<b>158 / MI-N</b>	-	-	-	-	-	-
	249,723252	87,062090	279,873929	11,67	79,98	19,22
<b>Node</b>	262	261	261	262	262	262
<b>Case</b>	6	ULS/95	ULS/45	ULS-/95	ULS-/95	ULS-/95
<b>Mode</b>						
<b>1-7-1 / M-A-X</b>	8320,655233	270,230657	15564,707578	13,03	1606,39	20,82
<b>Node</b>	244	245	244	245	244	245
<b>Case</b>	ULS/97	ULS/97	ULS/95	ULS-/97	ULS-/95	ULS-/97
<b>Mode</b>						
<b>171 / MIN</b>	-	-	-	-	-	-
	1475,041129	54,372270	3388,602266	2,67	346,52	26,33
<b>Node</b>	244	245	244	245	244	244
<b>Case</b>	7	7	6	7	6	ULS-/97
<b>Mode</b>						
<b>172 / MAX</b>	1836,529830	169,116315	7960,513323	2,43	692,03	12,30
<b>Node</b>	247	264	247	264	247	264
<b>Case</b>	ULS/81	ULS/97	ULS/95	ULS-/105	ULS-/95	ULS-/97
<b>Mode</b>						
<b>172 / M-IN</b>	-	-	-	-	-	-
	3821,411133	30,107318	1906,858789	2,02	145,90	4,08
<b>Node</b>	264	264	264	264	247	247
<b>Case</b>	ULS/10-1	7	ULS/11-1	ULS-/73	ULS-/78	ULS-/113
<b>Mode</b>						
<b>173 / MAX</b>	1450,232735	120,122949	2111,608941	1,03	129,88	7,14
<b>Node</b>	248	264	264	248	248	264
<b>Case</b>	ULS/10-9	ULS/95	ULS/91	ULS-/1	ULS-/70	ULS-/95
<b>Mode</b>						
<b>173 / MI-N</b>	-	-	-	-	-	-
	421,000649	89,913561	3163,713918	0,20	229,87	6,22
<b>Node</b>	248	248	248	264	248	248
<b>Case</b>	ULS/66	ULS/97	ULS/93	2	ULS-/93	ULS-/89
<b>Mode</b>						
<b>174 / MAX</b>	1535,838828	132,165534	9082,996164	4,43	832,30	9,35
<b>Node</b>	250	265	250	265	250	265
<b>Case</b>	ULS/93	ULS/97	ULS/97	ULS-/97	ULS-/97	ULS-/97
<b>Mode</b>						
<b>174 / MIN</b>	-	-	-	-	-	-
	1212,763474	23,392530	1804,070563	1,22	171,67	10,32
<b>Node</b>	265	250	265	265	250	250
<b>Case</b>	ULS/99	ULS/66	ULS/73	ULS-/90	ULS-/90	ULS-/101
<b>Mode</b>						

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>175 / MAX</b>	2007,509760	171,685230	1698,917708	1,58	133,94	11,46
Node	251	265	265	265	251	265
Case	ULS/69	ULS/97	ULS/73	ULS-/89	7	ULS-/95
Mode						
<b>175 / M-IN</b>	-	-	-	-	-	-
	2412,358222	37,897304	8408,731968	2,88	760,18	3,77
Node	265	251	251	265	251	251
Case	ULS/99	ULS/95	ULS/97	ULS-/97	ULS-/97	ULS-/91
Mode						
<b>176 / MAX</b>	1825,721872	169,327595	8853,344854	2,66	787,82	11,60
Node	266	266	253	266	253	266
Case	ULS/85	ULS/97	ULS/97	ULS-/105	ULS-/97	ULS-/97
Mode						
<b>176 / M-IN</b>	-	-	-	-	-	-
	3015,156772	30,588371	2412,254820	2,37	186,77	4,84
Node	266	266	266	266	253	253
Case	ULS/99	7	ULS/59	ULS-/73	ULS-/90	ULS-/105
Mode						
<b>177 / MAX</b>	2468,574128	160,092651	2265,827489	1,56	156,13	10,66
Node	254	266	266	266	254	266
Case	ULS/87	ULS/97	ULS/59	ULS-/73	ULS-/90	ULS-/99
Mode						
<b>177 / M-IN</b>	-	-	-	-	-	-
	1929,106930	63,716306	6268,194448	1,57	543,93	4,80
Node	266	254	254	266	254	254
Case	ULS/99	ULS/95	ULS/97	ULS-/105	ULS-/97	ULS-/93
Mode						
<b>178 / MAX</b>	1327,370323	173,438883	8733,023849	2,83	788,33	11,88
Node	256	267	256	267	256	267
Case	ULS/71	ULS/97	ULS/97	ULS-/97	ULS-/97	ULS-/99
Mode						
<b>178 / M-IN</b>	-	-	-	-	-	-
	2022,361456	30,943931	2176,568925	1,86	174,63	4,80
Node	267	267	267	267	256	256
Case	ULS/99	7	ULS/59	ULS-/89	ULS-/90	ULS-/111
Mode						
<b>179 / MAX</b>	2618,786909	167,320805	2052,418340	2,06	199,21	11,47
Node	267	267	257	267	257	267
Case	ULS/85	ULS/97	ULS/90	ULS-/73	ULS-/90	ULS-/97
Mode						
<b>179 / M-IN</b>	-	-	-	-	-	-
	3464,781728	29,897488	9013,062510	2,63	801,79	4,23
Node	267	267	257	267	257	257
Case	ULS/99	7	ULS/97	ULS-/105	ULS-/97	ULS-/105
Mode						



Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>180 / MAX</b>	1147,273893	134,117318	3214,707912	0,34	226,50	8,11
Node	259	268	259	259	259	259
Case	ULS/71	ULS/10-1	ULS/91	7	ULS-/91	ULS-/99
Mode						
<b>180 / MIN</b>	-782,091047	-134,736204	-2032,651412	-2,01	-46,54	-7,16
Node	268	259	268	259	259	259
Case	ULS/10-7	ULS/95	ULS/91	ULS-/95	ULS-/90	ULS-/85
Mode						
<b>181 / MAX</b>	2825,335153	181,450513	1936,088678	1,88	168,83	13,84
Node	268	268	268	268	260	268
Case	ULS/77	ULS/97	ULS/95	ULS-/89	7	ULS-/97
Mode						
<b>181 / MIN</b>	-4070,330527	-32,110597	-10020,444058	-3,51	-887,95	-7,97
Node	268	268	260	268	260	260
Case	ULS/95	7	ULS/95	ULS-/97	ULS-/101	ULS-/101
Mode						
<b>183 / MAX</b>	8219,486538	270,728085	3579,266776	2,54	357,37	20,87
Node	262	263	262	263	262	263
Case	ULS/99	ULS/99	6	6	6	ULS-/99
Mode						
<b>183 / MIN</b>	-1629,975035	-45,905716	-15883,189038	-12,82	-1609,98	-26,16
Node	262	263	262	263	262	262
Case	7	6	ULS/95	ULS-/99	ULS-/95	ULS-/99
Mode						
<b>184 / MAX</b>	8321,299084	319,437750	2828,509649	2,68	298,28	25,33
Node	223	224	223	224	223	224
Case	ULS/97	ULS/97	7	7	7	ULS-/97
Mode						
<b>184 / MIN</b>	-2056,017989	-109,229014	-15532,973731	-13,12	-1653,66	-15,14
Node	223	223	223	224	223	223
Case	ULS/89	ULS/95	ULS/95	ULS-/97	ULS-/101	ULS-/97
Mode						
<b>185 / MAX</b>	555,485870	240,549569	2382,401407	1,07	195,10	17,54
Node	269	269	226	269	226	269
Case	7	ULS/10-1	ULS/77	ULS-/74	ULS-/77	ULS-/101
Mode						
<b>185 / MIN</b>	-4253,025868	-175,758614	-7916,016462	-2,27	-693,52	-5,03
Node	269	226	226	269	226	269

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/10-1	ULS/95	ULS/95	ULS-/105	ULS-/95	ULS-/81
<b>Mode</b>						
<b>186 / MAX</b>	1225,718214	133,082092	2344,603118	0,24	281,72	9,34
<b>Node</b>	227	227	227	227	227	269
<b>Case</b>	ULS/10-3	ULS/97	ULS/10-7	6	ULS-/69	ULS-/95
<b>Mode</b>						
<b>186 / MIN</b>	-	-	-	-	-	-
	1312,668871	149,682535	3137,911938	1,24	186,90	6,15
<b>Node</b>	227	269	227	227	227	269
<b>Case</b>	ULS/61	ULS/95	ULS/69	ULS-/97	ULS-/107	ULS-/77
<b>Mode</b>						
<b>187 / MAX</b>	342,018050	198,853183	2702,042520	1,56	230,47	14,78
<b>Node</b>	229	270	229	270	229	270
<b>Case</b>	2	ULS/10-1	ULS/77	ULS-/74	ULS-/89	ULS-/97
<b>Mode</b>						
<b>187 / M-IN</b>	-	-	-	-	-	-
	2267,071019	89,379055	9380,692764	4,23	862,70	5,83
<b>Node</b>	270	229	229	270	229	270
<b>Case</b>	ULS/91	ULS/95	ULS/95	ULS-/105	ULS-/97	ULS-/89
<b>Mode</b>						
<b>188 / MAX</b>	395,508281	173,409857	8085,823809	2,17	160,33	16,06
<b>Node</b>	270	230	230	270	230	270
<b>Case</b>	7	ULS/97	ULS/97	ULS-/105	ULS-/90	ULS-/99
<b>Mode</b>						
<b>188 / MIN</b>	-	-	-	-	-	-
	2686,744295	227,427996	1849,338398	0,85	724,85	4,65
<b>Node</b>	270	270	230	270	230	270
<b>Case</b>	ULS/99	ULS/97	ULS/89	ULS-/74	ULS-/97	ULS-/85
<b>Mode</b>						
<b>189 / MAX</b>	411,046073	239,020266	2670,515381	1,93	229,68	16,80
<b>Node</b>	271	271	232	232	232	271
<b>Case</b>	7	ULS/10-1	ULS/89	ULS-/22	ULS-/90	ULS-/101
<b>Mode</b>						
<b>189 / MIN</b>	-	-	-	-	-	-
	3139,469984	179,214618	8624,797088	2,47	780,37	6,12
<b>Node</b>	271	232	232	271	232	271
<b>Case</b>	ULS/99	ULS/95	ULS/97	ULS-/105	ULS-/97	ULS-/81
<b>Mode</b>						
<b>190 / MAX</b>	324,253181	167,796471	6166,569341	1,51	212,10	14,75
<b>Node</b>	233	233	233	271	233	271
<b>Case</b>	ULS/10-9	ULS/99	ULS/97	ULS-/105	ULS-/89	ULS-/99
<b>Mode</b>						
<b>190 / MIN</b>	-	-	-	-	-	-
	2739,783909	212,911458	2542,116297	1,70	540,38	6,07
<b>Node</b>	271	271	233	271	233	271

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
<b>Case</b>	ULS/12	ULS/97	ULS/89	ULS- /22	ULS- /97	ULS- /85
<b>Mode</b>						
<b>191 / MAX</b>	776,155010	241,142818	2733,988646	1,40	232,42	17,46
<b>Node</b>	235	272	235	235	235	272
<b>Case</b>	ULS/10- 9	ULS/97	ULS/89	ULS- /22	ULS- /89	ULS- /99
<b>Mode</b>						
<b>191 / MIN</b>	-	-	-	-	-	-
	2834,398563	173,145581	8987,450551	2,54	810,61	5,65
<b>Node</b>	272	235	235	272	235	272
<b>Case</b>	ULS/48	ULS/99	ULS/97	ULS- /105	ULS- /97	ULS- /85
<b>Mode</b>						
<b>192 / MAX</b>	558,035465	180,674012	9035,840896	2,46	235,78	17,37
<b>Node</b>	272	236	236	272	236	272
<b>Case</b>	7	ULS/95	ULS/97	ULS- /105	ULS- /90	ULS- /97
<b>Mode</b>						
<b>192 / MIN</b>	-	-	-	-	-	-
	3692,899227	240,872160	2323,402568	2,05	807,82	5,55
<b>Node</b>	272	272	272	236	236	272
<b>Case</b>	ULS/99	ULS/97	ULS/45	ULS- /22	ULS- /97	ULS- /89
<b>Mode</b>						
<b>193 / MAX</b>	707,089291	169,485563	2036,502309	2,26	145,37	10,56
<b>Node</b>	238	273	238	238	238	273
<b>Case</b>	ULS/10- 1	ULS/99	ULS/73	ULS- /97	ULS- /73	ULS- /95
<b>Mode</b>						
<b>193 / MIN</b>	-	-	-	-	-	-
	1028,462853	169,772885	1525,113931	0,80	122,84	5,46
<b>Node</b>	273	238	238	238	273	273
<b>Case</b>	ULS/99	ULS/97	ULS/10- 5	6	ULS- /97	ULS- /77
<b>Mode</b>						
<b>194 / MAX</b>	789,867824	171,186334	9501,208021	3,09	167,99	19,86
<b>Node</b>	273	239	239	273	239	273
<b>Case</b>	7	ULS/95	ULS/95	ULS- /97	7	ULS- /101
<b>Mode</b>						
<b>194 / MIN</b>	-	-	-	-	-	-
	4156,897288	261,819616	1935,194860	0,88	855,61	5,52
<b>Node</b>	273	273	239	273	239	273
<b>Case</b>	ULS/10- 1	ULS/95	6	ULS- /90	ULS- /95	ULS- /81
<b>Mode</b>						
<b>19-6 / MAX</b>	8200,449692	115,441548	15779,751592	12,84	302,25	25,33
<b>Node</b>	241	241	241	242	241	242
<b>Case</b>	ULS/97	ULS/95	ULS/95	ULS- /99	7	ULS- /99
<b>Mode</b>						
<b>19-6 / MIN</b>	-	-	-	-	-	-
	2434,264999	318,732948	2832,433176	2,41	1650,69	14,43

Bar	FX (N)	FY (N)	FZ (N)	MX (Nm)	MY (Nm)	MZ (Nm)
Node	241	242	241	242	241	241
Case	ULS/89	ULS/95	7	6	ULS- /95	ULS- /99
Mode						

## Member Verification

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

## CODE GROUP:

MEMBER: 2 Beam\_2

POINT: 1

COORDINATE: x = 0.06 L = 750.00 mm

## LOADS:

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

## MATERIAL:

S 355 Fy = 355.00 MPa



## SECTION PARAMETERS: HEA 240

d=230.0 mm

b=240.0 mm

w=7.5 mm

t=12.0 mm

Ay=5760.00 mm<sup>2</sup>Iy=77630000.00 mm<sup>4</sup>Sy=675043.48 mm<sup>3</sup>Az=1725.00 mm<sup>2</sup>Iz=27690000.00 mm<sup>4</sup>Sz=230750.00 mm<sup>3</sup>A=7680.00 mm<sup>2</sup>J=421000.00 mm<sup>4</sup>

## INTERNAL FORCES AND CAPACITIES:

Cf = 104225.717892 N

Mfy = -17934.44 N\*m

Mfz = -12333.30 N\*m

Cr0 = 2453760.000000 N

Mry = 215676.39 N\*m

Mrz = 73724.63 N\*m

Vfy = -33961.369958 N

Vfz = 30594.375250 N

CLASS: = Semi-compact

Vry = 1214611.200000 N

Vrz = 363750.750000 N



## LATERAL BUCKLING PARAMETERS:

Le = 13250.00 mm

om2 = 2.08

Mre = 176164.26 N\*m

k = 0.73

Mu = 231584.61 N\*m

## BUCKLING PARAMETERS:



About Y axis:



About Z axis:

## VERIFICATION FORMULAS:

Cf/Cr0 + U1y\*Mfy/Mry + U1z\*Mfz/Mrz = 0.38 &lt; 1.00 (13.8.3(a))

Cf/Crz + U1y\*Mfy/Mre + U1z\*Mfz/Mrz = 0.73 &lt; 1.00 (13.8.3(c))

Vfy/Vry = 0.03 &lt; 1.00 (13.4.1) Vfz/Vrz = 0.08 &lt; 1.00 (13.4.1)

## LIMIT DISPLACEMENTS



## Deflections

uy = 0.0 mm &lt; uy max = L/300.00 = 44.2 mm Verified

Governing Load Case: 15 SLS /1/ 1\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm &lt; uz max = L/300.00 = 44.2 mm Verified

Governing Load Case: 15 SLS /1/ 1\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

Section OK !!!

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 3 Beam\_3

**POINT:** 4

**COORDINATE:** x = 0.50 L = 2100.00 mm

**LOADS:**

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 240**

d=230.0 mm

b=240.0 mm

w=7.5 mm

t=12.0 mm

Ay=5760.00 mm<sup>2</sup>

Iy=77630000.00 mm<sup>4</sup>

Sy=675043.48 mm<sup>3</sup>

Az=1725.00 mm<sup>2</sup>

Iz=27690000.00 mm<sup>4</sup>

Sz=230750.00 mm<sup>3</sup>

A=7680.00 mm<sup>2</sup>

J=421000.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -81969.069138 N

Tr = 2453760.000000 N

Mfy = 11119.62 N\*m

Mry = 215676.39 N\*m

Vfy = -280.811121 N

Vry = 1214611.200000 N

Mfz = -547.38 N\*m

Mrz = 73724.63 N\*m

Vfz = 649.343204 N

Vrz = 363750.750000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.98

om2 = 1.17

Mu = 566567.26 N\*m

Mre = 215676.39 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.09 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.03 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.9 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 4 Beam\_4

**POINT:** 7

**COORDINATE:** x = 0.94 L = 12500.00 mm

**LOADS:**

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 240**

d=230.0 mm

b=240.0 mm

w=7.5 mm

t=12.0 mm

Ay=5760.00 mm<sup>2</sup>

Iy=77630000.00 mm<sup>4</sup>

Sy=675043.48 mm<sup>3</sup>

Az=1725.00 mm<sup>2</sup>

Iz=27690000.00 mm<sup>4</sup>

Sz=230750.00 mm<sup>3</sup>

A=7680.00 mm<sup>2</sup>

J=421000.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 106091.502656 N

Cr0 = 2453760.000000 N

Mfy = -16945.21 N\*m

Mry = 215676.39 N\*m

Vfy = 33124.920552 N

Vry = 1214611.200000 N

Mfz = -11317.14 N\*m

Mrz = 73724.63 N\*m

Vfz = -31843.498049 N

Vrz = 363750.750000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 13250.00 mm

om2 = 2.03

Mre = 174423.23 N\*m

k = 0.02

Mu = 226106.74 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.36 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.71 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.03 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.09 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections*

uy = 0.0 mm < uy max = L/300.00 = 44.2 mm

Verified

**Governing Load Case:** 15 SLS /1/ 1\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 44.2 mm

Verified

**Governing Load Case:** 15 SLS /1/ 1\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 5 Beam\_5

**POINT:** 7

**COORDINATE:** x = 1.00 L = 4200.00 mm

**LOADS:**

Governing Load Case: 12 ULS /50/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 240**

d=230.0 mm

b=240.0 mm

w=7.5 mm

t=12.0 mm

Ay=5760.00 mm<sup>2</sup>

Iy=77630000.00 mm<sup>4</sup>

Sy=675043.48 mm<sup>3</sup>

Az=1725.00 mm<sup>2</sup>

Iz=27690000.00 mm<sup>4</sup>

Sz=230750.00 mm<sup>3</sup>

A=7680.00 mm<sup>2</sup>

J=421000.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -27668.949365 N

Tr = 2453760.000000 N

Mfy = -1419.54 N\*m

Mry = 215676.39 N\*m

Vfy = -2539.926948 N

Vry = 1214611.200000 N

Mfz = 5460.16 N\*m

Mrz = 73724.63 N\*m

Vfz = -10831.081198 N

Vrz = 363750.750000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.91

om2 = 1.18

Mu = 573602.64 N\*m

Mre = 215676.39 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.09 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.07 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.03 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.3 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.7 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /21/ 1\*1.00 + 7\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 6 Beam\_6

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -110764.308891 N

Tr = 1447335.000000 N

Mfy = 15724.37 N\*m

Mry = 93794.74 N\*m

Vfy = 74.396519 N

Vry = 721175.400000 N

Mfz = -149.59 N\*m

Mrz = 32837.50 N\*m

Vfz = -7589.843139 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.83

om2 = 1.26

Mu = 180892.83 N\*m

Mre = 90463.96 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.25 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.10 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.2 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **7 Beam\_7**

POINT: **1**

COORDINATE: **x = 0.62 L = 2610.00 mm**

LOADS:

Governing Load Case: **12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

$A_y = 3420.00$  mm<sup>2</sup>

$I_y = 25100000.00$  mm<sup>4</sup>

$S_y = 293567.25$  mm<sup>3</sup>

$A_z = 1026.00$  mm<sup>2</sup>

$I_z = 9250000.00$  mm<sup>4</sup>

$S_z = 102777.78$  mm<sup>3</sup>

$A = 4530.00$  mm<sup>2</sup>

$J = 148900.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -99563.814729$  N

$T_r = 1447335.000000$  N

$M_{fy} = 16417.75$  N\*m

$M_{ry} = 93794.74$  N\*m

$V_{fy} = -133.737758$  N

$V_{ry} = 721175.400000$  N

$M_{fz} = 97.30$  N\*m

$M_{rz} = 32837.50$  N\*m

$V_{fz} = -8060.818056$  N

$V_{rz} = 216352.620000$  N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

$L_e = 4200.00$  mm

$k = 0.72$

$\omega_2 = 1.31$

$M_u = 188683.23$  N\*m

$M_{re} = 91182.37$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.25 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot S_y / (M_{re} \cdot A) = 0.11 < 1.00$  (13.9.2(b))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_y \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 3.1$  mm  $< u_z \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 8 dJC\_Bm\_Crn\_8 **POINT:** 1

**COORDINATE:** x = 0.60 L = 6905.00 mm

**LOADS:**

Governing Load Case: 12 ULS /22/ 1\*1.25 + 5\*1.50 + 7\*0.40 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: IPE 140**

d=140.0 mm

b=73.0 mm

w=4.7 mm

t=6.9 mm

Ay=1007.40 mm<sup>2</sup>

Iy=5410000.00 mm<sup>4</sup>

Zy=88400.00 mm<sup>3</sup>

Az=658.00 mm<sup>2</sup>

Iz=449000.00 mm<sup>4</sup>

Zz=19240.00 mm<sup>3</sup>

A=1643.00 mm<sup>2</sup>

J=23990.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -7384.218399 N

Tr = 524938.500000 N

Mfy = 2013.67 N\*m

Mry = 28243.80 N\*m

Vfy = 138.417082 N

Vry = 212430.438000 N

Mfz = 79.03 N\*m

Mrz = 6147.18 N\*m

Vfz = -2993.954091 N

Vrz = 138752.460000 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 11500.00 mm

k = 0.00

om2 = 2.50

Mu = 9305.24 N\*m

Mre = 8374.72 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.10 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.21 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.02 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.3 mm < uy max = L/600.00 = 19.2 mm

Verified

**Governing Load Case:** 15 SLS /24/ 1\*1.00 + 6\*1.00 + 5\*1.00 + 4\*1.00

uz = 1.1 mm < uz max = L/600.00 = 19.2 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Instability !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 9 Beam\_9

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /15/ 1\*1.25 + 6\*0.40 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -101456.724164 N

Tr = 1447335.000000 N

Mfy = 16103.27 N\*m

Mry = 93794.74 N\*m

Vfy = 124.785194 N

Vry = 721175.400000 N

Mfz = -14.36 N\*m

Mrz = 32837.50 N\*m

Vfz = -7960.835436 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.77

om2 = 1.30

Mu = 186684.75 N\*m

Mre = 91003.80 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.24 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.11 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.1 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 10 Beam\_10

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -107782.638615 N

Tr = 1447335.000000 N

Mfy = 15849.25 N\*m

Mry = 93794.74 N\*m

Vfy = -145.361502 N

Vry = 721175.400000 N

Mfz = 87.84 N\*m

Mrz = 32837.50 N\*m

Vfz = -8072.786643 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.98

om2 = 1.29

Mu = 185663.07 N\*m

Mre = 90911.02 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.25 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Sy/(Mre*A) = 0.10 < 1.00$  (13.9.2(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.1 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 11 dJC\_Bm\_Cm\_11 **POINT:** 7

**COORDINATE:** x = 0.90 L = 10355.00 mm

**LOADS:**

Governing Load Case: 12 ULS /48/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: IPE 140**

d=140.0 mm

b=73.0 mm

w=4.7 mm

t=6.9 mm

Ay=1007.40 mm<sup>2</sup>

Iy=5410000.00 mm<sup>4</sup>

Zy=88400.00 mm<sup>3</sup>

Az=658.00 mm<sup>2</sup>

Iz=449000.00 mm<sup>4</sup>

Zz=19240.00 mm<sup>3</sup>

A=1643.00 mm<sup>2</sup>

J=23990.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -3361.719727 N

Tr = 524938.500000 N

Mfy = -749.41 N\*m

Mry = 28243.80 N\*m

Vfy = -7.920320 N

Vry = 212430.438000 N

Mfz = 9.47 N\*m

Mrz = 6147.18 N\*m

Vfz = -754.403236 N

Vrz = 138752.460000 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 11500.00 mm

k = 0.00

om2 = 1.30

Mu = 4826.22 N\*m

Mre = 4343.60 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.03 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.13 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.01 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/600.00 = 19.2 mm

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

uz = 0.8 mm < uz max = L/600.00 = 19.2 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Instability !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **12 Beam\_12**

POINT: **1**

COORDINATE: **x = 0.62 L = 2610.00 mm**

LOADS:

Governing Load Case: **12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

$A_y = 3420.00$  mm<sup>2</sup>

$I_y = 25100000.00$  mm<sup>4</sup>

$S_y = 293567.25$  mm<sup>3</sup>

$A_z = 1026.00$  mm<sup>2</sup>

$I_z = 9250000.00$  mm<sup>4</sup>

$S_z = 102777.78$  mm<sup>3</sup>

$A = 4530.00$  mm<sup>2</sup>

$J = 148900.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -109867.395796$  N

$T_r = 1447335.000000$  N

$M_{fy} = 16168.76$  N\*m

$M_{ry} = 93794.74$  N\*m

$V_{fy} = 148.425593$  N

$V_{ry} = 721175.400000$  N

$M_{fz} = -149.86$  N\*m

$M_{rz} = 32837.50$  N\*m

$V_{fz} = -7679.587559$  N

$V_{rz} = 216352.620000$  N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

$L_e = 4200.00$  mm

$k = 0.79$

$\omega_2 = 1.27$

$M_u = 182923.01$  N\*m

$M_{re} = 90657.07$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.25 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot S_y / (M_{re} \cdot A) = 0.10 < 1.00$  (13.9.2(b))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.2$  mm  $< u_y \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 3.2$  mm  $< u_z \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 13 Beam\_13

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -105707.285934 N

Tr = 1447335.000000 N

Mfy = 16632.96 N\*m

Mry = 93794.74 N\*m

Vfy = -93.853108 N

Vry = 721175.400000 N

Mfz = 107.90 N\*m

Mrz = 32837.50 N\*m

Vfz = -8529.350177 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.66

om2 = 1.30

Mu = 186798.46 N\*m

Mre = 91014.06 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.25 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.11 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.2 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 14 Beam\_14

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /15/ 1\*1.25 + 6\*0.40 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -101386.489506 N

Tr = 1447335.000000 N

Mfy = 16236.70 N\*m

Mry = 93794.74 N\*m

Vfy = 137.540139 N

Vry = 721175.400000 N

Mfz = 5.57 N\*m

Mrz = 32837.50 N\*m

Vfz = -8041.278213 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.73

om2 = 1.30

Mu = 187344.21 N\*m

Mre = 91063.15 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.24 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Sy/(Mre*A) = 0.11 < 1.00$  (13.9.2(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.1 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 15 Beam\_15

**POINT:** 1

**COORDINATE:** x = 0.62 L = 2610.00 mm

**LOADS:**

Governing Load Case: 12 ULS /15/ 1\*1.25 + 6\*0.40 + 4\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

Ay=3420.00 mm<sup>2</sup>

Iy=25100000.00 mm<sup>4</sup>

Sy=293567.25 mm<sup>3</sup>

Az=1026.00 mm<sup>2</sup>

Iz=9250000.00 mm<sup>4</sup>

Sz=102777.78 mm<sup>3</sup>

A=4530.00 mm<sup>2</sup>

J=148900.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -101548.280130 N

Tr = 1447335.000000 N

Mfy = 16246.22 N\*m

Mry = 93794.74 N\*m

Vfy = -123.143053 N

Vry = 721175.400000 N

Mfz = 41.26 N\*m

Mrz = 32837.50 N\*m

Vfz = -8001.046655 N

Vrz = 216352.620000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4200.00 mm

k = 0.78

om2 = 1.30

Mu = 187337.86 N\*m

Mre = 91062.58 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.24 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.11 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 3.1 mm < uz max = L/300.00 = 14.0 mm

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **16 Beam\_16**

POINT: **1**

COORDINATE: **x = 0.62 L = 2610.00 mm**

LOADS:

Governing Load Case: **12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

$A_y = 3420.00$  mm<sup>2</sup>

$I_y = 25100000.00$  mm<sup>4</sup>

$S_y = 293567.25$  mm<sup>3</sup>

$A_z = 1026.00$  mm<sup>2</sup>

$I_z = 9250000.00$  mm<sup>4</sup>

$S_z = 102777.78$  mm<sup>3</sup>

$A = 4530.00$  mm<sup>2</sup>

$J = 148900.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -109205.479311$  N

$T_r = 1447335.000000$  N

$M_{fy} = 16415.88$  N\*m

$M_{ry} = 93794.74$  N\*m

$V_{fy} = 213.852741$  N

$V_{ry} = 721175.400000$  N

$M_{fz} = -50.46$  N\*m

$M_{rz} = 32837.50$  N\*m

$V_{fz} = -7664.872651$  N

$V_{rz} = 216352.620000$  N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

$L_e = 4200.00$  mm

$k = 0.76$

$\omega_2 = 1.27$

$M_u = 183452.40$  N\*m

$M_{re} = 90706.73$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.25 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot S_y / (M_{re} \cdot A) = 0.10 < 1.00$  (13.9.2(b))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $<$   $u_y \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 3.3$  mm  $<$   $u_z \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **17 Beam\_17**

POINT: **1**

COORDINATE: **x = 0.62 L = 2610.00 mm**

LOADS:

Governing Load Case: **12 ULS /45/ 1\*1.25 + 2\*0.50 + 3\*1.50 + 5\*1.50 + 4\*1.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **HEA 180**

d=171.0 mm

b=180.0 mm

w=6.0 mm

t=9.5 mm

$A_y = 3420.00$  mm<sup>2</sup>

$I_y = 25100000.00$  mm<sup>4</sup>

$S_y = 293567.25$  mm<sup>3</sup>

$A_z = 1026.00$  mm<sup>2</sup>

$I_z = 9250000.00$  mm<sup>4</sup>

$S_z = 102777.78$  mm<sup>3</sup>

$A = 4530.00$  mm<sup>2</sup>

$J = 148900.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -105872.093785$  N

$T_r = 1447335.000000$  N

$M_{fy} = 17285.11$  N\*m

$M_{ry} = 93794.74$  N\*m

$V_{fy} = -166.299160$  N

$V_{ry} = 721175.400000$  N

$M_{fz} = 92.87$  N\*m

$M_{rz} = 32837.50$  N\*m

$V_{fz} = -9394.194518$  N

$V_{rz} = 216352.620000$  N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

$L_e = 4200.00$  mm

$k = 0.77$

$\omega_2 = 1.33$

$M_u = 191909.30$  N\*m

$M_{re} = 91462.80$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.26 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot S_y / (M_{re} \cdot A) = 0.12 < 1.00$  (13.9.2(b))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_y \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**

$u_z = 3.1$  mm  $< u_z \text{ max} = L/300.00 = 14.0$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 21 dJC\_Beam\_21 **POINT:** 7

**COORDINATE:** x = 1.00 L = 4100.60 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 18666.753099 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -1395.53 N\*m

Mry = 13118.67 N\*m

Vfy = 1308.831353 N

Vry = 179239.500000 N

Mfz = -216.84 N\*m

Mrz = 2700.47 N\*m

Vfz = -5888.576694 N

Vrz = 126522.000000 N



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 1.00

om2 = 1.22

Mu = 10649.95 N\*m

Mre = 9304.91 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.33 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.92 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.05 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.3 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 5.9 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 23 dJC\_Beam\_23 **POINT:** 3

**COORDINATE:** x = 0.49 L = 2017.75 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 235 Fy = 235.00 MPa



**SECTION PARAMETERS:** U\_100x50x5

d=100.0 mm

b=50.0 mm

w=5.0 mm

t=5.0 mm

Ay=500.00 mm<sup>2</sup>

Iy=1432916.67 mm<sup>4</sup>

Sy=28658.33 mm<sup>3</sup>

Az=450.00 mm<sup>2</sup>

Iz=225005.48 mm<sup>4</sup>

Sz=6310.12 mm<sup>3</sup>

A=950.00 mm<sup>2</sup>

J=7522.77 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -25545.526941 N

Tr = 200925.000000 N

Mfy = 1568.79 N\*m

Mrx = 6061.24 N\*m

Vfy = 7.211968 N

Vry = 69795.000000 N

Mfz = 4.35 N\*m

Mrz = 1334.59 N\*m

Vfz = 57.469664 N

Vrz = 62815.500000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.99

om2 = 1.18

Mu = 5038.92 N\*m

Mre = 4361.88 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.39 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.19 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 7.0 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **24 dJC\_Beam\_24** POINT: **7**

COORDINATE: **x = 0.48 L = 1952.67 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 235  $F_y = 235.00$  MPa



SECTION PARAMETERS: **U\_100x50x5**

d=100.0 mm

b=50.0 mm

w=5.0 mm

t=5.0 mm

$A_y=500.00$  mm<sup>2</sup>

$I_y=1432916.67$  mm<sup>4</sup>

$S_y=28658.33$  mm<sup>3</sup>

$A_z=450.00$  mm<sup>2</sup>

$I_z=225005.48$  mm<sup>4</sup>

$S_z=6310.12$  mm<sup>3</sup>

$A=950.00$  mm<sup>2</sup>

$J=7522.77$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -34953.437946$  N

$T_r = 200925.000000$  N

$M_{fy} = 1989.83$  N\*m

$M_{ry} = 6061.24$  N\*m

$V_{fy} = -23.826519$  N

$V_{ry} = 69795.000000$  N

$M_{fz} = 5.02$  N\*m

$M_{rz} = 1334.59$  N\*m

$V_{fz} = 184.770261$  N

$V_{rz} = 62815.500000$  N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

$L_e = 4100.60$  mm

$k = 0.92$

$\omega_2 = 1.16$

$M_u = 4972.14$  N\*m

$M_{re} = 4326.84$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.51 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot S_y / (M_{re} \cdot A) = 0.22 < 1.00$  (13.9.2(b))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_y \text{ max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 9.1$  mm  $< u_z \text{ max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **25 dJC\_Beam\_25** POINT: **7**

COORDINATE: **x = 1.00 L = 4100.60 mm**

LOADS:

Governing Load Case: **12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50**

MATERIAL:

S 235  $F_y = 235.00$  MPa



SECTION PARAMETERS: **U\_100x50x5**

d=100.0 mm

b=50.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 500.00$  mm<sup>2</sup>

$I_y = 1432916.67$  mm<sup>4</sup>

$S_y = 28658.33$  mm<sup>3</sup>

$A_z = 450.00$  mm<sup>2</sup>

$I_z = 225005.48$  mm<sup>4</sup>

$S_z = 6310.12$  mm<sup>3</sup>

$A = 950.00$  mm<sup>2</sup>

$J = 7522.77$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 6887.102679$  N

$Cr_0 = 200925.000000$  N

CLASS: = Semi-compact

$M_{fy} = -457.77$  N\*m

$M_{ry} = 6061.24$  N\*m

$V_{fy} = 992.277215$  N

$V_{ry} = 69795.000000$  N

$M_{fz} = -148.52$  N\*m

$M_{rz} = 1334.59$  N\*m

$V_{fz} = -3650.669880$  N

$V_{rz} = 62815.500000$  N



LATERAL BUCKLING PARAMETERS:

$Le = 4100.60$  mm

$k = 0.91$

$\omega_2 = 1.17$

$M_u = 5015.74$  N\*m

$M_{re} = 4349.82$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.26 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.55 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.01 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.06 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_{y \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: **15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**

$u_z = 7.8$  mm  $< u_{z \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: **15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 26 dJC\_Beam\_26 **POINT:** 7

**COORDINATE:** x = 0.48 L = 1952.67 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 235 Fy = 235.00 MPa



**SECTION PARAMETERS:** U\_100x50x5

d=100.0 mm

b=50.0 mm

w=5.0 mm

t=5.0 mm

Ay=500.00 mm<sup>2</sup>

Iy=1432916.67 mm<sup>4</sup>

Sy=28658.33 mm<sup>3</sup>

Az=450.00 mm<sup>2</sup>

Iz=225005.48 mm<sup>4</sup>

Sz=6310.12 mm<sup>3</sup>

A=950.00 mm<sup>2</sup>

J=7522.77 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -33609.027685 N

Tr = 200925.000000 N

Mfy = 1901.40 N\*m

Mry = 6061.24 N\*m

Vfy = 7.644248 N

Vry = 69795.000000 N

Mfz = -1.58 N\*m

Mrz = 1334.59 N\*m

Vfz = 187.755257 N

Vrz = 62815.500000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.99

om2 = 1.16

Mu = 4974.29 N\*m

Mre = 4327.98 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.48 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.21 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /25/ 1\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

uz = 8.8 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 27 dJC\_Beam\_27 **POINT:** 7

**COORDINATE:** x = 0.48 L = 1952.67 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 235 Fy = 235.00 MPa



**SECTION PARAMETERS:** U\_100x50x5

d=100.0 mm

b=50.0 mm

w=5.0 mm

t=5.0 mm

Ay=500.00 mm<sup>2</sup>

Iy=1432916.67 mm<sup>4</sup>

Sy=28658.33 mm<sup>3</sup>

Az=450.00 mm<sup>2</sup>

Iz=225005.48 mm<sup>4</sup>

Sz=6310.12 mm<sup>3</sup>

A=950.00 mm<sup>2</sup>

J=7522.77 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -29597.991341 N

Tr = 200925.000000 N

Mfy = 1730.73 N\*m

Mry = 6061.24 N\*m

Vfy = 33.161968 N

Vry = 69795.000000 N

Mfz = -9.51 N\*m

Mrz = 1334.59 N\*m

Vfz = 131.492766 N

Vrz = 62815.500000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.95

om2 = 1.17

Mu = 5017.00 N\*m

Mre = 4350.48 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.44 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Sy/(Mre*A) = 0.20 < 1.00$  (13.9.2(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.2 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 7.8 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 35 dJC\_Col\_35

**POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 17088.452108 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -634.61 N\*m

Mrz = 30566.18 N\*m

Vfy = -5131.696417 N

Vry = 289228.775220 N

Mfz = -1046.55 N\*m

Mrz = 30566.18 N\*m

Vfz = 2805.469569 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.68

U1y = 0.70



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.40

U1z = 0.41

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.07 < 1.00$  (13.8.3(a))

$Cf/Cr1 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.07 < 1.00$  (13.8.3(b))

$Vfy/Vry = 0.02 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

Governing Load Case: 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00

$v_y = 0.4 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

Governing Load Case: 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 36 dJC\_Col\_36

**POINT:** 1

**COORDINATE:** x = 0.06 L = 200.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 21315.683167 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -546.70 N\*m

Mrz = 30566.18 N\*m

Vfy = 28.760762 N

Vry = 289228.775220 N

Mfz = 19.85 N\*m

Mrz = 30566.18 N\*m

Vfz = 3445.196095 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.68

U1y = 0.71



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.57

U1z = 0.59

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.04 < 1.00$  (13.8.3(a))

$Cf/Cr1 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.07 < 1.00$  (13.8.3(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.1 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 0.5 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

Governing Load Case: 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 37 dJC\_Col\_37

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3240.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 4753.909505 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -62.16 N\*m

Mrz = 30566.18 N\*m

Vfy = -1350.802266 N

Vry = 289228.775220 N

Mfz = 3814.66 N\*m

Mrz = 30566.18 N\*m

Vfz = -676.624021 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.40

U1y = 0.40



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.53

U1z = 0.53

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.13 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.13 < 1.00$  (13.8.3)

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /45/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 1.6 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 38 dJC\_Col\_38

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3240.00 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 6116.867006 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -68.65 N\*m

Mrz = 30566.18 N\*m

Vfy = -2007.054604 N

Vry = 289228.775220 N

Mfz = 4808.62 N\*m

Mrz = 30566.18 N\*m

Vfz = -332.093393 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.66

U1y = 0.66



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.44

U1z = 0.45

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.17 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.16 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /45/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 0.5 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /16/ 1\*1.00 + 6\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

CODE GROUP:

MEMBER: 39 dJC\_Col\_39

POINT: 7

COORDINATE: x = 1.00 L = 3240.00 mm

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: SHSH 100x100x6.3

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 5738.333709 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -44.77 N\*m

Mrz = 30566.18 N\*m

Vfy = -1543.933166 N

Vry = 289228.775220 N

Mfz = 4455.11 N\*m

Mrz = 30566.18 N\*m

Vfz = -357.362792 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.44

U1y = 0.45



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.54

U1z = 0.54

VERIFICATION FORMULAS:

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.15 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.15 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections Not analyzed



Displacements

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 1.4 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

Governing Load Case: 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 40 dJC\_Col\_40

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3240.00 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 6388.034232 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 43.82 N\*m

Mrz = 30566.18 N\*m

Vfy = -2049.834070 N

Vry = 289228.775220 N

Mfz = 5157.66 N\*m

Mrz = 30566.18 N\*m

Vfz = 280.466732 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.66

U1y = 0.67



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.47

U1z = 0.47

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.18 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.17 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$v_y = 0.6 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /9/ 1\*1.00 + 6\*1.00

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 41 dJC\_Col\_41

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3240.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 4673.308067 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 89.27 N\*m

Mrz = 30566.18 N\*m

Vfy = -1470.528688 N

Vry = 289228.775220 N

Mfz = 4234.42 N\*m

Mrz = 30566.18 N\*m

Vfz = 770.645305 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3240.00 mm

KyLy = 3240.00 mm

KyLy/ry = 85.17

Lamy = 1.21

om1y = 0.40

U1y = 0.40



About Z axis:

Lz = 3240.00 mm

KzLz = 3240.00 mm

KzLz/rz = 85.17

Lamz = 1.21

om1z = 0.54

U1z = 0.54

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.15 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.14 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$v_y = 1.5 \text{ mm} < v_y \text{ max} = L/400.00 = 8.1 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **42 dJC\_Col\_42**

POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50**

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 17213.200392$  N

$Cr_0 = 876450.834000$  N

CLASS: = Plastic

$M_{fy} = 677.86$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = -5701.417317$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = -1111.85$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = -2797.912874$  N

$V_{rz} = 289228.775220$  N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:

$L_y = 3240.00$  mm

$K_y L_y = 3240.00$  mm

$K_y L_y / r_y = 85.17$

$\lambda_{my} = 1.21$

$om_{1y} = 0.66$

$U_{1y} = 0.68$



About Z axis:

$L_z = 3240.00$  mm

$K_z L_z = 3240.00$  mm

$K_z L_z / r_z = 85.17$

$\lambda_{mz} = 1.21$

$om_{1z} = 0.40$

$U_{1z} = 0.41$

VERIFICATION FORMULAS:

$C_f / Cr_0 + 1.00 * M_{fy} / M_{ry} + 1.00 * M_{fz} / M_{rz} = 0.08 < 1.00$  (13.8.3(a))

$C_f / Cr_1 + U_{1y} * M_{fy} / M_{ry} + U_{1z} * M_{fz} / M_{rz} = 0.07 < 1.00$  (13.8.3(b))

$V_{fy} / V_{ry} = 0.02 < 1.00$  (13.4.1)  $V_{fz} / V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections *Not analyzed*



Displacements

$v_x = 0.2$  mm  $< v_x \text{ max} = L / 400.00 = 8.1$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$v_y = 0.3$  mm  $< v_y \text{ max} = L / 400.00 = 8.1$  mm

Verified

Governing Load Case: **15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 43 dJC\_Col\_43

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3310.00 mm

**LOADS:**

Governing Load Case: 12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 3531.737499 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -41.79 N\*m

Mrz = 30566.18 N\*m

Vfy = 2261.843278 N

Vry = 289228.775220 N

Mfz = -3951.11 N\*m

Mrz = 30566.18 N\*m

Vfz = -475.972016 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.40

U1y = 0.40



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.58

U1z = 0.58

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.13 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.13 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.1 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 2.1 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /24/ 1\*1.00 + 6\*1.00 + 5\*1.00 + 4\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 44 dJC\_Col\_44

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3310.00 mm

**LOADS:**

Governing Load Case: 12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 4245.630355 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -52.61 N\*m

Mrz = 30566.18 N\*m

Vfy = 2299.674947 N

Vry = 289228.775220 N

Mfz = -4137.66 N\*m

Mrz = 30566.18 N\*m

Vfz = -270.136959 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.65

U1y = 0.66



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.60

U1z = 0.60

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.14 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.14 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 0.7 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 45 dJC\_Col\_45

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3310.00 mm

**LOADS:**

Governing Load Case: 12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 3914.300671 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -37.53 N\*m

Mrz = 30566.18 N\*m

Vfy = 2369.381745 N

Vry = 289228.775220 N

Mfz = -4303.30 N\*m

Mrz = 30566.18 N\*m

Vfz = -295.733596 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.40

U1y = 0.40



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.60

U1z = 0.60

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.15 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.14 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$v_y = 1.3 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 46 dJC\_Col\_46

**POINT:** 7

**COORDINATE:** x = 1.00 L = 3310.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 5520.455550 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 34.52 N\*m

Mrz = 30566.18 N\*m

Vfy = 1329.963151 N

Vry = 289228.775220 N

Mfz = -4417.11 N\*m

Mrz = 30566.18 N\*m

Vfz = 228.775391 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.65

U1y = 0.65



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.58

U1z = 0.59

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.15 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.15 < 1.00$  (13.8.3)

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.2 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$v_y = 0.8 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **47 dJC\_Col\_47**

POINT: **7**

COORDINATE: **x = 1.00 L = 3310.00 mm**

LOADS:

Governing Load Case: 12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 3639.398490 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 53.48 N\*m

Mrz = 30566.18 N\*m

Vfy = 2393.123848 N

Vry = 289228.775220 N

Mfz = -4279.74 N\*m

Mrz = 30566.18 N\*m

Vfz = 508.073981 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.40

U1y = 0.40



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.58

U1z = 0.59

VERIFICATION FORMULAS:

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.15 < 1.00$  (13.8.3(a))

$Mfy/Mry + Mfz/Mrz = 0.14 < 1.00$  (13.8.3)

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections Not analyzed



Displacements

$v_x = 0.3 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$v_y = 2.0 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

Governing Load Case: 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 48 dJC\_Col\_48

**POINT:** 1

**COORDINATE:** x = 0.06 L = 200.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 22609.755181 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 594.99 N\*m

Mrz = 30566.18 N\*m

Vfy = 24.056584 N

Vry = 289228.775220 N

Mfz = 33.06 N\*m

Mrz = 30566.18 N\*m

Vfz = -3245.067908 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:

Ly = 3310.00 mm

KyLy = 3310.00 mm

KyLy/ry = 87.01

Lamy = 1.24

om1y = 0.67

U1y = 0.70



About Z axis:

Lz = 3310.00 mm

KzLz = 3310.00 mm

KzLz/rz = 87.01

Lamz = 1.24

om1z = 0.58

U1z = 0.60

**VERIFICATION FORMULAS:**

$Cf/Cr0 + 1.00 * Mfy/Mry + 1.00 * Mfz/Mrz = 0.05 < 1.00$  (13.8.3(a))

$Cf/Cr1 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.07 < 1.00$  (13.8.3(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections Not analyzed*



*Displacements*

$v_x = 0.3 \text{ mm} < v_x \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$v_y = 0.4 \text{ mm} < v_y \text{ max} = L/400.00 = 8.3 \text{ mm}$

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **49 dJC\_Beam\_49** POINT: **1**

COORDINATE: **x = 0.01 L = 125.00 mm**

LOADS:

Governing Load Case: 12 ULS /59/ 1\*1.25 + 6\*1.40 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S160x160x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -270.014400 N

Tr = 876450.834000 N

Mfy = -1356.49 N\*m

Mry = 30566.18 N\*m

Vfy = 2177.654260 N

Vry = 289228.775220 N

Mfz = 1962.30 N\*m

Mrz = 30566.18 N\*m

Vfz = 17734.939258 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:



About Y axis:



About Z axis:

BUCKLING PARAMETERS:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.11 < 1.00 (13.9.1)

Vfy/Vry = 0.01 < 1.00 (13.4.1) Vfz/Vrz = 0.06 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 2.0 mm < uy max = L/300.00 = 43.8 mm

Verified

Governing Load Case: 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.3 mm < uz max = L/300.00 = 43.8 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Instability !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 50 dJC\_Beam\_50 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /92/ 1\*1.25 + 2\*0.50 + 7\*1.40

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -9965.699872 N

Tr = 876450.834000 N

Mfy = 537.04 N\*m

Mry = 30566.18 N\*m

Vfy = 1953.291248 N

Vry = 289228.775220 N

Mfz = 1491.54 N\*m

Mrz = 30566.18 N\*m

Vfz = -1852.316858 N

Vrz = 289228.775220 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.08 < 1.00 (13.9.1)

Vfy/Vry = 0.01 < 1.00 (13.4.1) Vfz/Vrz = 0.01 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections*

uy = 1.6 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /25/ 1\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

uz = 0.1 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

CODE GROUP:

MEMBER: 51 dJC\_Beam\_51 POINT: 7

COORDINATE:  $x = 0.34 L = 4425.00$  mm

LOADS:

Governing Load Case: 12 ULS /91/  $1*1.25 + 6*1.40 + 2*0.50$

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: SHSH 100x100x6.3

$d = 100.0$  mm

$b = 100.0$  mm

$w = 6.3$  mm

$t = 6.3$  mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -5897.042669$  N

$T_r = 876450.834000$  N

$M_{fy} = -772.30$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = 5552.454203$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = -3036.68$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = -8241.639756$  N

$V_{rz} = 289228.775220$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.13 < 1.00$  (13.9.1)

$V_{fy}/V_{ry} = 0.02 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.03 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 2.6$  mm  $< u_{y \max} = L/300.00 = 43.8$  mm

Verified

Governing Load Case: 15 SLS /24/  $1*1.00 + 6*1.00 + 5*1.00 + 4*1.00$

$u_z = 0.3$  mm  $< u_{z \max} = L/300.00 = 43.8$  mm

Verified

Governing Load Case: 15 SLS /35/  $1*1.00 + 6*1.00 + 2*1.00 + 3*1.00 + 5*1.00 + 4*1.00$



Displacements Not analyzed

**Instability !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **52 dJC\_Beam\_52** POINT: **7**

COORDINATE: **x = 1.00 L = 4100.00 mm**

LOADS:

Governing Load Case: 12 ULS /86/ 1\*0.90 + 7\*1.40 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S16 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 13113.312998 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = -410.22 N\*m

Mry = 30566.18 N\*m

Vfy = 3095.251774 N

Vry = 289228.775220 N

Mfz = -2346.31 N\*m

Mrz = 30566.18 N\*m

Vfz = -2210.106555 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.11 < 1.00$  (13.8.3(a))

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 2.6 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /42/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 7\*1.00

uz = 0.1 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **53 dJC\_Beam\_53** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S16 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -10766.893715 N

Mfy = 1458.93 N\*m

Mfz = 1626.56 N\*m

Tr = 876450.834000 N

Mrx = 30566.18 N\*m

Mrz = 30566.18 N\*m

Vfy = 7187.654556 N

Vfz = -8467.763403 N

CLASS: = Plastic

Vry = 289228.775220 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.11 < 1.00 (13.9.1)

Vfy/Vry = 0.02 < 1.00 (13.4.1) Vfz/Vrz = 0.03 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

CODE GROUP:

MEMBER: 54 dJC\_Beam\_54 POINT: 5

COORDINATE: x = 0.48 L = 1988.48 mm

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: SHSH 100x100x6.3

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -65781.130606 N

Mfy = 4072.60 N\*m

Mfz = -45.11 N\*m

Tr = 876450.834000 N

Mry = 30566.18 N\*m

Mrz = 30566.18 N\*m

Vfy = 33.578855 N

Vfz = -27.289794 N

CLASS: = Plastic

Vry = 289228.775220 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.21 < 1.00 (13.9.1)

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 7.7 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

Section OK !!!

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **55 dJC\_Beam\_55** POINT: **7**

COORDINATE: **x = 0.50 L = 2050.30 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S16 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -69118.371825 N

Tr = 876450.834000 N

Mfy = 4097.59 N\*m

Mry = 30566.18 N\*m

Vfy = 113.933729 N

Vry = 289228.775220 N

Mfz = -19.66 N\*m

Mrz = 30566.18 N\*m

Vfz = 177.116636 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:



About Y axis:



About Z axis:

BUCKLING PARAMETERS:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.21 < 1.00 (13.9.1)

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 8.2 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

CODE GROUP:

MEMBER: 56 dJC\_Beam\_56 POINT: 2

COORDINATE: x = 0.51 L = 2081.55 mm

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: SHSH 100x100x6.3

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -66088.142741 N

Mfy = 3959.15 N\*m

Mfz = 13.38 N\*m

Tr = 876450.834000 N

Mry = 30566.18 N\*m

Mrz = 30566.18 N\*m

Vfy = 14.961370 N

Vfz = 39.652392 N

CLASS: = Plastic

Vry = 289228.775220 N

Vrz = 289228.775220 N



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.21 < 1.00 (13.9.1)

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /36/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

uz = 7.9 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

Section OK !!!



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **57 dJC\_Beam\_57** POINT: **1**

COORDINATE: **x = 0.50 L = 2050.30 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -52777.449714$  N

$T_r = 876450.834000$  N

$M_{fy} = 3625.95$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = -23.522804$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = 23.80$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = -215.469035$  N

$V_{rz} = 289228.775220$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.18 < 1.00$  (13.9.1)

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 7.1$  mm  $< u_{z \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **58 dJC\_Beam\_58** POINT: **7**

COORDINATE: **x = 0.49 L = 1996.12 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -52546.699959 N

Tr = 876450.834000 N

Mfy = 3552.36 N\*m

Mry = 30566.18 N\*m

Vfy = -22.604623 N

Vry = 289228.775220 N

Mfz = 42.16 N\*m

Mrz = 30566.18 N\*m

Vfz = 28.633805 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.18 < 1.00 (13.9.1)

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 6.7 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **59 dJC\_Beam\_59** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -11082.320333 N

Tr = 876450.834000 N

Mfy = 1489.34 N\*m

Mry = 30566.18 N\*m

Vfy = -7153.224416 N

Vry = 289228.775220 N

Mfz = -1639.60 N\*m

Mrz = 30566.18 N\*m

Vfz = -8698.959993 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.12 < 1.00 (13.9.1)

Vfy/Vry = 0.02 < 1.00 (13.4.1) Vfz/Vrz = 0.03 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 60 dJC\_Beam\_60 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -5649.926907 N

Tr = 876450.834000 N

Mfy = -308.11 N\*m

Mry = 30566.18 N\*m

Vfy = -15393.549610 N

Vry = 289228.775220 N

Mfz = -1550.63 N\*m

Mrz = 30566.18 N\*m

Vfz = 597.114846 N

Vrz = 289228.775220 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Vfy/Vry = 0.05 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections*

uy = 0.1 mm < uy max = L/300.00 = 7.0 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.0 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **61 dJC\_Beam\_61** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -5403.844419 N

Tr = 876450.834000 N

Mfy = -331.78 N\*m

Mrz = 30566.18 N\*m

Vfy = 15414.991109 N

Vry = 289228.775220 N

Mfz = 1546.96 N\*m

Mrz = 30566.18 N\*m

Vfz = 945.942343 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Vfy/Vry = 0.05 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



*Deflections*

uy = 0.1 mm < uy max = L/300.00 = 7.0 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.0 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **62 dJC\_Beam\_62** POINT: **7**

COORDINATE: **x = 0.36 L = 819.00 mm**

LOADS:

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S16 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 2671.346716 N

Cr0 = 876450.834000 N

Mfy = 494.65 N\*m

Mry = 30566.18 N\*m

Vfy = -6219.474896 N

Vry = 289228.775220 N

Mfz = 722.08 N\*m

Mrz = 30566.18 N\*m

Vfz = 3835.336574 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.04 < 1.00$  (13.8.3(a))

$Vfy/Vry = 0.02 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 7.7 mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.7 mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: CAN/CSA S16-09

ANALYSIS TYPE: Member Verification

CODE GROUP:

MEMBER: 63 dJC\_Beam\_63 POINT: 7

COORDINATE:  $x = 0.36 L = 819.00 \text{ mm}$

LOADS:

Governing Load Case: 12 ULS /101/  $1*1.25 + 2*1.50 + 3*0.50 + 4*0.50$

MATERIAL:

S 420  $F_y = 420.00 \text{ MPa}$



SECTION PARAMETERS: SHSH 100x100x6.3

$d = 100.0 \text{ mm}$

$b = 100.0 \text{ mm}$

$w = 6.3 \text{ mm}$

$t = 6.3 \text{ mm}$

$A_y = 1159.33 \text{ mm}^2$

$I_y = 3355722.00 \text{ mm}^4$

$Z_y = 80862.90 \text{ mm}^3$

$A_z = 1159.33 \text{ mm}^2$

$I_z = 3355722.00 \text{ mm}^4$

$Z_z = 80862.90 \text{ mm}^3$

$A = 2318.65 \text{ mm}^2$

$J = 5341795.00 \text{ mm}^4$

INTERNAL FORCES AND CAPACITIES:

$C_f = 2887.844704 \text{ N}$

$Cr_0 = 876450.834000 \text{ N}$

CLASS: = Plastic

$M_{fy} = 459.23 \text{ N}\cdot\text{m}$

$M_{ry} = 30566.18 \text{ N}\cdot\text{m}$

$V_{fy} = 5886.352308 \text{ N}$

$V_{ry} = 289228.775220 \text{ N}$

$M_{fz} = -679.53 \text{ N}\cdot\text{m}$

$M_{rz} = 30566.18 \text{ N}\cdot\text{m}$

$V_{fz} = 3691.633282 \text{ N}$

$V_{rz} = 289228.775220 \text{ N}$



LATERAL BUCKLING PARAMETERS:



About Y axis:



About Z axis:

BUCKLING PARAMETERS:

VERIFICATION FORMULAS:

$C_f / Cr_0 + U_{1y} * M_{fy} / M_{ry} + U_{1z} * M_{fz} / M_{rz} = 0.04 < 1.00 \quad (13.8.3(a))$

$V_{fy} / V_{ry} = 0.02 < 1.00 \quad (13.4.1) \quad V_{fz} / V_{rz} = 0.01 < 1.00 \quad (13.4.1)$

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1 \text{ mm} < u_{y \text{ max}} = L / 300.00 = 7.7 \text{ mm}$

Verified

Governing Load Case: 15 SLS /31/  $1*1.00 + 2*1.00 + 3*1.00 + 4*1.00$

$u_z = 0.0 \text{ mm} < u_{z \text{ max}} = L / 300.00 = 7.7 \text{ mm}$

Verified

Governing Load Case: 15 SLS /31/  $1*1.00 + 2*1.00 + 3*1.00 + 4*1.00$



Displacements Not analyzed

Section OK !!!

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **64 dJC\_Beam\_64** POINT: **1**

COORDINATE: **x = 0.63 L = 1448.00 mm**

LOADS:

Governing Load Case: **12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50**

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: **S16.1 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -1494.128797$  N

$T_r = 876450.834000$  N

$M_{fy} = 435.37$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = 5048.675355$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = 586.10$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = -3272.454614$  N

$V_{rz} = 289228.775220$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.04 < 1.00$  (13.9.1)

$V_{fy}/V_{ry} = 0.02 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_{y \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: **15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 65 dJC\_Beam\_65 **POINT:** 1

**COORDINATE:** x = 0.63 L = 1448.00 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 561.719655 N

Cr0 = 876450.834000 N

CLASS: = Plastic

Mfy = 446.73 N\*m

Mry = 30566.18 N\*m

Vfy = -5031.073382 N

Vry = 289228.775220 N

Mfz = -584.77 N\*m

Mrz = 30566.18 N\*m

Vfz = -3462.870918 N

Vrz = 289228.775220 N



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Vfy/Vry = 0.02 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 7.7 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.7 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **66 dJC\_Beam\_66** POINT: **7**

COORDINATE: **x = 1.00 L = 2300.00 mm**

LOADS:

Governing Load Case: **12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50**

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: **S16.1 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -2882.096730$  N

$T_r = 876450.834000$  N

$M_{fy} = -94.81$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = 6435.661602$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = -1207.57$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = 331.784814$  N

$V_{rz} = 289228.775220$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:



About Y axis:



About Z axis:

BUCKLING PARAMETERS:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.05 < 1.00$  (13.9.1)

$V_{fy}/V_{ry} = 0.02 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_{y \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: **15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **67 dJC\_Beam\_67** POINT: **1**

COORDINATE: **x = 0.91 L = 2100.00 mm**

LOADS:

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **S16 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 2074.285338 N

Cr0 = 876450.834000 N

Mfy = 72.72 N\*m

Mry = 30566.18 N\*m

Vfy = -12356.434715 N

Vry = 289228.775220 N

Mfz = -600.99 N\*m

Mrz = 30566.18 N\*m

Vfz = -346.533869 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Vfy/Vry = 0.04 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 7.7 mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.7 mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **68 dJC\_Beam\_68** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 420  $F_y = 420.00$  MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

$A_y = 1159.33$  mm<sup>2</sup>

$I_y = 3355722.00$  mm<sup>4</sup>

$Z_y = 80862.90$  mm<sup>3</sup>

$A_z = 1159.33$  mm<sup>2</sup>

$I_z = 3355722.00$  mm<sup>4</sup>

$Z_z = 80862.90$  mm<sup>3</sup>

$A = 2318.65$  mm<sup>2</sup>

$J = 5341795.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -2516.735520$  N

$T_r = 876450.834000$  N

$M_{fy} = -45.85$  N\*m

$M_{ry} = 30566.18$  N\*m

$V_{fy} = -4452.812637$  N

$V_{ry} = 289228.775220$  N

$M_{fz} = -1013.29$  N\*m

$M_{rz} = 30566.18$  N\*m

$V_{fz} = -539.476708$  N

$V_{rz} = 289228.775220$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.04 < 1.00$  (13.9.1)

$V_{fy}/V_{ry} = 0.02 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.1$  mm  $< u_{y \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 7.7$  mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **69 dJC\_Beam\_69** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /105/ 1\*0.90 + 2\*1.50 + 3\*0.50

MATERIAL:

S 420 Fy = 420.00 MPa



SECTION PARAMETERS: **SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -1149.695614 N

Tr = 876450.834000 N

Mfy = -7.25 N\*m

Mry = 30566.18 N\*m

Vfy = 2984.255201 N

Vry = 289228.775220 N

Mfz = 897.26 N\*m

Mrz = 30566.18 N\*m

Vfz = -824.392982 N

Vrz = 289228.775220 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:



About Y axis:



About Z axis:

BUCKLING PARAMETERS:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.03 < 1.00 (13.9.1)

Vfy/Vry = 0.01 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



*Deflections*

uy = 0.1 mm < uy max = L/300.00 = 7.7 mm Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 7.7 mm Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 70 dJC\_Beam\_70 **POINT:** 7

**COORDINATE:** x = 1.00 L = 1850.00 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -5536.567822 N

Tr = 876450.834000 N

Mfy = -314.37 N\*m

Mrx = 30566.18 N\*m

Vfy = 15553.141932 N

Vry = 289228.775220 N

Mfz = -1581.78 N\*m

Mrz = 30566.18 N\*m

Vfz = -592.704888 N

Vrz = 289228.775220 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Vfy/Vry = 0.05 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 6.2 mm Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 6.2 mm Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 71 dJC\_Beam\_71 **POINT:** 7

**COORDINATE:** x = 1.00 L = 1850.00 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 420 Fy = 420.00 MPa



**SECTION PARAMETERS: SHSH 100x100x6.3**

d=100.0 mm

b=100.0 mm

w=6.3 mm

t=6.3 mm

Ay=1159.33 mm<sup>2</sup>

Iy=3355722.00 mm<sup>4</sup>

Zy=80862.90 mm<sup>3</sup>

Az=1159.33 mm<sup>2</sup>

Iz=3355722.00 mm<sup>4</sup>

Zz=80862.90 mm<sup>3</sup>

A=2318.65 mm<sup>2</sup>

J=5341795.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -5471.450128 N

Tr = 876450.834000 N

Mfy = -335.17 N\*m

Mry = 30566.18 N\*m

Vfy = -15640.602164 N

Vry = 289228.775220 N

Mfz = 1573.58 N\*m

Mrz = 30566.18 N\*m

Vfz = -902.677342 N

Vrz = 289228.775220 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Vfy/Vry = 0.05 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections*

uy = 0.1 mm < uy max = L/300.00 = 6.2 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 6.2 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **77 dJC\_Beam\_77** POINT: **7**

COORDINATE: **x = 1.00 L = 4100.60 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 5300.501373 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -630.43 N\*m

Mry = 13118.67 N\*m

Vfy = 229.258583 N

Vry = 179239.500000 N

Mfz = -49.29 N\*m

Mrz = 2700.47 N\*m

Vfz = -4553.279797 N

Vrz = 126522.000000 N



LATERAL BUCKLING PARAMETERS:

Le = 4100.60 mm

k = 0.99

om2 = 1.18

Mu = 10266.09 N\*m

Mre = 9088.73 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.08 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.26 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 6.8 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **78 dJC\_Beam\_78** POINT: **1**

COORDINATE: **x = 0.52 L = 2147.93 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -47273.027577 N

Tr = 429727.500000 N

Mfy = 2772.24 N\*m

Mry = 13118.67 N\*m

Vfy = 31.684241 N

Vry = 179239.500000 N

Mfz = 8.76 N\*m

Mrz = 2700.47 N\*m

Vfz = -286.310574 N

Vrz = 126522.000000 N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

Le = 4100.60 mm

k = 0.97

om2 = 1.17

Mu = 10153.87 N\*m

Mre = 9022.44 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.32 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Sy/(Mre\*A) = 0.15 < 1.00 (13.9.2(b))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 8.8 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 79 dJC\_Beam\_79 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 9761.320020 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -993.51 N\*m

Mry = 13118.67 N\*m

Vfy = 301.294018 N

Vry = 179239.500000 N

Mfz = 37.86 N\*m

Mrz = 2700.47 N\*m

Vfz = 7001.959851 N

Vrz = 126522.000000 N



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.90

om2 = 1.16

Mu = 10100.88 N\*m

Mre = 8990.62 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.12 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.44 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.06 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /25/ 1\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

uz = 9.4 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 80 dJC\_Beam\_80 **POINT:** 7

**COORDINATE:** x = 1.00 L = 4100.60 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 8761.080990 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -907.22 N\*m

Mry = 13118.67 N\*m

Vfy = 191.179505 N

Vry = 179239.500000 N

Mfz = -48.38 N\*m

Mrz = 2700.47 N\*m

Vfz = -6463.160830 N

Vrz = 126522.000000 N



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.98

om2 = 1.17

Mu = 10229.49 N\*m

Mre = 9067.27 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.12 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.40 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.05 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 9.4 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 81 dJC\_Beam\_81 **POINT:** 1

**COORDINATE:** x = 0.43 L = 1757.40 mm

**LOADS:**

Governing Load Case: 12 ULS /77/ 1\*0.90 + 6\*1.40

**MATERIAL:**

S 355  $F_y = 355.00$  MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

$A_y = 850.00$  mm<sup>2</sup>

$I_y = 2053000.00$  mm<sup>4</sup>

$S_y = 41060.00$  mm<sup>3</sup>

$A_z = 600.00$  mm<sup>2</sup>

$I_z = 291600.00$  mm<sup>4</sup>

$S_z = 8452.17$  mm<sup>3</sup>

$A = 1345.00$  mm<sup>2</sup>

$J = 25210.00$  mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

$C_f = 8216.156153$  N

$Cr_0 = 429727.500000$  N

CLASS: = Semi-compact

$M_{fy} = -479.19$  N\*m

$M_{ry} = 13118.67$  N\*m

$V_{fy} = -12.860944$  N

$V_{ry} = 179239.500000$  N

$M_{fz} = -1.30$  N\*m

$M_{rz} = 2700.47$  N\*m

$V_{fz} = 18.243346$  N

$V_{rz} = 126522.000000$  N



**LATERAL BUCKLING PARAMETERS:**

$Le = 4100.60$  mm

$k = -0.73$

$\omega_2 = 1.18$

$M_u = 10249.61$  N\*m

$M_{re} = 9079.09$  N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.06 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.32 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

$u_y = 0.0$  mm  $< u_y \text{ max} = L/300.00 = 13.7$  mm

Verified

**Governing Load Case:** 15 SLS /36/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

$u_z = 8.7$  mm  $< u_z \text{ max} = L/300.00 = 13.7$  mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 82 dJC\_Beam\_82 **POINT:** 7

**COORDINATE:** x = 1.00 L = 4100.60 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 10324.363067 N

Cr0 = 429727.500000 N

Mfy = -1098.83 N\*m

Mry = 13118.67 N\*m

Vfy = 366.470552 N

Vry = 179239.500000 N

Mfz = -56.69 N\*m

Mrz = 2700.47 N\*m

Vfz = -7481.417146 N

Vrz = 126522.000000 N

CLASS: = Semi-compact



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.99

om2 = 1.18

Mu = 10258.12 N\*m

Mre = 9084.07 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.14 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.48 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.06 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 10.6 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 83 dJC\_Beam\_83 **POINT:** 1

**COORDINATE:** x = 0.43 L = 1757.40 mm

**LOADS:**

Governing Load Case: 12 ULS /77/ 1\*0.90 + 6\*1.40

**MATERIAL:**

S 355  $F_y = 355.00$  MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

$A_y = 850.00$  mm<sup>2</sup>

$I_y = 2053000.00$  mm<sup>4</sup>

$S_y = 41060.00$  mm<sup>3</sup>

$A_z = 600.00$  mm<sup>2</sup>

$I_z = 291600.00$  mm<sup>4</sup>

$S_z = 8452.17$  mm<sup>3</sup>

$A = 1345.00$  mm<sup>2</sup>

$J = 25210.00$  mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

$C_f = 12329.467454$  N

$Cr_0 = 429727.500000$  N

CLASS: = Semi-compact

$M_{fy} = -612.90$  N\*m

$M_{ry} = 13118.67$  N\*m

$V_{fy} = -12.632665$  N

$V_{ry} = 179239.500000$  N

$M_{fz} = -0.48$  N\*m

$M_{rz} = 2700.47$  N\*m

$V_{fz} = -15.353377$  N

$V_{rz} = 126522.000000$  N



**LATERAL BUCKLING PARAMETERS:**

$Le = 4100.60$  mm

$k = -0.16$

$\omega_2 = 1.19$

$M_u = 10375.89$  N\*m

$M_{re} = 9152.19$  N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.08 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.46 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

$u_y = 0.0$  mm <  $u_y \text{ max} = L/300.00 = 13.7$  mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$u_z = 10.4$  mm <  $u_z \text{ max} = L/300.00 = 13.7$  mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **84 dJC\_Beam\_84** POINT: **7**

COORDINATE: **x = 1.00 L = 4100.60 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

$A_y = 850.00$  mm<sup>2</sup>

$I_y = 2053000.00$  mm<sup>4</sup>

$S_y = 41060.00$  mm<sup>3</sup>

$A_z = 600.00$  mm<sup>2</sup>

$I_z = 291600.00$  mm<sup>4</sup>

$S_z = 8452.17$  mm<sup>3</sup>

$A = 1345.00$  mm<sup>2</sup>

$J = 25210.00$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 9801.838230$  N

$Cr_0 = 429727.500000$  N

CLASS: = Semi-compact

$M_{fy} = -1053.02$  N\*m

$M_{ry} = 13118.67$  N\*m

$V_{fy} = 439.338437$  N

$V_{ry} = 179239.500000$  N

$M_{fz} = -68.68$  N\*m

$M_{rz} = 2700.47$  N\*m

$V_{fz} = -7324.216702$  N

$V_{rz} = 126522.000000$  N



LATERAL BUCKLING PARAMETERS:

$Le = 4100.60$  mm

$k = 0.94$

$\omega_2 = 1.18$

$M_u = 10253.94$  N\*m

$M_{re} = 9081.62$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.14 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.47 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.06 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

$u_z = 10.6$  mm  $< u_{z \max} = L/300.00 = 13.7$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 85 dJC\_Beam\_85 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 12409.562999 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -1277.04 N\*m

Mry = 13118.67 N\*m

Vfy = 512.109052 N

Vry = 179239.500000 N

Mfz = 76.90 N\*m

Mrz = 2700.47 N\*m

Vfz = 8338.470042 N

Vrz = 126522.000000 N



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.93

om2 = 1.17

Mu = 10167.67 N\*m

Mre = 9030.67 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.17 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.58 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.07 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.1 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 10.8 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **86 dJC\_Beam\_86** POINT: **5**

COORDINATE: **x = 0.50 L = 2033.63 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -38859.893448 N

Tr = 429727.500000 N

Mfy = 2328.58 N\*m

Mry = 13118.67 N\*m

Vfy = 9.034828 N

Vry = 179239.500000 N

Mfz = -10.20 N\*m

Mrz = 2700.47 N\*m

Vfz = -32.879378 N

Vrz = 126522.000000 N

CLASS: = Semi-compact



LATERAL BUCKLING PARAMETERS:

Le = 4100.60 mm

k = 0.85

om2 = 1.15

Mu = 10043.01 N\*m

Mre = 8955.50 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.27 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Sy/(Mre*A) = 0.13 < 1.00$  (13.9.2(b))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.2 mm < uy max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 7.5 mm < uz max = L/300.00 = 13.7 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 87 dJC\_Beam\_87 **POINT:** 7

**COORDINATE:** x = 1.00 L = 4100.60 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: UNP 100**

d=100.0 mm

b=50.0 mm

w=6.0 mm

t=8.5 mm

Ay=850.00 mm<sup>2</sup>

Iy=2053000.00 mm<sup>4</sup>

Sy=41060.00 mm<sup>3</sup>

Az=600.00 mm<sup>2</sup>

Iz=291600.00 mm<sup>4</sup>

Sz=8452.17 mm<sup>3</sup>

A=1345.00 mm<sup>2</sup>

J=25210.00 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 19154.982019 N

Cr0 = 429727.500000 N

CLASS: = Semi-compact

Mfy = -1472.21 N\*m

Mry = 13118.67 N\*m

Vfy = -1108.369903 N

Vry = 179239.500000 N

Mfz = 186.71 N\*m

Mrz = 2700.47 N\*m

Vfz = -6494.083541 N

Vrz = 126522.000000 N



**LATERAL BUCKLING PARAMETERS:**

Le = 4100.60 mm

k = 0.98

om2 = 1.22

Mu = 10595.12 N\*m

Mre = 9274.98 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.31 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.93 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.05 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.3 mm < uy max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 6.9 mm < uz max = L/300.00 = 13.7 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **88 dJC\_Beam\_88** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 6576.386455$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -852.03$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 23.232151$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -3.74$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -7074.784566$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.59$

$\omega_2 = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.10 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.12 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.03 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **89 dJC\_Beam\_89** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -1653.183974 N

Tr = 383400.000000 N

Mfy = -45.30 N\*m

Mry = 11502.00 N\*m

Vfy = 7.571750 N

Vry = 19464.923077 N

Mfz = -2.15 N\*m

Mrz = 958.50 N\*m

Vfz = -417.697966 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.84 mm

k = -0.67

om2 = 2.35

Mu = 65798.73 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.01 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.00 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **90 dJC\_Beam\_90** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /81/ 1\*0.90 + 6\*1.40 + 5\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 1024.735094$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 17.54$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -78.067357$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -5.36$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -39.058030$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = 0.14$

$\omega_2 = 1.49$

$M_u = 41634.53$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 91 dJC\_Beam\_91 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 15680.842550 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 497.04 N\*m

Mry = 11502.00 N\*m

Vfy = -4.591016 N

Vry = 19464.923077 N

Mfz = -0.17 N\*m

Mrz = 958.50 N\*m

Vfz = -2452.488490 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.27

om2 = 2.12

Mu = 59509.80 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.08 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.14 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /24/ 1\*1.00 + 6\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **92 dJC\_Beam\_92** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -611.408038 N

Tr = 383400.000000 N

Mfy = 127.28 N\*m

Mry = 11502.00 N\*m

Vfy = 6.051311 N

Vry = 19464.923077 N

Mfz = 1.87 N\*m

Mrz = 958.50 N\*m

Vfz = -897.944212 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.84 mm

k = -0.96

om2 = 2.34

Mu = 65538.89 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.01 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Zy/(Mre*A) = 0.01 < 1.00$  (13.9.2(a))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 93 dJC\_Beam\_93 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -981.724239 N

Tr = 383400.000000 N

Mfy = 43.31 N\*m

Mry = 11502.00 N\*m

Vfy = -0.714899 N

Vry = 19464.923077 N

Mfz = -1.13 N\*m

Mrz = 958.50 N\*m

Vfz = -218.134436 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.55

om2 = 2.24

Mu = 62893.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.01 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.00 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /9/ 1\*1.00 + 6\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **94 dJC\_Beam\_94** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 166.278573$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 64.19$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 3.516330$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -1.37$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 243.166592$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.16$

$\omega_2 = 1.86$

$M_u = 52276.93$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /9/ 1\*1.00 + 6\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **95 dJC\_Beam\_95** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -1313.963538 N

Tr = 383400.000000 N

Mfy = -230.93 N\*m

Mry = 11502.00 N\*m

Vfy = -7.429445 N

Vry = 19464.923077 N

Mfz = 2.57 N\*m

Mrz = 958.50 N\*m

Vfz = -1294.282061 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.84 mm

k = -0.20

om2 = 2.39

Mu = 66956.65 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.03 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.02 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.01 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 96 dJC\_Beam\_96 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -558.243464 N

Tr = 383400.000000 N

Mfy = -389.34 N\*m

Mry = 11502.00 N\*m

Vfy = 3.991687 N

Vry = 19464.923077 N

Mfz = 1.62 N\*m

Mrz = 958.50 N\*m

Vfz = 2751.139492 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.49

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.04 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.03 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.01 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /9/ 1\*1.00 + 6\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 97 dJC\_Beam\_97 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1188.307118 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 39.38 N\*m

Mry = 11502.00 N\*m

Vfy = -25.482201 N

Vry = 19464.923077 N

Mfz = -3.37 N\*m

Mrz = 958.50 N\*m

Vfz = -53.681174 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.47

om2 = 1.26

Mu = 35362.34 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **98 dJC\_Beam\_98** POINT: **4**

COORDINATE: **x = 0.50 L = 141.42 mm**

LOADS:

Governing Load Case: 12 ULS /73/ 1\*1.25 + 6\*1.40 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -431.786534 N

Tr = 383400.000000 N

Mfy = -3.83 N\*m

Mry = 11502.00 N\*m

Vfy = 10.450722 N

Vry = 19464.923077 N

Mfz = 5.45 N\*m

Mrz = 958.50 N\*m

Vfz = -9.453728 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.84 mm

k = 0.60

om2 = 1.56

Mu = 43818.50 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.01 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.00 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /24/ 1\*1.00 + 6\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **100 dJC\_Beam\_100** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 6120.633593$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -1014.13$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -26.400955$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -4.16$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 8295.546647$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = -0.48$

$\omega_2 = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.11 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.13 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 102 dJC\_Beam\_102 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 6469.795925 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -882.21 N\*m

Mry = 11502.00 N\*m

Vfy = 41.744932 N

Vry = 19464.923077 N

Mfz = -9.74 N\*m

Mrz = 958.50 N\*m

Vfz = -7326.275208 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.52

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.10 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.12 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.03 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /36/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **104 dJC\_Beam\_104** POINT: **4**

COORDINATE: **x = 0.50 L = 141.42 mm**

LOADS:

Governing Load Case: **12 ULS /77/ 1\*0.90 + 6\*1.40**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 731.372064$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 16.73$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -5.796724$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 2.82$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -95.490433$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = 0.07$

$\omega_2 = 1.60$

$M_u = 44718.44$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /45/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 105 dJC\_Beam\_105 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 804.708293 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 61.09 N\*m

Mry = 11502.00 N\*m

Vfy = -31.130434 N

Vry = 19464.923077 N

Mfz = 3.55 N\*m

Mrz = 958.50 N\*m

Vfz = 175.166440 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.10

om2 = 1.59

Mu = 44676.02 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /9/ 1\*1.00 + 6\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **106 dJC\_Beam\_106** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 16214.887176$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 452.29$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 114.205359$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 7.99$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -2237.598425$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = -0.13$

$\omega_2 = 2.09$

$M_u = 58718.55$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.09 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.14 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.01 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 107 dJC\_Beam\_107 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /111/ 1\*1.25 + 6\*0.40 + 2\*1.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -344.214381 N

Tr = 383400.000000 N

Mfy = -162.09 N\*m

Mry = 11502.00 N\*m

Vfy = 15.175175 N

Vry = 19464.923077 N

Mfz = -4.44 N\*m

Mrz = 958.50 N\*m

Vfz = -1043.714427 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.79

om2 = 2.42

Mu = 67719.63 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.02 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.02 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 108 dJC\_Beam\_108 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -1016.808022 N

Tr = 383400.000000 N

Mfy = 57.93 N\*m

Mry = 11502.00 N\*m

Vfy = 8.741846 N

Vry = 19464.923077 N

Mfz = 1.11 N\*m

Mrz = 958.50 N\*m

Vfz = -289.691103 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.51

om2 = 2.23

Mu = 62502.68 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.01 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.00 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.00 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **109 dJC\_Beam\_109** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -186.403143$  N

$T_r = 383400.000000$  N

$M_{fy} = 73.25$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -32.392443$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 3.49$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 307.777227$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.26$

$\omega_2 = 1.99$

$M_u = 55806.59$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.01 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.01 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /20/ 1\*1.00 + 6\*1.00 + 4\*1.00**

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **110 dJC\_Beam\_110** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -1267.785500$  N

$T_r = 383400.000000$  N

$M_{fy} = -262.08$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -4.003911$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -2.48$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -1474.888514$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.25$

$\omega_m = 2.40$

$M_u = 67354.70$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.03 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.02 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **111 dJC\_Beam\_111** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -903.286809$  N

$T_r = 383400.000000$  N

$M_{fy} = -414.19$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -4.898851$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -4.10$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 2921.169004$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.45$

$\omega_m = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.04 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.04 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 112 dJC\_Beam\_112 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1238.674749 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 21.34 N\*m

Mry = 11502.00 N\*m

Vfy = 31.123590 N

Vry = 19464.923077 N

Mfz = -5.33 N\*m

Mrz = 958.50 N\*m

Vfz = -69.431980 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.60

om2 = 1.17

Mu = 32877.19 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **113 dJC\_Beam\_113** POINT: **4**

COORDINATE: **x = 0.50 L = 141.42 mm**

LOADS:

Governing Load Case: **12 ULS /77/ 1\*0.90 + 6\*1.40**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 260.756404$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 7.84$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 5.732528$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 2.87$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 64.753959$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = -0.15$

$\omega_2 = 1.76$

$M_u = 49297.67$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.00 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.01 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /45/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 114 dJC\_Beam\_114 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 7233.504288 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -992.89 N\*m

Mry = 11502.00 N\*m

Vfy = -51.142101 N

Vry = 19464.923077 N

Mfz = -11.20 N\*m

Mrz = 958.50 N\*m

Vfz = 8308.795913 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.49

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.12 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.14 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 131 dJC\_Beam\_131 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1272.921191 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -76.38 N\*m

Mry = 11502.00 N\*m

Vfy = -81.429992 N

Vry = 19464.923077 N

Mfz = 19.42 N\*m

Mrz = 958.50 N\*m

Vfz = -401.169953 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.89

om2 = 1.51

Mu = 42387.34 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 133 dJC\_Beam\_133 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 2491.738816 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -22.60 N\*m

Mry = 11502.00 N\*m

Vfy = -30.351697 N

Vry = 19464.923077 N

Mfz = 12.22 N\*m

Mrz = 958.50 N\*m

Vfz = -545.784439 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.33

om2 = 1.37

Mu = 38394.33 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 134 dJC\_Beam\_134 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1180.164296 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 24.18 N\*m

Mry = 11502.00 N\*m

Vfy = 15.716275 N

Vry = 19464.923077 N

Mfz = 8.38 N\*m

Mrz = 958.50 N\*m

Vfz = -258.043470 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.53

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.01 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /36/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **135 dJC\_Beam\_135** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 3265.418998$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 25.77$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -39.069617$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 16.87$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 4.081101$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = -0.26$

$\omega_2 = 2.50$

$Mu = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U1y * M_{fy}/M_{ry} + U1z * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U1y * M_{fy}/M_{re} + U1z * M_{fz}/M_{rz} = 0.04 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 136 dJC\_Beam\_136 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 808.069427 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 36.72 N\*m

Mry = 11502.00 N\*m

Vfy = 30.015268 N

Vry = 19464.923077 N

Mfz = 13.31 N\*m

Mrz = 958.50 N\*m

Vfz = -153.104090 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.28

om2 = 2.17

Mu = 60968.82 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **137 dJC\_Beam\_137** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 1364.460854$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 50.44$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -34.682860$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 13.80$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 88.137419$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.42$

$\omega_2 = 1.60$

$M_u = 44771.93$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.02 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 138 dJC\_Beam\_138 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 760.641601 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 48.51 N\*m

Mrz = 11502.00 N\*m

Vfy = 26.372795 N

Vry = 19464.923077 N

Mfz = 11.72 N\*m

Mrz = 958.50 N\*m

Vfz = -227.628508 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.12

om2 = 2.01

Mu = 56216.54 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 139 dJC\_Beam\_139 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 958.747216 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 50.25 N\*m

Mry = 11502.00 N\*m

Vfy = -38.003218 N

Vry = 19464.923077 N

Mfz = 15.33 N\*m

Mrz = 958.50 N\*m

Vfz = 174.304365 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.12

om2 = 1.82

Mu = 51085.71 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **140 dJC\_Beam\_140** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 2172.154076$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 12.38$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 36.436955$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 14.87$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 251.175937$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.24$

$\omega_2 = 1.91$

$M_u = 53653.69$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.02 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **141 dJC\_Beam\_141** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /73/ 1\*1.25 + 6\*1.40 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -1546.786688$  N

$T_r = 383400.000000$  N

$M_{fy} = 58.97$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 39.473687$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -7.36$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 627.253048$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.40$

$\omega_m = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.02 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.01 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 142 dJC\_Beam\_142 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 2878.193417 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -25.25 N\*m

Mry = 11502.00 N\*m

Vfy = 40.579612 N

Vry = 19464.923077 N

Mfz = 14.96 N\*m

Mrz = 958.50 N\*m

Vfz = 634.279209 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.97

om2 = 1.33

Mu = 37315.45 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 144 dJC\_Beam\_144 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1067.310839 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -76.82 N\*m

Mry = 11502.00 N\*m

Vfy = 80.682545 N

Vry = 19464.923077 N

Mfz = 19.17 N\*m

Mrz = 958.50 N\*m

Vfz = 451.360412 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.78

om2 = 1.63

Mu = 45732.40 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y * Mfy/Mry + U1z * Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y * Mfy/Mre + U1z * Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **145 dJC\_Beam\_145** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 1423.551762$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -83.90$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 81.354874$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -19.45$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -470.324379$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = 0.92$

$\omega_2 = 1.58$

$M_u = 44305.08$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.04 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **147 dJC\_Beam\_147** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 2364.941824$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -24.49$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 31.417121$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -12.10$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -538.391364$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = 0.36$

$\omega_2 = 1.83$

$M_u = 51337.61$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.02 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /37/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 148 dJC\_Beam\_148 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /91/ 1\*1.25 + 6\*1.40 + 2\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 865.510163 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -12.30 N\*m

Mry = 11502.00 N\*m

Vfy = -62.636792 N

Vry = 19464.923077 N

Mfz = -12.29 N\*m

Mrz = 958.50 N\*m

Vfz = 217.652332 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.20

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **149 dJC\_Beam\_149** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 2924.342981$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = 23.06$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 35.276982$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -14.81$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 32.534459$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = -0.22$

$\omega_2 = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 150 dJC\_Beam\_150 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /91/ 1\*1.25 + 6\*1.40 + 2\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1251.480604 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -50.87 N\*m

Mry = 11502.00 N\*m

Vfy = -72.810547 N

Vry = 19464.923077 N

Mfz = -12.18 N\*m

Mrz = 958.50 N\*m

Vfz = 551.715769 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.57

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 151 dJC\_Beam\_151 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /91/ 1\*1.25 + 6\*1.40 + 2\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1936.999762 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -78.29 N\*m

Mry = 11502.00 N\*m

Vfy = 64.889536 N

Vry = 19464.923077 N

Mfz = -11.97 N\*m

Mrz = 958.50 N\*m

Vfz = -837.896596 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.97

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **152 dJC\_Beam\_152** POINT: **7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /59/ 1\*1.25 + 6\*1.40 + 3\*0.50 + 5\*0.50 + 4\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Cf = 1420.842116 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 123.43 N\*m

Mry = 11502.00 N\*m

Vfy = 26.620132 N

Vry = 19464.923077 N

Mfz = -5.91 N\*m

Mrz = 958.50 N\*m

Vfz = 923.822076 N

Vrz = 233579.076923 N



LATERAL BUCKLING PARAMETERS:

Le = 282.84 mm

k = -0.49

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 153 dJC\_Beam\_153 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.84 mm

**LOADS:**

Governing Load Case: 12 ULS /91/ 1\*1.25 + 6\*1.40 + 2\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1830.338518 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -71.43 N\*m

Mry = 11502.00 N\*m

Vfy = 65.495807 N

Vry = 19464.923077 N

Mfz = -11.30 N\*m

Mrz = 958.50 N\*m

Vfz = -765.236458 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.97

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 154 dJC\_Beam\_154 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1782.520980 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 12.68 N\*m

Mry = 11502.00 N\*m

Vfy = -36.944447 N

Vry = 19464.923077 N

Mfz = -13.74 N\*m

Mrz = 958.50 N\*m

Vfz = 196.021321 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = -0.24

om2 = 2.50

Mu = 70080.07 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.02 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **155 dJC\_Beam\_155 POINT: 7**

COORDINATE: **x = 1.00 L = 282.84 mm**

LOADS:

Governing Load Case: 12 ULS /93/ 1\*0.90 + 6\*1.40 + 2\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 1402.882176$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -46.31$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 64.935527$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -12.14$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -526.807697$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.84$  mm

$k = -0.90$

$\omega_2 = 2.50$

$M_u = 70080.07$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U1y*M_{fy}/M_{ry} + U1z*M_{fz}/M_{rz} = 0.02 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U1y*M_{fy}/M_{re} + U1z*M_{fz}/M_{rz} = 0.02 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $< u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 156 dJC\_Beam\_156 **POINT:** 1

**COORDINATE:** x = 0.00 L = 0.00 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 2876.096848 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -31.61 N\*m

Mry = 11502.00 N\*m

Vfy = -42.379240 N

Vry = 19464.923077 N

Mfz = -14.96 N\*m

Mrz = 958.50 N\*m

Vfz = 682.211881 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.84 mm

k = 0.99

om2 = 1.71

Mu = 47977.23 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.04 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.00 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /35/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /41/ 1\*1.00 + 6\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **158 dJC\_Beam\_158** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 1048.149268$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -79.98$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -79.645436$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -19.22$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = 475.627664$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.84$  mm

$k = 0.78$

$\omega_2 = 1.65$

$M_u = 46147.32$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.00 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00**

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 171 dJC\_Beam\_171 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 8320.655233 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 1604.71 N\*m

Mry = 11502.00 N\*m

Vfy = 121.693885 N

Vry = 19464.923077 N

Mfz = -26.33 N\*m

Mrz = 958.50 N\*m

Vfz = 15546.487051 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = -0.12

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.19 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.22 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.07 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 172 dJC\_Beam\_172 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -1318.883792 N

Tr = 383400.000000 N

Mfy = 692.03 N\*m

Mry = 11502.00 N\*m

Vfy = -24.937530 N

Vry = 19464.923077 N

Mfz = -3.96 N\*m

Mrz = 958.50 N\*m

Vfz = 7960.513323 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.26

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.06 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.03 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **173 dJC\_Beam\_173** POINT: **7**

COORDINATE: **x = 1.00 L = 282.86 mm**

LOADS:

Governing Load Case: 12 ULS /93/ 1\*0.90 + 6\*1.40 + 2\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 980.588320$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -229.87$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 50.995629$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -5.65$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -3163.713918$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$L_e = 282.86$  mm

$k = 0.77$

$\omega_2 = 2.50$

$M_u = 70074.98$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.03 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_y \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

$u_z = 0.0$  mm  $<$   $u_z \text{ max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /25/ 1\*1.00 + 5\*1.00 + 7\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **174 dJC\_Beam\_174** POINT: **7**

COORDINATE: **x = 1.00 L = 282.86 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -26.622853 N

Tr = 383400.000000 N

Mfy = 832.30 N\*m

Mry = 11502.00 N\*m

Vfy = 43.385842 N

Vry = 19464.923077 N

Mfz = -10.31 N\*m

Mrz = 958.50 N\*m

Vfz = 9082.996164 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.86 mm

k = -0.05

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.08 < 1.00$  (13.9.1)

$Mfy/Mre + Mfz/Mrz - Tf*Zy/(Mre*A) = 0.08 < 1.00$  (13.9.2(a))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 175 dJC\_Beam\_175 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -39.751143 N

Tr = 383400.000000 N

Mfy = -760.18 N\*m

Mry = 11502.00 N\*m

Vfy = -36.987362 N

Vry = 19464.923077 N

Mfz = -3.25 N\*m

Mrz = 958.50 N\*m

Vfz = -8408.731968 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = -0.07

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.07 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



*Deflections*

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



*Displacements Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 176 dJC\_Beam\_176 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -403.858509 N

Tr = 383400.000000 N

Mfy = 787.82 N\*m

Mry = 11502.00 N\*m

Vfy = -21.298249 N

Vry = 19464.923077 N

Mfz = -4.75 N\*m

Mrz = 958.50 N\*m

Vfz = 8853.344854 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.12

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.07 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 177 dJC\_Beam\_177 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 189.408571 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -543.93 N\*m

Mry = 11502.00 N\*m

Vfy = -61.593279 N

Vry = 19464.923077 N

Mfz = -0.27 N\*m

Mrz = 958.50 N\*m

Vfz = -6268.194448 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.04

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.05 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.05 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.03 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 178 dJC\_Beam\_178 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 772.798513 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 781.66 N\*m

Mry = 11502.00 N\*m

Vfy = -25.491348 N

Vry = 19464.923077 N

Mfz = -4.66 N\*m

Mrz = 958.50 N\*m

Vfz = 8656.368892 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.04

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.07 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.08 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **179 dJC\_Beam\_179** POINT: **7**

COORDINATE: **x = 1.00 L = 282.86 mm**

LOADS:

Governing Load Case: **12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -889.237777$  N

$T_r = 383400.000000$  N

$M_{fy} = -801.79$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -24.532276$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -4.11$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -9013.062510$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.86$  mm

$k = 0.06$

$\omega_m = 2.50$

$M_u = 70074.98$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.08 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.07 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.04 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $<$   $u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**

$u_z = 0.0$  mm  $<$   $u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**



Displacements *Not analyzed*

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 180 dJC\_Beam\_180 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /91/ 1\*1.25 + 6\*1.40 + 2\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 1135.560442 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = 226.50 N\*m

Mry = 11502.00 N\*m

Vfy = 40.994906 N

Vry = 19464.923077 N

Mfz = -4.80 N\*m

Mrz = 958.50 N\*m

Vfz = 3214.707912 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.79

om2 = 2.41

Mu = 67497.74 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.03 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.01 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **181 dJC\_Beam\_181** POINT: **7**

COORDINATE: **x = 1.00 L = 282.86 mm**

LOADS:

Governing Load Case: 12 ULS /101/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 4\*0.50

MATERIAL:

S 355 Fy = 355.00 MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

Tf = -1016.486020 N

Tr = 383400.000000 N

Mfy = -887.95 N\*m

Mry = 11502.00 N\*m

Vfy = 10.473999 N

Vry = 19464.923077 N

Mfz = -7.97 N\*m

Mrz = 958.50 N\*m

Vfz = -10017.394927 N

Vrz = 233579.076923 N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

Le = 282.86 mm

k = 0.20

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.09 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.08 < 1.00 (13.9.2(a))

Vfy/Vry = 0.00 < 1.00 (13.4.1) Vfz/Vrz = 0.04 < 1.00 (13.4.1)

LIMIT DISPLACEMENTS



Deflections

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 183 dJC\_Beam\_183 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /99/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 8219.486538 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -1608.13 N\*m

Mry = 11502.00 N\*m

Vfy = 123.329406 N

Vry = 19464.923077 N

Mfz = -26.16 N\*m

Mrz = 958.50 N\*m

Vfz = -15861.636394 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = -0.12

om2 = 2.50

Mu = 70074.96 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.19 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.22 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.01 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.07 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /29/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**

## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **184 dJC\_Beam\_184** POINT: **7**

COORDINATE: **x = 1.00 L = 282.86 mm**

LOADS:

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$C_f = 8321.299084$  N

$Cr_0 = 383400.000000$  N

CLASS: = Plastic

$M_{fy} = -1652.27$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = -108.879753$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = -15.14$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -15516.672761$  N

$V_{rz} = 233579.076923$  N



LATERAL BUCKLING PARAMETERS:

$Le = 282.86$  mm

$k = -0.14$

$\omega_2 = 2.50$

$M_u = 70074.98$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$C_f/Cr_0 + U_{1y} * M_{fy}/M_{ry} + U_{1z} * M_{fz}/M_{rz} = 0.18 < 1.00$  (13.8.3(a))

$C_f/Cr_z + U_{1y} * M_{fy}/M_{re} + U_{1z} * M_{fz}/M_{rz} = 0.21 < 1.00$  (13.8.3(c))

$V_{fy}/V_{ry} = 0.01 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.07 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: 15 SLS /31/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 4\*1.00



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 185 dJC\_Beam\_185 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /95/ 1\*1.25 + 2\*1.50 + 3\*0.50 + 5\*0.50 + 4\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Tf = -1649.010470 N

Tr = 383400.000000 N

Mfy = -693.52 N\*m

Mry = 11502.00 N\*m

Vfy = -175.758614 N

Vry = 19464.923077 N

Mfz = 4.44 N\*m

Mrz = 958.50 N\*m

Vfz = -7916.016462 N

Vrz = 233579.076923 N

CLASS: = Plastic



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = 0.27

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

Tf/Tr + Mfy/Mry + Mfz/Mrz = 0.07 < 1.00 (13.9.1)

Mfy/Mre + Mfz/Mrz - Tf\*Zy/(Mre\*A) = 0.06 < 1.00 (13.9.2(a))

Vfy/Vry = 0.01 < 1.00 (13.4.1) Vfz/Vrz = 0.03 < 1.00 (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00



**Displacements** Not analyzed

**Section OK !!!**



## STEEL DESIGN

CODE: **CAN/CSA S16-09**

ANALYSIS TYPE: **Member Verification**

CODE GROUP:

MEMBER: **186 dJC\_Beam\_186** POINT: **1**

COORDINATE: **x = 0.00 L = 0.00 mm**

LOADS:

Governing Load Case: **12 ULS /61/ 1\*1.25 + 6\*1.40**

MATERIAL:

S 355  $F_y = 355.00$  MPa



SECTION PARAMETERS: **RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

$A_y = 92.31$  mm<sup>2</sup>

$I_y = 1440000.00$  mm<sup>4</sup>

$Z_y = 36000.00$  mm<sup>3</sup>

$A_z = 1107.69$  mm<sup>2</sup>

$I_z = 10000.00$  mm<sup>4</sup>

$Z_z = 3000.00$  mm<sup>3</sup>

$A = 1200.00$  mm<sup>2</sup>

$J = 37899.23$  mm<sup>4</sup>

INTERNAL FORCES AND CAPACITIES:

$T_f = -1312.668871$  N

$T_r = 383400.000000$  N

$M_{fy} = 280.04$  N\*m

$M_{ry} = 11502.00$  N\*m

$V_{fy} = 2.944730$  N

$V_{ry} = 19464.923077$  N

$M_{fz} = 3.44$  N\*m

$M_{rz} = 958.50$  N\*m

$V_{fz} = -3115.340177$  N

$V_{rz} = 233579.076923$  N

CLASS: = Plastic



LATERAL BUCKLING PARAMETERS:

$L_e = 282.86$  mm

$k = 0.05$

$\omega_m = 2.50$

$M_u = 70074.98$  N\*m

$M_{re} = 11502.00$  N\*m

BUCKLING PARAMETERS:



About Y axis:



About Z axis:

VERIFICATION FORMULAS:

$T_f/T_r + M_{fy}/M_{ry} + M_{fz}/M_{rz} = 0.03 < 1.00$  (13.9.1)

$M_{fy}/M_{re} + M_{fz}/M_{rz} - T_f \cdot Z_y / (M_{re} \cdot A) = 0.02 < 1.00$  (13.9.2(a))

$V_{fy}/V_{ry} = 0.00 < 1.00$  (13.4.1)  $V_{fz}/V_{rz} = 0.01 < 1.00$  (13.4.1)

LIMIT DISPLACEMENTS



Deflections

$u_y = 0.0$  mm  $< u_{y \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /27/ 1\*1.00 + 2\*1.00 + 3\*1.00**

$u_z = 0.0$  mm  $< u_{z \max} = L/300.00 = 0.9$  mm

Verified

Governing Load Case: **15 SLS /24/ 1\*1.00 + 6\*1.00 + 5\*1.00 + 4\*1.00**



Displacements Not analyzed

**Section OK !!!**

## STEEL DESIGN

**CODE:** CAN/CSA S16-09

**ANALYSIS TYPE:** Member Verification

**CODE GROUP:**

**MEMBER:** 187 dJC\_Beam\_187 **POINT:** 7

**COORDINATE:** x = 1.00 L = 282.86 mm

**LOADS:**

Governing Load Case: 12 ULS /97/ 1\*1.25 + 2\*1.50 + 3\*0.50

**MATERIAL:**

S 355 Fy = 355.00 MPa



**SECTION PARAMETERS: RECT 120x10**

d=120.0 mm

b=10.0 mm

w=5.0 mm

t=5.0 mm

Ay=92.31 mm<sup>2</sup>

Iy=1440000.00 mm<sup>4</sup>

Zy=36000.00 mm<sup>3</sup>

Az=1107.69 mm<sup>2</sup>

Iz=10000.00 mm<sup>4</sup>

Zz=3000.00 mm<sup>3</sup>

A=1200.00 mm<sup>2</sup>

J=37899.23 mm<sup>4</sup>

**INTERNAL FORCES AND CAPACITIES:**

Cf = 38.767927 N

Cr0 = 383400.000000 N

CLASS: = Plastic

Mfy = -862.70 N\*m

Mry = 11502.00 N\*m

Vfy = -87.965436 N

Vry = 19464.923077 N

Mfz = -4.17 N\*m

Mrz = 958.50 N\*m

Vfz = -9373.044862 N

Vrz = 233579.076923 N



**LATERAL BUCKLING PARAMETERS:**

Le = 282.86 mm

k = -0.02

om2 = 2.50

Mu = 70074.98 N\*m

Mre = 11502.00 N\*m

**BUCKLING PARAMETERS:**



About Y axis:



About Z axis:

**VERIFICATION FORMULAS:**

$Cf/Cr0 + U1y*Mfy/Mry + U1z*Mfz/Mrz = 0.08 < 1.00$  (13.8.3(a))

$Cf/Crz + U1y*Mfy/Mre + U1z*Mfz/Mrz = 0.08 < 1.00$  (13.8.3(c))

$Vfy/Vry = 0.00 < 1.00$  (13.4.1)  $Vfz/Vrz = 0.04 < 1.00$  (13.4.1)

**LIMIT DISPLACEMENTS**



**Deflections**

uy = 0.0 mm < uy max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00

uz = 0.0 mm < uz max = L/300.00 = 0.9 mm

Verified

**Governing Load Case:** 15 SLS /26/ 1\*1.00 + 2\*1.00 + 3\*1.00 + 5\*1.00 + 4\*1.00





**Displacements** Not analyzed

**Section OK !!!**



## **Appendix G      Addendum**

Title : 49540.6110 Structural Analysis - Addendum REVO  
 Client : De Jong Combustion BV  
 Project : Carmon Creek  
 Number : 405109540

0	First issue				
		BvH	2015-06-27	ARo	2015-06-27
<b>Rev:</b>	<b>Description:</b>	<b>Prepared:</b>	<b>Date:</b>	<b>Checked:</b>	<b>Date:</b>

## 1 Introduction

For the Shell Carmon Creek site, 3 burner skid units will be delivered by De Jong Combustion BV. For each unit, 5 burner skids will be installed on an enclosure skid with dropover enclosure for protection against environmental conditions.

Alara-Lukagro BV has designed and manufactured the 3 enclosure skids and dropover enclosures.

This structural analysis addendum considers the lifting verification for the 3<sup>rd</sup> unit that showed a 250 mm deviation in all lifting point positions. The lifting points are assembled in mirrored positions.

Results will be shown for:

- Verification according Canadian structural code CSA S16-09
- Stress values in the structure
- Deformation values in the structure

This report is an addendum to approved document:  
 49540.6000 Structural Analysis – REV 1.0.

## 2 Materials - Primary steel

The following materials were used for the structural members.

Table 2-1 Primary structural steel

Application	Pos	Use		Grade	fy (MPa) yield	fu (MPa) tensile	Cert.
Rectangular Hollow Sections	Enclosure	Primary	EN 10219	S420MH	420	500-660	3.1
Open H-; I-; U- profiles	Skid	Primary	EN 10225	S355G11+M	355	460-490	3.2
Plating 2mm	Encl. Walls	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>1</sup>
Plating 3mm	Encl. Roof	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>1</sup>
Plating (Checker plate) 4mm	Skid Floor	Primary	EN 10025-2	S235JR	235	360-510	2.2 <sup>1</sup>

<sup>1</sup> EN 10152 is applicable for plate material, for impact test ref. EN 10025-1 §7.3.2.1 which states that impact tests are not required for nominal thickness <6mm.

Title : **49540.6110 Structural Analysis - Addendum REV0**  
 Client : **De Jong Combustion BV**  
 Project : **Carmon Creek**  
 Number : **405109540**

0	First issue				
		BvH	2015-06-27	ARo	2015-06-27
<b>Rev:</b>	<b>Description:</b>	<b>Prepared:</b>	<b>Date:</b>	<b>Checked:</b>	<b>Date:</b>

## 1 Introduction

For the Shell Carmon Creek site, 3 burner skid units will be delivered by De Jong Combustion BV. For each unit, 5 burner skids will be installed on an enclosure skid with dropover enclosure for protection against environmental conditions.

Alara-Lukagro BV has designed and manufactured the 3 enclosure skids and dropover enclosures.

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- Verification according Canadian structural code CSA S16-09
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 49540.6000 Structural Analysis – REV 1.0.

## 2 Materials - Primary steel

The following materials were used for the structural members.

*Table 2-1 Primary structural steel*

Application	Pos	Use		Grade	fy (MPa) yield	fu (MPa) tensile	Cert.
Rectangular Hollow Sections	Enclosure	Primary	EN 10219	S420MH	420	500-660	3.1
Open H-; I-; U- profiles	Skid	Primary	EN 10225	S355G11+M	355	460-490	3.2
Plating 2mm	Encl. Walls	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>1</sup>
Plating 3mm	Encl. Roof	Primary	EN 10152	DC01+ZE25	140	270-410	2.2 <sup>1</sup>
Plating (Checker plate) 4mm	Skid Floor	Primary	EN 10025-2	S235JR	235	360-510	2.2 <sup>1</sup>

<sup>1</sup> EN 10152 is applicable for plate material, for impact test ref. EN 10025-1 §7.3.2.1 which states that impact tests are not required for nominal thickness <6mm.

### 3 FEA Model

The set will be lifted from the enclosure skid with a spreader beam as seen below.

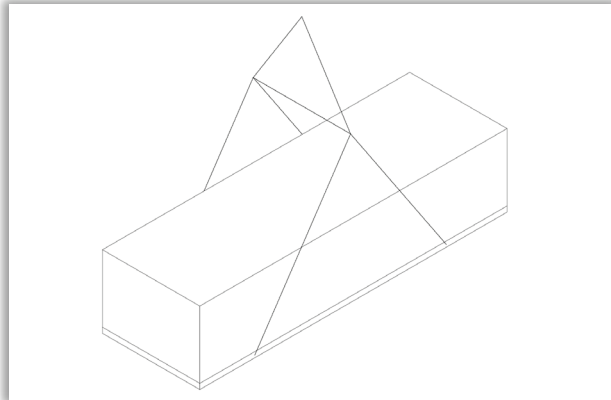


Figure 3-1 Lifting set up with spreader beam

To comply with the degrees of freedom of the lifting setup, the two lifting points on the left side are fixed in X, Y and Z direction and the lifting points on the right side are free to translate in X direction.

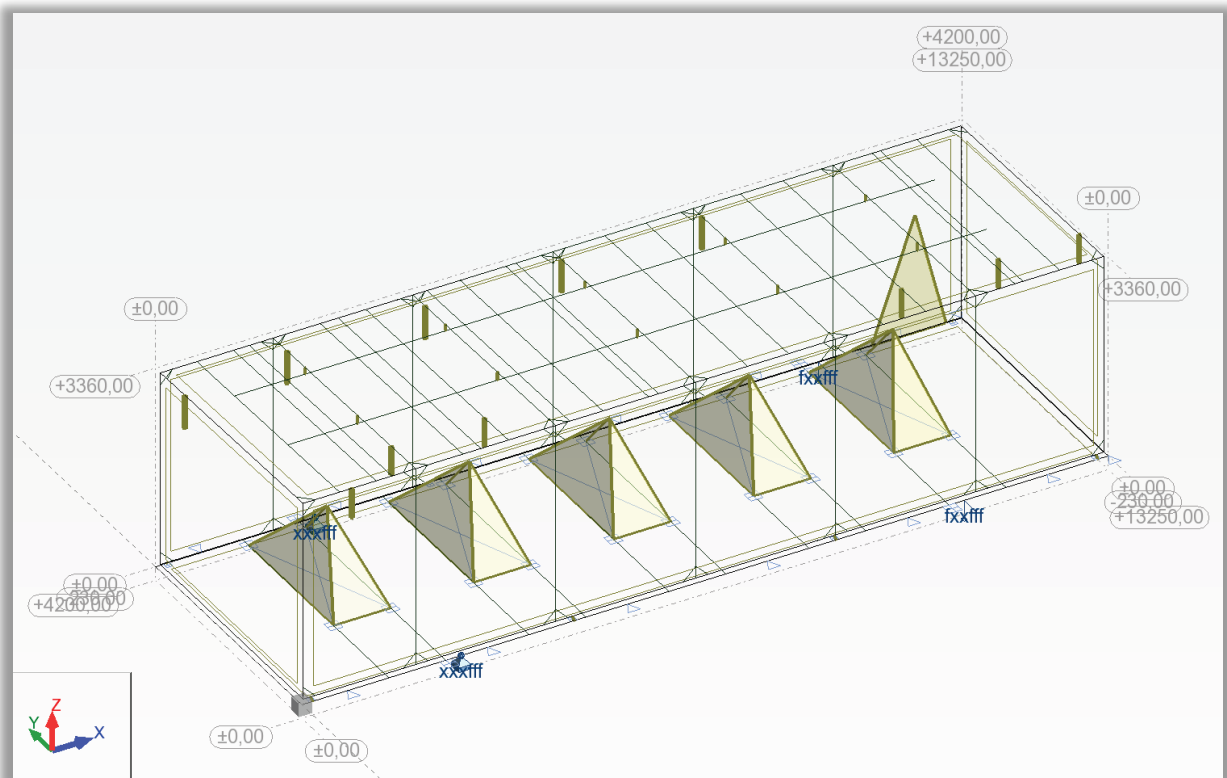


Figure 3-2 FEA model with constraints (x=fixed; f=free)

For this analysis the mirrored positions are used as seen in following Figure.

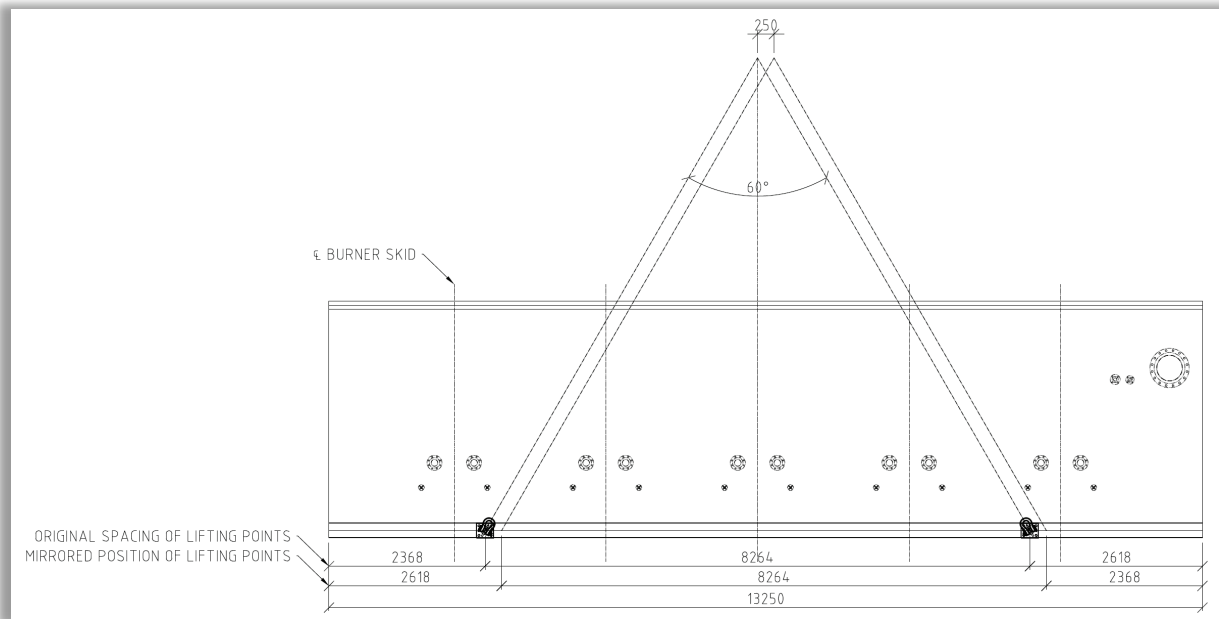


Figure 3-3 Original and mirrored lifting points spacing

#### 4 Load cases

Table 4-1 Load cases and application

Case	Load	Nature	Base Value	Application
1	Selfweight	Dead	Auto	Steel structure selfweight automatically added

Several nodal masses are added for all equipment.

The weight of the total structure is increased to reflect the weight of the produced unit of 25.500 kg. Please see attached weight control sheet for BU-101.

The weight is further increased to incorporate an impact factor of 1,1 up to 28.050 kg

#### 5 Results

Below the results of the structural calculation. The profiles will be checked according CSA S16-09. Stress and deformation will be displayed to show the behavior of the structure.

##### 5.1 Unity Checks

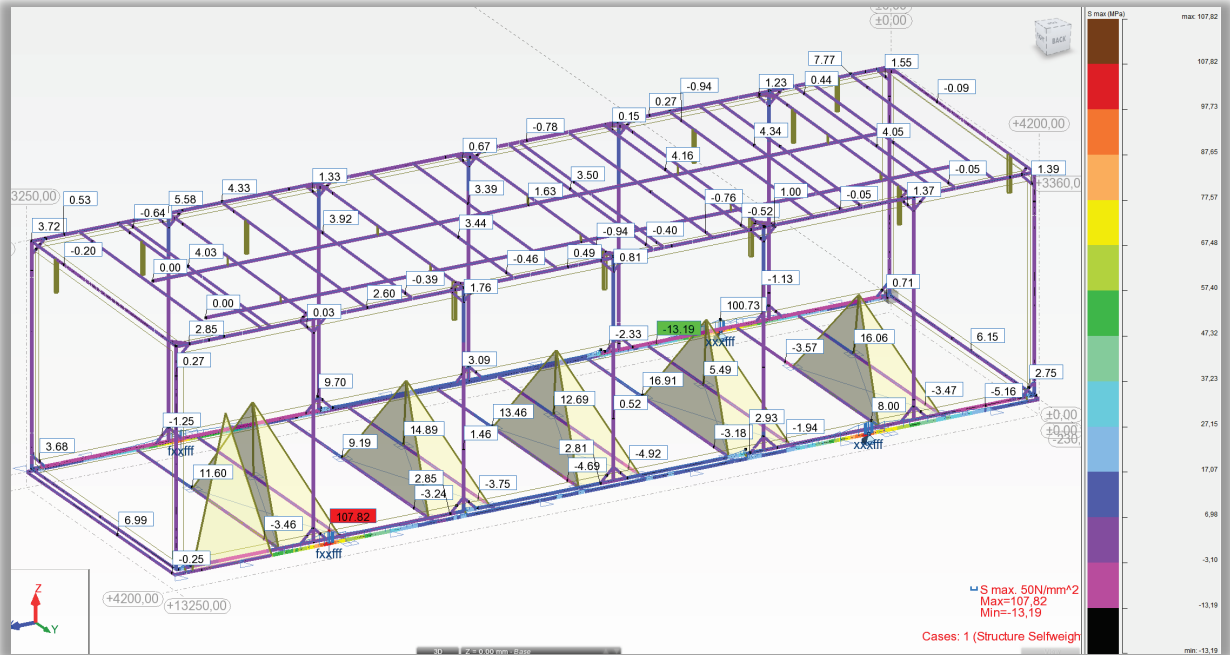
CAN/CSA S16-09 - Member Verification ( SLS ; ULS ) 2to17 20to27 35to50 52to71 77to98 100 102 104to114 131 133to142 144 145 147to156 158 171to181 183to194 196										
Member	Section	Material	Lay	Laz	Ratio	Case	Ratio(uy)	Case (uy)	Ratio(uz)	Case (uz)
4 Beam 4	HEA 240	S 355	131.79	220.67	0.99	1 Structure Selfweight	0.01	1 Structure Selfweight	0.07	1 Structure Selfweight
2 Beam 2	HEA 240	S 355	131.79	220.67	0.84	1 Structure Selfweight	0.00	1 Structure Selfweight	0.06	1 Structure Selfweight
8 dJC Bm Cm 8	IPE 140	S 355	200.41	695.65	0.11	1 Structure Selfweight	0.00	1 Structure Selfweight	0.01	1 Structure Selfweight
17 Beam 17	HEA 180	S 355	56.42	92.95	0.11	1 Structure Selfweight	0.01	1 Structure Selfweight	0.12	1 Structure Selfweight
6 Beam 6	HEA 180	S 355	56.42	92.95	0.10	1 Structure Selfweight	0.00	1 Structure Selfweight	0.10	1 Structure Selfweight
20	SHSH 100x100x6.3	S 420	169.54	169.54	0.10	1 Structure Selfweight	0.01	1 Structure Selfweight	0.00	1 Structure Selfweight
16 Beam 16	HEA 180	S 355	56.42	92.95	0.09	1 Structure Selfweight	0.01	1 Structure Selfweight	0.12	1 Structure Selfweight
85 dJC Beam 85	UNP 100	S 355	104.96	278.49	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.12	1 Structure Selfweight
7 Beam 7	HEA 180	S 355	56.42	92.95	0.09	1 Structure Selfweight	0.01	1 Structure Selfweight	0.11	1 Structure Selfweight
79 dJC Beam 79	UNP 100	S 355	104.96	278.49	0.09	1 Structure Selfweight	0.00	1 Structure Selfweight	0.11	1 Structure Selfweight

Figure 5-1 Unity Checks for top utilized profiles (>10%), sorted on overall ratio high to low

As can be seen the highest utilized members are the long beams HEA 240 4 and 2. 99% / 84% of its capacity is used and therefore suffices to the structural verification according CSA S16-09.



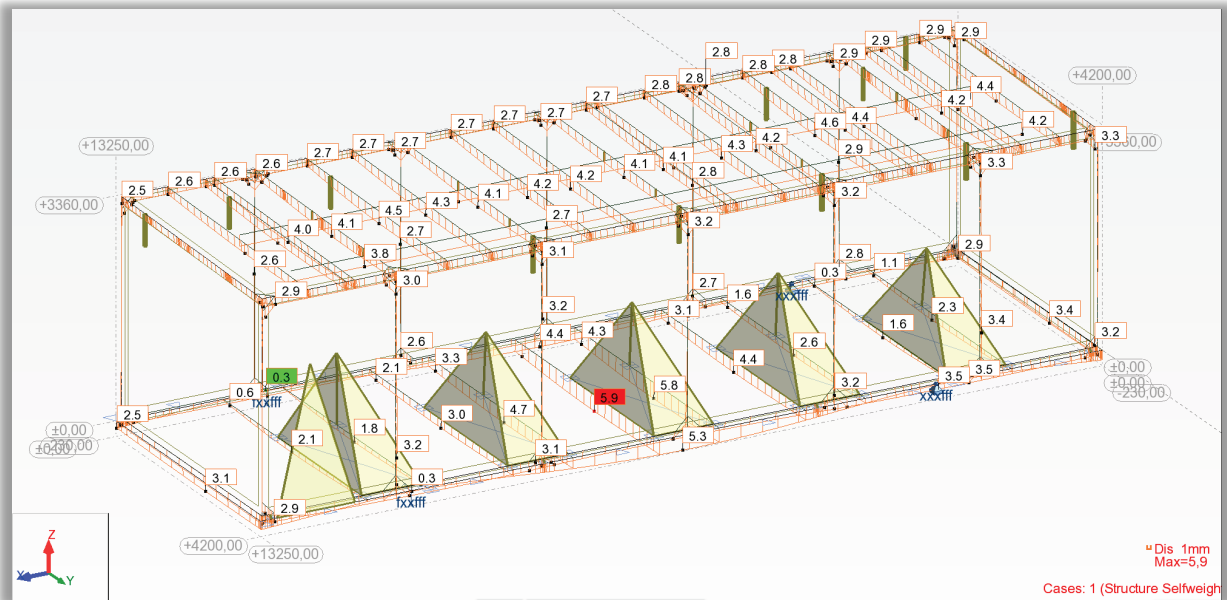
## 5.2 Stress



As can be seen the highest stress peak is 108 MPa.  
This is within limits:  $\max 108 < 355 \text{ MPa}$ .

## 5.3 Deformation

As can be seen the largest deformation is about 5,9 mm in the floor.  
This is within limits:  $(4200/5,9) = 1/711 < 1/300$ .







## 5.4 Conclusion

This report is an addendum to approved document:  
49540.6000 Structural Analysis – REV 1.0.

This structural analysis addendum considers the lifting verification of one of the units that showed a 250 mm deviation in all lifting point positions. The lifting points are assembled in mirrored positions.

The lifting calculation is updated with loads reflecting the lifted weight of 25,5T and increased with an impact factor of 1,1 for lifting.

- Verification according governing Canadian CSA S16-09 shows a max utilization of 99% of the carrying HEA240 longitudinal beam on the burner skid penetration side.
- The stress values in the structure are well below the stated limit of 355 MPa with a max peak of 108 MPa.
- The deformation values in the structure are well below stated limit of 1/300 with 5,9 mm global deformation in the floorbeams.

This concludes that the structure is safe for lifting considering the mirrored positions of the lifting points.

## 6 Appendix

- Weight Control Sheet for BU-101 25,5 T dated 22-06-2015

# Weight Control Data Sheet

Carmon Creek

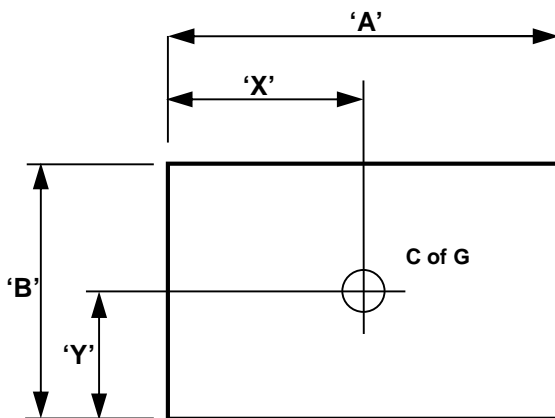
REQUISITION NO.:		Project NO.:		ISSUE:	
		<b>405109540</b>			
EQUIPMENT NO.:		EQUIPMENT DESCRIPTION:			
<b>BU-101</b>		<b>Acoustic Enclosure</b>			
TOLERANCE CODE (Please Tick (✓) appropriate box)	PRELIMINARY ESTIMATE	DESIGN ESTIMATE	M.T.O. CALCULATED	CATALOGUE WEIGHT	WEIGHED
					<b>X</b>

## WEIGHT DATA (Tonnes)

DRY	<b>25.50</b>	OPERATING		TEST	
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OTHER TEMPORARY WEIGHTS	DESCRIPTION <b>Slings + Shackles + Spreader Beam</b>	<b>0.30</b>
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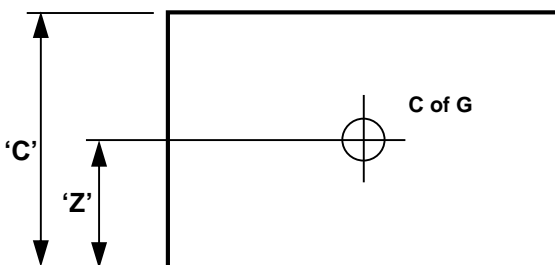
## DIMENSIONAL DATA (mm)



**PLAN**

OVERALL SIZES	
DIMENSION 'A'	<b>13200</b>
DIMENSION 'B'	<b>4200</b>
DIMENSION 'C'	<b>3700</b>

CENTRE OF GRAVITY		
DIM'N	DRY	OPERATING
'X'	<b>Ca. 6800</b>	
'Y'	<b>Ca. 2000</b>	
'Z'	<b>Ca. 1400</b>	



**ELEVATION**

**NOTES:**

- 1) ONE SHEET TO BE COMPLETED FOR EACH SEPARATELY INSTALLED SKID / ITEM.
- 2) EQUIPMENT ORIENTATION ON EACH SKID OR ITEM TO BE INDICATED.

Comments:	Revision	Date	Prepared By
	R00	22-06-2015	AVi